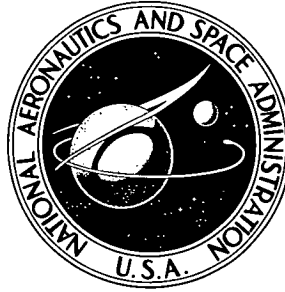


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ON 140° , 160° , AND 180° CONES
AT MACH NUMBERS FROM 2.30 TO 4.63
AND ANGLES OF ATTACK FROM 0° TO 20°

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SUMMARY

An experimental investigation has been conducted to obtain surface-pressure distributions on spherically blunted cones with apex angles of 140° , 160° , and 180° (flat disk). The 140° and 160° cones had a ratio of nose radius to base radius of 0.25. The studies were conducted at Mach numbers from 2.30 to 4.63 and at angles of attack from 0° to 20° .

Results of this study indicated that an increase in cone angle or angle of attack or both leads to an increase in pressure windward of the measured stagnation point; a decrease in cone angle or an increase in angle of attack leads to a decrease in pressure leeward of the measured stagnation point. Mach number has little effect on the pressure distributions for the cones at zero angle of attack. At angles of attack greater than zero, an increase in Mach number results in a decrease in pressure on the leeward side of all the configurations. A correlation parameter successfully correlates the stagnation-point locations for the entire range of test Mach number, cone angle, and angle of attack; an empirical representation of this correlation is in good agreement with the experimental results. Pressure distributions obtained on the cone models at zero angle of attack are in good agreement with a theoretical solution based on the one-strip method of integral relations. Circumferential pressure distributions on large-angle conical bodies are amenable to approximation by second-order polynomials.

INTRODUCTION

Vehicles with low ballistic coefficients (i.e., high aerodynamic drag) are being considered for use as unmanned probes to traverse planetary atmospheres. The function of this type of vehicle is to protect the payload from the severe loading and heating environments associated with entry while providing sufficient aerodynamic deceleration. One particular body shape which appears to be amenable to this type of mission is the large-angle cone (ref. 1). Optimization of the conical shape for a particular mission profile is dependent on an adequate knowledge of local flow properties, local aerodynamic heating

rates, and local structural loading. These criteria can be determined from surface-pressure distributions. The experimental investigations of references 2 and 3 provide pressure distributions on a 120° cone. For the purpose of optimization, the acquisition of similar pressure data on cones with larger apex angles is desirable.

The present investigation was undertaken to obtain surface-pressure distributions on 140° , 160° , and 180° cone configurations. The 140° and 160° cones had a ratio of nose radius to base radius of 0.25; the 180° cone was a flat disk. The data were obtained at Mach numbers from 2.30 to 4.63 and at angles of attack from 0° to 20° . Reynolds number for these studies was 2.0×10^6 based on model (base) diameter.

SYMBOLS

A,B,C	constants (see eq. (3))
C_p	pressure coefficient, $\frac{p_l - p_\infty}{q_\infty}$
D	base diameter
M_l	local Mach number
M_∞	free-stream Mach number
p_L	local static pressure along leeward ray ($\theta = 0^\circ$) for $\alpha > 0^\circ$
p_l	local static pressure
p_t	free-stream stagnation pressure
$p_{t,2}$	stagnation pressure behind a normal shock
p_W	local static pressure along windward ray ($\theta = 180^\circ$) for $\alpha > 0^\circ$
p_∞	free-stream static pressure
q_∞	free-stream dynamic pressure
r_b	base radius
r_n	nose radius

s	surface length (see fig. 1)
s^*	total surface length (i.e., surface length from most forward station on model to shoulder corner) (see fig. 1)
$(s/s^*)_{sp}$	stagnation-point location
α	angle of attack
β	nondimensionalized parameter used to correlate stagnation-point location, $\frac{\alpha}{120^\circ - \sigma_c}$ (see eq. (8))
γ	ratio of specific heats
θ	meridian angle
σ_c	cone semiapex angle
ϕ	roll angle

APPARATUS AND TESTS

Wind Tunnel

Studies were performed in the high Mach number test section of the Langley Unitary Plan wind tunnel, which is a variable-pressure continuous-flow facility. The test section is approximately 4 feet (1.22 meters) square and 7 feet (2.13 meters) long. The nozzle leading to the test section is of the asymmetric sliding-block type, which permits a continuous variation in the test-section Mach number from about 2.30 to 4.63.

Models and Instrumentation

Details of the cone models with apex angles of 140° , 160° , and 180° are presented in figure 1. The models were constructed of polished aluminum and had sharp shoulders. The 140° and 160° cone models had spherically blunted noses, the radii of which were 25 percent of the magnitude of the base radii. Some amount of thickness was necessary for the 180° cone (flat disk) to facilitate the installation of the pressure orifices. A sharp shoulder was produced in the 180° cone by the 15° bevel illustrated in figure 1(b). Base diameter of all the models was 8.00 inches (20.32 cm), and the sting utilized for the studies had a diameter of 1.50 inches (3.81 cm). The surfaces of the 140° and 160° cone

models were instrumented with 49 pressure orifices, whereas the 180° cone model was instrumented with 45 pressure orifices. (See fig. 1.) Internal diameter for the pressure orifices was 0.050 inch (0.127 cm). The orifices were located along the meridians $\theta = 0^\circ, 90^\circ, 180^\circ$, and 270° .

The pressures were recorded by using two 48-channel pressure-sampling valves which sequentially transmit each pressure sampling to an electrical pressure transducer. The transducer transforms the pressure information into an electrical signal which is then recorded in digital form on punch cards. The two gages had a maximum range of 10.0 psia (6.89 N/cm²).

Accuracy and Test Conditions

The accuracy of the pressure-sampling values is within 1 percent of the full-scale range of the gage; this accuracy includes all errors of linearity, hysteresis, and repeatability. The stagnation pressure was measured with a precision mercury manometer, the accuracy of which is ± 0.5 psf (± 23.94 N/m²). The models were tested at free-stream Mach numbers of 2.30, 2.96, 3.95, and 4.63 for a Reynolds number of 2.0×10^6 based on model (base) diameter. The results of a test-section calibration indicated the following deviations in Mach number:

For $M_\infty = 2.30$	± 0.02
For $M_\infty = 2.96$	± 0.02
For $M_\infty = 3.95$	± 0.06
For $M_\infty = 4.63$	± 0.05

Tunnel stagnation temperatures were 150° F (338.7° K) at $M_\infty = 2.30$ and 2.96 and 175° F (352.6° K) at $M_\infty = 3.95$ and 4.63. Pressure data were obtained for the models at angles of attack from 0° to 20° for a zero sideslip condition. Circumferential pressure distributions were obtained by rolling the model from 0° to 90° at constant angles of attack. Boundary-layer trips were not affixed to the models and base pressure measurements were not made.

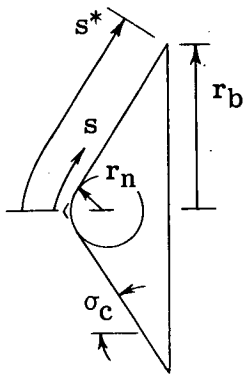
TABULATION OF EXPERIMENTAL DATA

The experimental pressure data obtained during the course of this investigation are presented in tables I to XII. Listed along with the measured static pressures are the pressure coefficients and Mach numbers. The values of $p_l/p_{t,2}$ and M_l are based on the computed stagnation pressure behind a normal shock, which was obtained from normal-shock relations, together with free-stream Mach number and stagnation pressure. The isentropic flow equation used to calculate M_l is

$$M_L = \sqrt{\frac{2}{\gamma - 1} \left[\left(\frac{p_L}{p_{t,2}} \right)^{\frac{\gamma-1}{\gamma}} - 1 \right]} \quad (1)$$

where the value γ was taken to be 1.4.

Each pressure listed in the tables is identified by an orifice number (as defined in fig. 1) and the associated meridian angle and surface length. Surface length is presented nondimensionalized by both the base diameter D and the total surface length s^* . For the spherically blunted cone, as illustrated in the sketch, the total surface length is found to be



$$s^* = r_n (90^\circ - \sigma_c) + \csc \sigma_c (r_b - r_n \cos \sigma_c) \quad (2)$$

An index to the tabular data is as follows:

Model	M_∞	Table (*)
140° cone	2.30	I
	2.96	II
	3.95	III
	4.63	IV
160° cone	2.30	V
	2.96	VI
	3.95	VII
	4.63	VIII
180° cone (flat disk)	2.30	IX
	2.96	X
	3.95	XI
	4.63	XII

*Each table is divided into five parts with part (a) being for $\alpha = 0^\circ$, part (b) for $\alpha = 5^\circ$, part (c) for $\alpha = 10^\circ$, part (d) for $\alpha = 15^\circ$, and part (e) for $\alpha = 20^\circ$.

It should be noted that the data for orifice 29 on the 140° cone were incorrect because of leakage and are not presented in the tables.

RESULTS AND DISCUSSION

The discussion presented herein is limited to the effects of cone angle, angle of attack, and free-stream Mach number on the variation of local static pressure.

Experimental Pressure Distributions

The effect of cone angle on the pressure distributions can be seen in figure 2, in which the local static pressures, nondimensionalized by stagnation pressure behind a normal shock, are plotted as a function of local surface length, nondimensionalized by total surface length. These results are presented for a free-stream Mach number of 2.96 and for angles of attack of 0° , 10° , and 20° and are typical of those results obtained at the other test Mach numbers. Experimental data for a 120° cone (ref. 2), having the same percentage of nose bluntness as the 140° and 160° cone models of the present investigation, are included for comparison.

As shown in figure 2, at zero angle of attack, an increase in cone angle results in an increase in pressure over the entire face of the cone, and the stagnation point (indicated by the maximum measured pressure) is located, as expected, at the apex of the cones regardless of cone angle. At an angle of attack of 10° , the stagnation point shifts to the windward side of the cones, and the pressures in the direction of the windward shoulder become noticeably greater than those for the $\alpha = 0^\circ$ condition. Further increase in angle of attack accentuates this shift in stagnation-point location and increase in pressure. Similarly, for angles of attack greater than 0° , an increase in cone angle leads to a further shift in stagnation-point location toward the windward shoulder. Increasing cone angle also results in increases in the pressures located between the stagnation point and the windward shoulder; however, the greatest pressure increase for an increase in cone angle occurs at zero angle of attack.

For the cones at an angle of attack greater than 0° , the expanded flow around the spherical nose results in decreases in pressure from the maximum value at the stagnation point; this decrease in pressure toward the leeward side becomes more significant with decrease in cone angle and increase in angle of attack. The data indicate the existence of an adverse pressure gradient near the sphere-cone juncture on the leeward sides of the 120° cone at $\alpha = 10^\circ$ and the 120° and 140° cones at $\alpha = 20^\circ$. Increasing cone angle from 120° decreases the strength of the expansion and adverse pressure gradient, so that a uniform pressure distribution exists on the flat disk (180° cone).

The experimental results presented in figure 2 for the models at $\alpha = 0^\circ$ and $M_\infty = 2.96$ are compared in figure 3 with the results from the one-strip method of integral relations described in reference 4. The pressures predicted by the integral-relations method are in good agreement with the experimental values for all the cone models. A maximum deviation in agreement occurs at a value of s/s^* of about 0.8, where the theoretical predictions are approximately 3 percent less than the experimental values.

The effect of angle of attack on the pressure distributions of the three cone models is more clearly illustrated in figures 4 to 6 for all the test Mach numbers. The curves faired through the pressure data are extrapolated to the sonic condition which theoretically exists at the shoulder. As previously indicated, an increase in angle of attack results in higher pressures on the windward side and lower pressures on the leeward side. A progressive shift in the stagnation point toward the windward shoulder is noted as angle of attack is increased to the highest test value. The adverse pressure gradient located near the sphere-cone juncture on the leeward side of the 140° cone (mentioned previously) is seen in figure 4 to increase with increased angle of attack. Similar trends in pressure distribution exist for the 160° cone, as shown in figure 5, though to a lesser degree than exist for the 140° cone. Increasing cone angle and decreasing angle of attack have similar effects on the pressure distributions on the leeward side of the models; increasing cone angle and increasing angle of attack have similar effects on the pressure distributions on the windward side.

The data presented in figures 7 to 9 illustrate the effect of free-stream Mach number on the pressure distributions for the cone models at angles of attack of 0° , 10° , and 20° . At $\alpha = 0^\circ$, only small effects of Mach number are seen for the different cone configurations. The small differences in pressure between the 0° and 180° meridians noted at the highest test Mach numbers are probably due to slight data acquisition inaccuracies. At angles of attack greater than 0° , the pressures windward of the stagnation point are relatively insensitive to increase in Mach number, whereas the pressures leeward of the stagnation point decrease with increased Mach number. This decrease in pressure is particularly obvious near the sphere-cone juncture. An increase in angle of attack increases this Mach number effect.

Pressures obtained by rolling the cone models from 0° to 90° at a constant angle of attack are presented in figures 10 to 12 for $M_\infty = 2.96$. Data shown for $0^\circ \leq \theta \leq 90^\circ$ were actually obtained in the quadrant $270^\circ \leq \theta \leq 360^\circ$, but since the flow is symmetrical about the plane of symmetry, they are presented as a continuous variation of θ from 0° to 180° . For each s/D station for which circumferential pressure distributions are shown, local pressure is nondimensionalized by the pressure along the windward meridian ($\theta = 180^\circ$). Plotted in this form, the circumferential pressures show progressively

larger variations from the windward meridian ($\theta = 180^\circ$) to the leeward meridian ($\theta = 0^\circ$) at increased distances from the nose or at larger angles of attack or both.

Analytical Pressure Distributions

Attempts have been made by several investigators to curve-fit the type of circumferential pressure distributions plotted in figures 10 to 12 by using a second-order polynomial of the form

$$\frac{p_l}{p_w} = A \cos^2 \theta + B \cos \theta + C \quad (3)$$

In particular, reference 2 has shown that equation (3) provides good agreement with experimental pressures obtained on a 120° cone if the following conditions are met:

At $\theta = 0^\circ$,

$$\frac{p_l}{p_w} = \frac{p_L}{p_w}$$

at $\theta = 180^\circ$,

$$\frac{p_l}{p_w} = 1$$

and at $\theta = 0^\circ$,

$$\frac{d^2}{d\theta^2} \left(\frac{p_l}{p_w} \right) = 0$$

By using these conditions, equation (3) becomes

$$\frac{p_l}{p_w} = \frac{1}{4} \left(1 - \frac{p_L}{p_w} \right) (\cos^2 \theta - 2 \cos \theta - 3) + 1 \quad (4)$$

The circumferential pressure distributions predicted by this expression for the 120° cone are seen in figures 10 to 12 to provide good agreement with the measured values of the 140° , 160° , and 180° cone data; however, some degradation of agreement is noted with increased cone angle. The circumferential pressure distributions on a flat disk also have been approximated by the following empirical expression, which was derived by Robert L. Stallings, Jr., of the Langley Research Center:

$$\frac{p_l}{p_w} = \left(1 - \frac{p_L}{p_w} \right) (0.072 \cos^2 \theta - 0.500 \cos \theta + 0.428) + \frac{p_L}{p_w} \quad (5)$$

The curves derived from this expression are presented in figure 12 and are seen generally to provide a better estimation of the circumferential pressure distributions on the flat disk than the curves given by equation (4).

The extent to which the circumferential pressure distributions for the three cone models deviate from those predicted by equations (4) and (5) can be found by separating the variables of these equations. Equation (4) becomes

$$\frac{p_W - p_L}{p_W - p_L} = \frac{1}{4}(-\cos^2 \theta + 2 \cos \theta + 3) \quad (6)$$

and equation (5) becomes

$$\frac{p_W - p_L}{p_W - p_L} = 1 - (0.072 \cos^2 \theta - 0.500 \cos \theta + 0.428) \quad (7)$$

Curves obtained from these expressions are presented in figure 13 along with experimental results obtained from figures 10 to 12 for the three cone models. It should be noted that the experimental results shown are averaged values obtained from the various conditions of s/D and α in figures 10 to 12 for which the curve fits were attempted. As can be seen, good agreement exists between the experimental circumferential pressures obtained for the 140° cone and those estimated by equation (6), whereas increasing cone angle results in greater disagreement between this expression and the experimental data. The circumferential pressure distribution generated by equation (7) agrees well with that obtained experimentally on the flat disk. These results indicate that circumferential pressure distributions on large-angle conical bodies are amenable to approximation by second-order polynomials.

The experimental data presented in figures 2 to 9 have indicated that the movement of the stagnation point along the windward meridian is dependent primarily on cone angle and angle of attack. An attempt was made to correlate the stagnation-point locations for the cone configurations of this investigation and of reference 2 by using a correlating parameter similar to that suggested in reference 2. Experimental stagnation-point location $(s/s^*)_{sp}$ is shown in figure 14 as a function of the nondimensionalized parameter $\frac{\alpha}{120^\circ - \sigma_c} = \beta$. By using these experimental data, an empirical expression was generated by the method of least squares resulting in the following third-order polynomial equation:

$$\left(\frac{s}{s^*}\right)_{sp} = -4.210\beta^3 + 3.825\beta^2 + 0.432\beta \quad (8)$$

As can be seen in figure 14, this expression yields a smooth variation in $(s/s^*)_{sp}$ with β . The maximum deviation between the experimental data and empirical curve is within

about 0.1 of $(s/s^*)_{sp}$ for the entire range of cone angle, angle of attack, and Mach number.

CONCLUDING REMARKS

Local flow properties have been experimentally obtained from surface-pressure distributions on spherically blunted cones with apex angles of 140° , 160° , and 180° . The 140° and 160° cones had a ratio of nose radius to base radius of 0.25; the 180° cone was a flat disk. The studies were conducted at Mach numbers from 2.30 to 4.63 and at angles of attack from 0° to 20° . Analysis of the results was limited to variations in local static pressure and indicated the following concluding remarks:

1. An increase in cone angle or angle of attack or both leads to an increase in pressure windward of the measured stagnation point; a decrease in cone angle or an increase in angle of attack leads to a decrease in pressure leeward of the measured stagnation point.
2. Mach number has little effect on the pressure distributions for the cones at zero angle of attack. At angles of attack greater than zero, an increase in Mach number results in a decrease in pressure on the leeward side of all the configurations.
3. A correlation parameter successfully correlates the stagnation-point locations for the entire range of test Mach number, cone angle, and angle of attack; an empirical representation of this correlation is in good agreement with the experimental results.
4. Pressure distributions obtained on the cone models at zero angle of attack are in good agreement with a theoretical solution based on the one-strip method of integral relations.
5. Circumferential pressure distributions on large-angle conical bodies are amenable to approximation by second-order polynomials.

Langley Research Center,

National Aeronautics and Space Administration,

Langley Station, Hampton, Va., February 18, 1969,

124-07-03-12-23.

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TABLE 1.- DATA^a FOR 140° CONE; $M_{\infty} = 2.30$ (a) $\alpha = 0^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ$, $p_t = 2292.0$ psf					$\phi = 22.5^\circ$, $p_t = 2291.0$ psf					$\phi = 45.0^\circ$, $p_t = 2291.6$ psf				
				p_t , psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,\infty}$	M_L	p_t , psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,\infty}$	M_L	p_t , psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,\infty}$	M_L
1	0	0.330	0.000	1332.0	1.692	0.9931	7.26695	7.26695	1333.5	1.695	0.9785	7.27810	-0.5543	1331.5	1.693	0.9759	7.27619	-0.5868
2	0	0.330	0.025	1327.2	1.595	0.9273	7.24071	-1.0216	1327.1	1.606	0.9304	7.24071	-1.0216	1327.1	1.606	0.9304	7.24071	-1.0216
3	0	0.330	0.050	1322.8	1.564	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
4	0	0.330	0.075	1318.4	1.544	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
5	0	0.330	0.100	1314.0	1.524	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
6	0	0.330	0.125	1309.6	1.504	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
7	0	0.330	0.150	1305.2	1.484	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
8	0	0.330	0.175	1300.8	1.464	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
9	0	0.330	0.200	1296.4	1.444	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
10	0	0.330	0.225	1292.0	1.424	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
11	0	0.330	0.250	1287.6	1.404	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
12	0	0.330	0.275	1283.2	1.384	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
13	0	0.330	0.300	1278.8	1.364	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
14	0	0.330	0.325	1274.4	1.344	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
15	0	0.330	0.350	1270.0	1.324	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
16	0	0.330	0.375	1265.6	1.304	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
17	0	0.330	0.400	1261.2	1.284	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
18	0	0.330	0.425	1256.8	1.264	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
19	0	0.330	0.450	1252.4	1.244	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
20	0	0.330	0.475	1248.0	1.224	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
21	0	0.330	0.500	1243.6	1.204	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
22	0	0.330	0.525	1239.2	1.184	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
23	0	0.330	0.550	1234.8	1.164	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
24	0	0.330	0.575	1230.4	1.144	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
25	0	0.330	0.600	1226.0	1.124	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
26	0	0.330	0.625	1221.6	1.104	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
27	0	0.330	0.650	1217.2	1.084	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
28	0	0.330	0.675	1212.8	1.064	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
29	0	0.330	0.700	1208.4	1.044	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
30	0	0.330	0.725	1204.0	1.024	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
31	0	0.330	0.750	1199.6	1.004	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
32	0	0.330	0.775	1195.2	0.984	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
33	0	0.330	0.800	1190.8	0.964	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
34	0	0.330	0.825	1186.4	0.944	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
35	0	0.330	0.850	1182.0	0.924	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
36	0	0.330	0.875	1177.6	0.904	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
37	0	0.330	0.900	1173.2	0.884	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
38	0	0.330	0.925	1168.8	0.864	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
39	0	0.330	0.950	1164.4	0.844	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
40	0	0.330	0.975	1160.0	0.824	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
41	0	0.330	1.000	1155.6	0.804	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
42	0	0.330	1.025	1151.2	0.784	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
43	0	0.330	1.050	1146.8	0.764	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
44	0	0.330	1.075	1142.4	0.744	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
45	0	0.330	1.100	1138.0	0.724	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
46	0	0.330	1.125	1133.6	0.704	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
47	0	0.330	1.150	1129.2	0.684	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
48	0	0.330	1.175	1124.8	0.664	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558
49	0	0.330	1.200	1120.4	0.644	0.9198	7.16229	-1.8145	1321.3	1.637	0.9350	7.17338	-1.5637	1316.3	1.678	0.9032	7.17150	-1.5558

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE 1. - DATA^a FOR 140° CONE; $M_{\infty} = 2.30$ - Continued

(a) $\alpha = 0^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ, P_t = 2291.7 \text{ psf}$					$\Phi = 90.0^\circ, P_t = 2291.5 \text{ psf}$				
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/\rho\infty$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/\rho\infty$	M_t
1	0	+0.20	+0.000	1331.9	1.492	+0.9637	7.26730	+0.7206	1335.1	1.497	+0.9885	7.28536	+0.4055
2	0	+0.50	+0.025	1328.7	1.488	+0.9398	7.24987	+0.9289	1333.3	1.490	+0.9527	7.25922	+0.8237
3	0	+1.00	+0.043	1322.3	1.478	+0.8991	7.21501	+1.2462	1333.9	1.481	+0.9049	7.22436	+1.1694
4	0	+1.50	+0.086	1306.3	1.455	+0.7726	7.12788	+1.8195	1334.3	1.466	+0.8121	7.17207	+1.5521
5	0	+2.00	+0.125	1289.4	1.431	+0.6531	7.06431	+2.0444	1309.5	1.460	+0.7973	7.14593	+1.7128
6	0	+2.50	+0.163	1270.4	1.407	+0.5346	6.96551	+2.2514	1292.0	1.454	+0.7376	7.10235	+1.9527
7	0	+3.00	+0.200	1248.0	1.422	+0.6053	7.00518	+2.4053	1284.0	1.462	+0.9062	7.05007	+2.2086
8	0	+3.50	+0.237	1217.2	1.493	+0.9598	6.93617	+2.6594	1272.8	1.606	+0.9525	6.96449	+2.4630
9	0	+4.00	+0.275	1185.0	1.518	+0.9097	6.82269	+2.8171	1250.5	1.571	+0.9408	6.89321	+2.7151
10	0	+4.50	+0.312	1150.5	1.548	+0.8329	6.68289	+2.9103	1230.2	1.571	+0.9408	6.89321	+2.7151
11	0	+5.00	+0.350	1115.5	1.586	+0.7264	6.51946	+3.0046	1208.1	1.559	+0.9286	6.87120	+2.9694
12	0	+5.50	+0.388	1080.1	1.622	+0.6340	6.37681	+3.1014	1184.9	1.540	+0.9164	6.84848	+3.2232
13	0	+6.00	+0.426	1044.4	1.658	+0.5562	6.24994	+3.2000	1161.8	1.523	+0.9044	6.82608	+3.4770
14	0	+6.50	+0.464	1008.7	1.694	+0.4886	6.13499	+3.2999	1138.7	1.498	+0.8921	6.80387	+3.7307
15	0	+7.00	+0.502	973.0	1.730	+0.4309	6.02858	+3.4000	1115.6	1.471	+0.8815	6.78194	+3.9845
16	0	+7.50	+0.540	937.3	1.766	+0.3732	5.92826	+3.5000	1092.6	1.443	+0.8698	6.76049	+4.2382
17	0	+8.00	+0.578	901.5	1.802	+0.3256	5.83361	+3.6000	1069.6	1.408	+0.8581	6.73947	+4.4920
18	0	+8.50	+0.616	865.8	1.838	+0.2879	5.74427	+3.7000	1046.6	1.373	+0.8464	6.71886	+4.7457
19	0	+9.00	+0.654	830.1	1.874	+0.2502	5.65967	+3.8000	1023.6	1.338	+0.8347	6.69865	+5.0000
20	0	+9.50	+0.692	794.4	1.910	+0.2125	5.57947	+3.9000	1000.6	1.303	+0.8230	6.67884	+5.2543
21	0	+10.00	+0.730	758.7	1.946	+0.1748	5.50326	+4.0000	977.6	1.268	+0.8113	6.65947	+5.5086
22	180	+2.00	+0.025	1304.1	1.485	+0.9157	7.27601	+0.8499	1335.0	1.695	+0.9876	7.28473	+0.4264
23	180	+4.00	+0.050	1268.5	1.483	+0.8959	7.12575	+1.0988	1327.5	1.697	+0.9878	7.24111	+0.1077
24	180	+6.00	+0.075	1232.9	1.481	+0.8761	6.97550	+1.3479	1320.0	1.699	+0.9880	7.19844	+0.1914
25	180	+8.00	+0.100	1197.3	1.479	+0.8563	6.82524	+1.5970	1312.6	1.654	+0.9802	7.16259	+0.1921
26	180	+1.00	+0.025	1330.1	1.468	+0.9736	7.16530	+1.1744	1303.0	1.650	+0.9784	7.11055	+0.1914
27	180	+1.20	+0.150	1289.6	1.436	+0.6770	7.08417	+1.2709	1293.4	1.636	+0.9676	7.05790	+0.2121
28	180	+1.40	+0.275	1249.0	1.406	+0.5613	6.96233	+1.3633	1283.9	1.622	+0.9569	7.00583	+0.2328
29	180	+1.60	+0.400	1208.4	1.376	+0.4456	6.84003	+1.4557	1274.5	1.608	+0.9461	6.95396	+0.2535
30	180	+1.80	+0.525	1167.8	1.346	+0.3300	6.71773	+1.5480	1265.0	1.594	+0.9353	6.90209	+0.2742
31	180	+2.00	+0.650	1127.2	1.316	+0.2143	6.59543	+1.6404	1255.5	1.579	+0.9246	6.85022	+0.2949
32	180	+2.20	+0.775	1086.6	1.286	+0.1563	6.50597	+1.7328	1246.0	1.565	+0.9138	6.79847	+0.3156
33	180	+2.40	+0.900	1046.0	1.256	+0.0983	6.41650	+1.8252	1236.5	1.551	+0.9030	6.74672	+0.3363
34	180	+2.60	+1.025	1005.4	1.226	+0.0403	6.32704	+1.9176	1227.0	1.536	+0.8922	6.69497	+0.3570
35	180	+2.80	+1.150	964.8	1.196	+0.0000	6.23758	+2.0100	1217.5	1.522	+0.8814	6.64322	+0.3777
36	180	+3.00	+1.275	924.2	1.166	+0.0000	6.14812	+2.1024	1208.0	1.508	+0.8706	6.59147	+0.3984
37	180	+3.20	+1.400	883.6	1.136	+0.0000	6.05866	+2.1948	1198.5	1.494	+0.8598	6.53972	+0.4191
38	180	+3.40	+1.525	843.0	1.106	+0.0000	5.96920	+2.2872	1189.0	1.480	+0.8490	6.48797	+0.4398
39	180	+3.60	+1.650	802.4	1.076	+0.0000	5.87974	+2.3796	1179.5	1.466	+0.8382	6.43622	+0.4605
40	180	+3.80	+1.775	761.8	1.046	+0.0000	5.79028	+2.4720	1170.0	1.452	+0.8274	6.38447	+0.4812
41	180	+4.00	+1.900	721.2	1.016	+0.0000	5.70082	+2.5644	1160.5	1.438	+0.8166	6.33272	+0.5019
42	180	+4.20	+2.025	680.6	0.986	+0.0000	5.61136	+2.6568	1151.0	1.424	+0.8058	6.28097	+0.5226
43	180	+4.40	+2.150	640.0	0.956	+0.0000	5.52190	+2.7492	1141.5	1.410	+0.7950	6.22922	+0.5433
44	180	+4.60	+2.275	600.4	0.926	+0.0000	5.43244	+2.8416	1132.0	1.396	+0.7842	6.17747	+0.5640
45	180	+4.80	+2.400	560.8	0.896	+0.0000	5.34298	+2.9340	1122.5	1.382	+0.7734	6.12572	+0.5847
46	180	+5.00	+2.525	521.2	0.866	+0.0000	5.25352	+3.0264	1113.0	1.368	+0.7626	6.07397	+0.6054
47	180	+5.20	+2.650	481.6	0.836	+0.0000	5.16406	+3.1188	1103.5	1.354	+0.7518	6.02222	+0.6261
48	180	+5.40	+2.775	442.0	0.806	+0.0000	5.07460	+3.2112	1094.0	1.340	+0.7410	5.97047	+0.6468
49	180	+5.60	+2.900	402.4	0.776	+0.0000	4.98514	+3.3036	1084.5	1.326	+0.7302	5.91872	+0.6675

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE I.- DATA^a FOR 140° CONE; $M_{\infty} = 2.30$ - Continued(b) $\alpha = 5^\circ$

Orifice θ , deg	s , in.	s/D	s/k^*	$\Phi = 0.0^\circ$, $P_t = 2292.5$ psf					$\Phi = 22.5^\circ$, $P_t = 2290.5$ psf					$\Phi = 45.0^\circ$, $P_t = 2291.6$ psf				
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t\infty}$	M_t
1	0	.320	.3000	1324.1	1.630	.99019	7.22221	-1.1875	1317.2	1.675	.98740	7.20186	-1.3470	1323.8	1.576	.98812	7.20712	-1.3076
2	0	.420	.2500	1293.8	1.636	.97466	7.10896	-1.2178	1294.5	1.644	.97186	7.08851	-1.2034	1304.8	1.653	.97617	7.11997	-1.1892
3	0	.520	.2000	1264.2	1.641	.95950	6.95668	-1.2512	1265.1	1.635	.95708	6.93504	-1.1780	1289.9	1.629	.96423	7.03282	-1.1050
4	0	.620	.1500	1234.6	1.645	.94433	6.80311	-1.2847	1235.3	1.604	.95194	6.84029	-1.1476	1260.9	1.613	.95825	6.98925	-1.0328
5	0	.720	.1000	1205.0	1.649	.92916	6.64957	-1.3182	1205.7	1.573	.93956	6.89669	-1.1172	1231.3	1.603	.95108	6.93925	-0.9606
6	0	.820	.0500	1175.4	1.653	.91399	6.49600	-1.3517	1176.1	1.542	.92438	6.84388	-1.0868	1201.7	1.592	.94391	6.88925	-0.8884
7	0	.920	.0000	1145.8	1.657	.89882	6.34243	-1.3852	1146.5	1.511	.90978	6.79126	-1.0560	1172.1	1.581	.93644	6.83469	-0.8162
8	0	1.020	.0000	1116.2	1.661	.88365	6.18886	-1.4187	1116.9	1.480	.89464	6.73909	-1.0252	1142.5	1.570	.92897	6.77938	-0.7440
9	0	1.120	.0000	1086.6	1.665	.86848	6.03529	-1.4522	1087.3	1.449	.87964	6.68632	-0.9944	1112.9	1.559	.92150	6.72467	-0.6718
10	0	1.220	.0000	1057.0	1.669	.85331	5.88172	-1.4857	1057.7	1.418	.86481	6.63375	-0.9636	1083.3	1.548	.91402	6.66996	-0.6000
11	0	1.320	.0000	1027.4	1.673	.83814	5.72815	-1.5192	1028.1	1.387	.84992	6.58118	-0.9328	1053.7	1.537	.90654	6.61521	-0.5282
12	0	1.420	.0000	997.8	1.677	.82297	5.57458	-1.5527	998.5	1.356	.83575	6.52861	-0.9020	1024.1	1.526	.89906	6.56046	-0.4564
13	0	1.520	.0000	968.2	1.681	.80780	5.42101	-1.5862	968.9	1.325	.82152	6.47604	-0.8712	994.5	1.515	.89158	6.50571	-0.3846
14	0	1.620	.0000	938.6	1.685	.79263	5.26744	-1.6197	939.3	1.294	.80729	6.42347	-0.8404	964.9	1.504	.88410	6.45096	-0.3128
15	0	1.720	.0000	909.0	1.689	.77746	5.11387	-1.6532	909.7	1.263	.79306	6.37090	-0.8096	935.3	1.493	.87662	6.39621	-0.2410
16	0	1.820	.0000	879.4	1.693	.76229	4.96030	-1.6867	880.1	1.232	.77885	6.31833	-0.7788	905.7	1.482	.86914	6.34146	-0.1692
17	0	1.920	.0000	849.8	1.697	.74712	4.80673	-1.7202	850.5	1.201	.76464	6.26576	-0.7480	876.1	1.471	.86166	6.28669	-0.0974
18	0	2.020	.0000	820.2	1.701	.73195	4.65316	-1.7537	820.9	1.170	.75047	6.21319	-0.7172	846.5	1.460	.85418	6.23191	-0.0256
19	0	2.120	.0000	790.6	1.705	.71678	4.49959	-1.7872	791.3	1.139	.73629	6.16062	-0.6864	816.9	1.449	.84670	6.17714	.0462
20	0	2.220	.0000	761.0	1.709	.70161	4.34602	-1.8207	761.7	1.108	.72210	6.10805	-0.6556	787.3	1.438	.83922	6.12236	.1178
21	0	2.320	.0000	731.4	1.713	.68644	4.19245	-1.8542	732.1	1.077	.70793	6.05548	-0.6248	757.7	1.427	.83174	6.06761	.1894
22	180	.020	.025	1336.8	1.699	.99866	7.29129	-1.2196	1333.4	1.646	.98816	7.25137	-1.1880	1328.8	1.588	.99410	7.22509	-1.0914
23	180	.030	.050	1335.2	1.697	.99847	7.28257	-1.2682	1332.0	1.604	.98966	7.22161	-1.0691	1325.6	1.683	.99171	7.23326	-1.0914
24	180	.040	.075	1333.6	1.695	.99828	7.27385	-1.3168	1330.8	1.562	.99116	7.19185	-1.0482	1323.4	1.674	.98863	7.19840	-1.13724
25	180	.050	.100	1332.0	1.693	.99809	7.26512	-1.3654	1329.6	1.520	.99368	7.16209	-1.0273	1321.2	1.667	.98554	7.16509	-1.18509
26	180	.060	.125	1330.4	1.691	.99790	7.25639	-1.4140	1328.4	1.478	.99616	7.13238	-1.0064	1319.0	1.659	.98245	7.13226	-1.23284
27	180	.070	.150	1328.8	1.689	.99771	7.24766	-1.4626	1327.2	1.436	.99864	7.10267	-0.9855	1316.8	1.650	.97936	7.10044	-1.28068
28	180	.080	.175	1327.2	1.687	.99752	7.23893	-1.5112	1326.0	1.394	.99112	7.07296	-0.9646	1314.6	1.642	.97627	7.06768	-1.32852
29	180	.090	.200	1325.6	1.685	.99733	7.23020	-1.5598	1324.8	1.352	.98360	7.04325	-0.9437	1312.4	1.634	.97318	7.03844	-1.37636
30	180	.100	.225	1324.0	1.683	.99714	7.22147	-1.6084	1323.6	1.310	.97608	7.01354	-0.9228	1310.2	1.626	.97009	7.00968	-1.42420
31	180	.110	.250	1322.4	1.681	.99695	7.21274	-1.6570	1322.4	1.268	.96852	6.98383	-0.9019	1308.0	1.618	.96700	6.98100	-1.47204
32	180	.120	.275	1320.8	1.679	.99676	7.20401	-1.7056	1321.2	1.226	.96096	6.95412	-0.8810	1305.8	1.610	.96491	6.96310	-1.51988
33	180	.130	.300	1319.2	1.677	.99657	7.19528	-1.7542	1319.6	1.184	.95340	6.92441	-0.8601	1303.6	1.602	.96282	6.93338	-1.56772
34	180	.140	.325	1317.6	1.675	.99638	7.18655	-1.8028	1318.0	1.142	.94588	6.89470	-0.8392	1301.4	1.594	.96073	6.90366	-1.61556
35	180	.150	.350	1316.0	1.673	.99619	7.17782	-1.8514	1316.4	1.100	.93836	6.86500	-0.8183	1299.2	1.586	.95864	6.87394	-1.66340
36	180	.160	.375	1314.4	1.671	.99600	7.16909	-1.9000	1314.8	1.058	.93084	6.83529	-0.7974	1297.0	1.578	.95655	6.84422	-1.71124
37	180	.170	.400	1312.8	1.669	.99581	7.16036	-1.9486	1313.2	1.016	.92332	6.80558	-0.7765	1294.8	1.570	.95446	6.81450	-1.75908
38	180	.180	.425	1311.2	1.667	.99562	7.15163	-1.9972	1311.6	0.974	.91580	6.77587	-0.7556	1292.6	1.562	.95237	6.78478	-1.80692
39	180	.190	.450	1309.6	1.665	.99543	7.14290	-2.0458	1310.0	0.932	.90828	6.74616	-0.7347	1290.4	1.554	.95028	6.75506	-1.85476
40	180	.200	.475	1308.0	1.663	.99524	7.13417	-2.0944	1308.4	0.890	.90076	6.71645	-0.7138	1288.2	1.546	.94819	6.72535	-1.90260
41	180	.210	.500	1306.4	1.661	.99505	7.12544	-2.1430	1306.8	0.848	.89324	6.68674	-0.6929	1286.0	1.538	.94610	6.69564	-1.95044
42	270	.020	.025	1304.8	1.659	.99486	7.11671	-2.1916	1305.2	0.806	.88572	6.65703	-0.6720	1283.8	1.530	.94401	6.66594	-2.00000
43	270	.030	.050	1303.2	1.657	.99467	7.10798	-2.2402	1303.6	0.764	.87820	6.62732	-0.6511	1281.6	1.522	.94192	6.63623	-2.04964
44	270	.040	.075	1301.6	1.655	.99448	7.09925	-2.2888	1302.0	0.722	.87068	6.59761	-0.6302	1279.4	1.514	.93983	6.60652	-2.09928
45	270	.050	.100	1300.0	1.653	.99429	7.09052	-2.3374	1300.4	0.680	.86316	6.56790	-0.6093	1277.2	1.506	.93774	6.57682	-2.14892
46	270	.060	.125	1298.4	1.651	.99410	7.08179	-2.3860	1298.8	0.638	.85564	6.53819	-0.5884	1275.0	1.498	.93565	6.54714	-2.19856
47	270	.070	.150	1296.8	1.649	.99391	7.07306	-2.4346	1297.2	0.596	.84812	6.50848	-0.5675	1272.8	1.490	.93356	6.51746	-2.24820
48	270	.080	.175	1295.2	1.647	.99372	7.06433	-2.4832	1295.6	0.554	.84060	6.47877	-0.5466	1270.6	1.482	.93147	6.48778	-2.29784
49	270	.090	.200	1293.6	1.645	.99353	7.05560	-2.5318	1294.0	0.512	.83308	6.44906	-0.5257	1268.4	1.474	.92938	6.45809	-2.34748
50	270	.100	.225	1292.0	1.643	.99334	7.04687	-2.5804	1292.4	0.470	.82556	6.41935	-0.5048	1266.2	1.466	.92729	6.42840	-2.39712

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE 1.- DATA^a FOR 140° CONE; $M_{\infty} = 2.30$ - Continued

(b) $\alpha = 5^\circ$ - Concluded

Orifice ϕ , deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ$, $P_t = 2290.7$ psf					$\Phi = 90.0^\circ$, $P_t = 2291.3$ psf				
				P_t , psf	C_p	$P_t/P_{t,2}$	P_t/ρ_{∞}	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	P_t/ρ_{∞}	M_t
1	0	-0.210	-0.000	1317.5	1.672	.98625	7.19201	-1.4180	1320.7	1.676	.98818	7.20756	-1.3043
2	0	-0.230	-0.071	1307.9	1.658	.97888	7.10490	-1.37490	1314.3	1.667	.98340	7.17270	-1.5481
3	0	-0.250	-0.141	1298.2	1.644	.97151	7.01779	-1.33988	1307.9	1.657	.97801	7.13949	-1.6571
4	0	-0.260	-0.212	1288.6	1.630	.96414	6.93069	-1.30486	1299.8	1.647	.97256	7.10628	-1.7661
5	0	-0.270	-0.283	1279.0	1.618	.95678	6.84358	-1.26984	1291.8	1.637	.96706	7.07307	-1.8751
6	0	-0.280	-0.354	1269.4	1.606	.94942	6.75642	-1.23482	1283.8	1.627	.96154	7.03986	-1.9841
7	0	-0.290	-0.425	1259.8	1.594	.94206	6.66926	-1.19980	1275.8	1.617	.95602	7.00665	-2.0931
8	0	-0.300	-0.496	1250.2	1.582	.93470	6.58210	-1.16478	1267.8	1.607	.95050	6.97344	-2.2021
9	0	-0.310	-0.567	1240.6	1.570	.92734	6.49494	-1.12976	1259.8	1.597	.94498	6.94023	-2.3111
10	0	-0.320	-0.638	1231.0	1.558	.91998	6.40778	-1.09474	1251.8	1.587	.93946	6.90702	-2.4201
11	0	-0.330	-0.709	1221.4	1.546	.91262	6.32062	-1.05972	1243.8	1.577	.93394	6.87381	-2.5291
12	0	-0.340	-0.780	1211.8	1.534	.90526	6.23346	-1.02470	1235.8	1.567	.92842	6.84060	-2.6381
13	0	-0.350	-0.851	1202.2	1.522	.89790	6.14630	-98968	1227.8	1.557	.92290	6.80739	-2.7471
14	0	-0.360	-0.922	1192.6	1.510	.89054	6.05914	-95466	1219.8	1.547	.91738	6.77418	-2.8561
15	0	-0.370	-0.993	1183.0	1.498	.88318	5.97198	-91964	1211.8	1.537	.91186	6.74097	-2.9651
16	0	-0.380	-1.064	1173.4	1.486	.87582	5.88482	-88462	1203.8	1.527	.90634	6.70776	-3.0741
17	0	-0.390	-1.135	1163.8	1.474	.86846	5.79766	-84960	1195.8	1.517	.90082	6.67455	-3.1831
18	0	-0.400	-1.206	1154.2	1.462	.86110	5.71050	-81458	1187.8	1.507	.89530	6.64134	-3.2921
19	0	-0.410	-1.277	1144.6	1.450	.85374	5.62334	-77956	1179.8	1.497	.88978	6.60813	-3.4011
20	0	-0.420	-1.348	1135.0	1.438	.84638	5.53618	-74454	1171.8	1.487	.88426	6.57492	-3.5101
21	0	-0.430	-1.419	1125.4	1.426	.83902	5.44902	-70952	1163.8	1.477	.87874	6.54171	-3.6191
22	0	-0.440	-1.490	1115.8	1.414	.83166	5.36186	-67450	1155.8	1.467	.87322	6.50850	-3.7281
23	0	-0.450	-1.561	1106.2	1.402	.82430	5.27470	-63948	1147.8	1.457	.86770	6.47529	-3.8371
24	0	-0.460	-1.632	1096.6	1.390	.81694	5.18754	-60446	1139.8	1.447	.86218	6.44208	-3.9461
25	0	-0.470	-1.703	1087.0	1.378	.80958	5.10038	-56944	1131.8	1.437	.85666	6.40887	-4.0551
26	0	-0.480	-1.774	1077.4	1.366	.80222	5.01322	-53442	1123.8	1.427	.85114	6.37566	-4.1641
27	0	-0.490	-1.845	1067.8	1.354	.79486	4.92606	-49940	1115.8	1.417	.84562	6.34245	-4.2731
28	0	-0.500	-1.916	1058.2	1.342	.78750	4.83890	-46438	1107.8	1.407	.84010	6.30924	-4.3821
29	0	-0.510	-1.987	1048.6	1.330	.78014	4.75174	-42936	1099.8	1.397	.83458	6.27603	-4.4911
30	0	-0.520	-2.058	1039.0	1.318	.77278	4.66458	-39434	1091.8	1.387	.82906	6.24282	-4.6001
31	0	-0.530	-2.129	1029.4	1.306	.76542	4.57742	-35932	1083.8	1.377	.82354	6.20961	-4.7091
32	0	-0.540	-2.200	1019.8	1.294	.75806	4.49026	-32430	1075.8	1.367	.81802	6.17640	-4.8181
33	0	-0.550	-2.271	1010.2	1.282	.75070	4.40310	-28928	1067.8	1.357	.81250	6.14319	-4.9271
34	0	-0.560	-2.342	1000.6	1.270	.74334	4.31594	-25426	1059.8	1.347	.80698	6.11000	-5.0361
35	0	-0.570	-2.413	991.0	1.258	.73598	4.22878	-21924	1051.8	1.337	.80146	6.07679	-5.1451
36	0	-0.580	-2.484	981.4	1.246	.72862	4.14162	-18422	1043.8	1.327	.79594	6.04358	-5.2541
37	0	-0.590	-2.555	971.8	1.234	.72126	4.05446	-14920	1035.8	1.317	.79042	6.01037	-5.3631
38	0	-0.600	-2.626	962.2	1.222	.71390	3.96730	-11418	1027.8	1.307	.78490	5.97716	-5.4721
39	0	-0.610	-2.697	952.6	1.210	.70654	3.88014	-7916	1019.8	1.297	.77938	5.94395	-5.5811
40	0	-0.620	-2.768	943.0	1.198	.69918	3.79298	-4414	1011.8	1.287	.77386	5.91074	-5.6901
41	0	-0.630	-2.839	933.4	1.186	.69182	3.70582	-912	1003.8	1.277	.76834	5.87753	-5.7991
42	0	-0.640	-2.910	923.8	1.174	.68446	3.61866	338	995.8	1.267	.76282	5.84432	-5.9081
43	0	-0.650	-2.981	914.2	1.162	.67710	3.53150	688	987.8	1.257	.75730	5.81111	-6.0171
44	0	-0.660	-3.052	904.6	1.150	.66974	3.44434	1186	979.8	1.247	.75178	5.77790	-6.1261
45	0	-0.670	-3.123	895.0	1.138	.66238	3.35718	1684	971.8	1.237	.74626	5.74469	-6.2351
46	0	-0.680	-3.194	885.4	1.126	.65502	3.27002	2182	963.8	1.227	.74074	5.71148	-6.3441
47	0	-0.690	-3.265	875.8	1.114	.64766	3.18286	2680	955.8	1.217	.73522	5.67827	-6.4531
48	0	-0.700	-3.336	866.2	1.102	.64030	3.09570	3178	947.8	1.207	.72970	5.64506	-6.5621
49	0	-0.710	-3.407	856.6	1.090	.63294	3.00854	3676	939.8	1.197	.72418	5.61185	-6.6711
50	0	-0.720	-3.478	847.0	1.078	.62558	2.92138	4174	931.8	1.187	.71866	5.57864	-6.7801

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE 1.- DATA^a FOR 140° CONE; $M_{\infty} = 2.30$ - Continued(c) $\alpha = 10^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ, p_t = 2293.8 \text{ psf}$					$\Phi = 22.5^\circ, p_t = 2290.8 \text{ psf}$					$\Phi = 45.0^\circ, p_t = 2291.6 \text{ psf}$				
				p_t , psf	C_p	$p_t/\rho_{t,2}$	p_t/ρ_{∞}	M_t	p_t , psf	C_p	$p_t/\rho_{t,2}$	p_t/ρ_{∞}	M_t	p_t , psf	C_p	$p_t/\rho_{t,2}$	p_t/ρ_{∞}	M_t
1	0	.330	.0000	1292.5	1.618	.95853	6.99125	24674	1280.7	1.618	.95845	6.99073	24956	1279.3	1.615	.95706	6.98953	25119
2	0	.200	.0025	1247.3	1.566	.93227	6.78971	31813	1248.6	1.571	.93053	6.79000	32139	1245.7	1.566	.93197	6.78957	30697
3	0	.130	.0050	1244.2	1.590	.92916	6.71872	33815	1215.9	1.552	.91055	6.76618	33571	1233.4	1.566	.92719	6.77552	31887
4	0	.100	.0075	1240.0	1.618	.92586	6.64786	35821	1183.2	1.535	.88745	6.74186	35477	1201.7	1.566	.92419	6.76266	33042
5	0	.070	.0100	1235.8	1.650	.92246	6.57702	37830	1150.5	1.519	.86455	6.71756	37330	1170.0	1.566	.92241	6.74780	34165
6	0	.330	.0125	1231.5	1.682	.91916	6.50639	39840	1117.8	1.504	.84165	6.69326	39285	1137.3	1.517	.91763	6.72353	35350
7	0	1.200	.2859	1227.2	1.713	.91586	6.43576	41850	1085.1	1.489	.81875	6.66896	41240	1104.6	1.517	.89463	6.69920	36535
8	0	1.530	.3300	1223.0	1.744	.91256	6.36512	43860	1052.4	1.474	.79584	6.64466	43195	1071.9	1.504	.87172	6.67494	37720
9	0	1.860	.3750	1218.7	1.775	.90926	6.29448	45870	1019.7	1.459	.77293	6.62036	45150	1039.2	1.489	.84881	6.65068	38905
10	0	1.930	.2225	1214.5	1.806	.90596	6.22384	47880	987.0	1.444	.75002	6.59606	47105	1006.5	1.474	.82590	6.62640	40090
11	0	2.260	.4715	1199.5	1.937	.88661	6.32086	44102	1173.6	1.474	.88546	6.60589	42051	1194.6	1.490	.89373	6.61865	40386
12	0	2.590	.5186	1184.3	1.968	.88331	6.25022	46112	1140.9	1.459	.86251	6.58169	43962	1161.9	1.474	.87103	6.60140	42071
13	0	2.920	.5658	1169.1	1.999	.88001	6.17958	48122	1108.2	1.444	.83960	6.55749	45873	1129.2	1.459	.84833	6.58364	43756
14	0	2.630	.3255	1164.9	2.030	.87671	6.10894	50132	1075.5	1.429	.81669	6.53329	47784	1096.5	1.444	.82536	6.56589	45441
15	0	3.300	.3775	1150.6	2.061	.87341	6.03830	52142	1042.8	1.414	.79378	6.50909	49695	1063.8	1.429	.80209	6.54814	47126
16	0	3.630	.4245	1136.4	2.092	.87011	5.96766	54152	1010.1	1.399	.77087	6.48489	51606	1031.1	1.414	.77982	6.53039	48811
17	0	3.960	.4714	1122.2	2.123	.86681	5.89692	56162	977.4	1.384	.74796	6.46069	53517	1008.4	1.399	.75775	6.51264	50496
18	0	4.290	.5183	1108.0	2.154	.86351	5.82618	58172	944.7	1.369	.72505	6.43649	55428	975.7	1.384	.73568	6.49491	52181
19	0	4.620	.5652	1093.8	2.185	.86021	5.75544	60182	912.0	1.354	.70214	6.41229	57339	943.0	1.369	.71371	6.47716	53866
20	0	4.950	.6121	1079.6	2.216	.85691	5.68470	62192	879.3	1.339	.67923	6.38809	59250	910.3	1.354	.69474	6.45941	55551
21	0	5.280	.6590	1065.4	2.247	.85361	5.61396	64202	846.6	1.324	.65632	6.36389	61161	877.6	1.339	.67226	6.44166	57236
22	0	4.300	.5003	921.5	1.037	.68875	5.02360	74972	919.4	1.085	.68803	5.01831	75094	930.2	1.189	.74079	5.60316	62349
23	0	4.630	.5472	907.3	1.068	.68545	4.95286	76982	886.7	1.070	.68473	4.99353	77116	907.0	1.174	.73648	5.57987	60962
24	0	4.960	.5941	893.0	1.099	.68215	4.88212	78992	854.0	1.055	.68143	4.96923	79238	874.3	1.159	.73219	5.55658	59577
25	0	5.290	.6410	878.7	1.130	.67885	4.81138	80992	821.3	1.040	.67811	4.94493	81360	841.6	1.144	.72790	5.53329	58192
26	0	5.620	.6879	864.5	1.161	.67555	4.74064	82992	788.6	1.025	.67480	4.92063	83482	808.9	1.129	.72361	5.51000	56807
27	0	1.000	.125	1331.4	1.700	.98921	7.25997	30000	1330.4	1.691	.99564	7.26194	30706	1311.1	1.662	.98085	7.14405	16644
28	0	1.200	.150	1336.8	1.698	.98911	7.28727	30354	1328.8	1.689	.99444	7.26194	30706	1312.7	1.664	.98204	7.14278	16110
29	0	1.400	.175	1342.2	1.696	.98902	7.27456	30708	1326.6	1.687	.99377	7.24222	30925	1310.5	1.660	.97955	7.14153	15583
30	0	1.600	.200	1347.6	1.694	.98893	7.26185	31062	1324.4	1.685	.99300	7.22222	31146	1298.3	1.632	.97626	7.08808	14958
31	0	1.800	.225	1353.0	1.692	.98884	7.24914	31416	1322.2	1.683	.99223	7.20222	31367	1286.1	1.617	.97497	7.06880	14333
32	0	2.000	.250	1358.0	1.690	.98875	7.23643	31770	1320.0	1.681	.99146	7.18222	31588	1273.9	1.602	.97368	7.04952	13708
33	0	2.200	.275	1363.0	1.688	.98866	7.22372	32124	1317.8	1.679	.99069	7.16222	31809	1261.7	1.587	.97239	7.03024	13083
34	0	2.400	.300	1368.0	1.686	.98857	7.21101	32478	1315.6	1.677	.98990	7.14222	32030	1249.5	1.572	.97110	7.01096	12458
35	0	2.600	.325	1373.0	1.684	.98848	7.19830	32832	1313.4	1.675	.98911	7.12222	32251	1237.3	1.557	.96981	6.99168	11833
36	0	2.800	.350	1378.0	1.682	.98839	7.18559	33186	1311.2	1.673	.98832	7.10222	32472	1225.1	1.542	.96852	6.97240	11208
37	0	3.000	.375	1383.0	1.680	.98830	7.17288	33540	1309.0	1.671	.98753	7.08222	32693	1212.9	1.527	.96723	6.95312	10583
38	0	3.200	.400	1388.0	1.678	.98821	7.16017	33894	1306.8	1.669	.98674	7.06222	32914	1200.7	1.512	.96594	6.93384	9958
39	0	3.400	.425	1393.0	1.676	.98812	7.14746	34248	1304.6	1.667	.98595	7.04222	33135	1188.5	1.497	.96465	6.91456	9333
40	0	3.600	.450	1398.0	1.674	.98803	7.13475	34602	1302.4	1.665	.98516	7.02222	33356	1176.3	1.482	.96336	6.89528	8708
41	0	3.800	.475	1403.0	1.672	.98794	7.12204	34956	1300.2	1.663	.98437	7.00222	33577	1164.1	1.467	.96207	6.87600	8083
42	0	4.000	.500	1408.0	1.670	.98785	7.10933	35310	1298.0	1.661	.98358	6.98222	33798	1151.9	1.452	.96078	6.85672	7458
43	0	4.200	.525	1413.0	1.668	.98776	7.09662	35664	1295.8	1.659	.98279	6.96222	34019	1139.7	1.437	.95949	6.83744	6833
44	0	4.400	.550	1418.0	1.666	.98767	7.08391	36018	1293.6	1.657	.98199	6.94222	34240	1127.5	1.422	.95820	6.81816	6208
45	0	4.600	.575	1423.0	1.664	.98758	7.07120	36372	1291.4	1.655	.98120	6.92222	34461	1115.3	1.407	.95691	6.79888	5583
46	0	4.800	.600	1428.0	1.662	.98749	7.05849	36726	1289.2	1.653	.98041	6.90222	34682	1103.1	1.392	.95562	6.77960	4958
47	0	5.000	.625	1433.0	1.660	.98740	7.04578	37080	1287.0	1.651	.97962	6.88222	34903	1090.9	1.377	.95433	6.76032	4333
48	0	5.200	.650	1438.0	1.658	.98731	7.03307	37434	1284.8	1.649	.97883	6.86222	35124	1078.7	1.362	.95304	6.74104	3708
49	0	5.400	.675	1443.0	1.656	.98722	7.02036	37788	1282.6	1.647	.97804	6.84222	35345	1066.5	1.347	.95175	6.72176	3083
50	0	5.600	.700	1448.0	1.654	.98713	7.00765	38142	1280.4	1.645	.97725	6.82222	35566	1054.3	1.332	.95046	6.70248	2458

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE 1.- DATA^a FOR 140° CONE; $M_{\infty} = 2.30$ - Continued

(c) $\alpha = 10^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ$, $P_t = 2289.6$ psf					$\phi = 90.0^\circ$, $P_t = 2283.0$ psf				
				$P_{t, \text{psf}}$	C_p	$P_t/P_{t,2}$	$P_t/\rho\infty$	M_t	$P_{t, \text{psf}}$	C_p	$P_t/P_{t,2}$	$P_t/\rho\infty$	M_t
1	0	-0.00	-0.000	1277.7	1.614	95570	6.97791	25227	1274.6	1.615	95713	6.98110	25096
2	0	-0.25	-0.471	1261.7	1.591	94474	6.89068	28614	1269.8	1.608	95154	6.99410	26158
3	0	-0.50	-0.943	1255.9	1.584	94115	6.82363	29564	1265.6	1.603	95114	6.93741	26945
4	0	-0.75	-1.415	1250.2	1.574	93158	6.72764	30792	1266.6	1.603	95114	6.93741	26946
5	0	-1.00	-1.886	1244.2	1.565	92680	6.79474	31980	1261.8	1.596	94455	6.91200	27849
6	0	-1.25	-2.357	1237.8	1.555	92382	6.75985	33134	1257.0	1.589	94366	6.88496	28823
7	0	-1.50	-2.829	1229.8	1.544	91395	6.71624	34531	1250.7	1.580	93917	6.85004	30078
8	0	-1.75	-3.300	1220.2	1.510	90365	6.62059	37461	1255.9	1.573	93557	6.82383	33092
9	0	-2.00	-3.772	1212.2	1.508	90267	6.56795	39897	1247.9	1.567	93166	6.78014	32467
10	0	-2.25	-4.243	1202.6	1.504	90049	6.51997	41967	1228.3	1.547	92339	6.72772	34168
11	0	-2.50	-4.715	1193.0	1.490	89332	6.45562	44071	1218.8	1.513	91521	6.67529	35904
12	0	-2.75	-5.186	1180.3	1.471	88375	6.41494	46291	1209.2	1.518	90802	6.62287	37384
13	0	-3.00	-5.658	1169.1	1.454	87538	6.38478	48480	1199.6	1.504	90093	6.57045	38916
14	0	-3.25	-6.130	1158.3	1.435	86841	6.35388	50741	1190.9	1.492	89762	6.50055	40881
15	0	-3.50	-6.601	1148.3	1.412	86335	6.32778	52952	1170.9	1.462	88729	6.44584	42953
16	0	-3.75	-7.072	1139.3	1.388	84189	6.14066	56146	1154.9	1.438	86729	6.32580	45263
17	0	-4.00	-7.544	1126.4	1.358	82635	6.02717	59200	1134.2	1.408	85172	6.21222	48438
18	0	-4.25	-8.015	1109.6	1.322	80841	5.89633	62531	1111.9	1.375	83495	6.08989	51425
19	0	-4.50	-8.486	1094.6	1.280	78589	5.75217	65431	1081.6	1.330	81219	5.92389	55334
20	0	-4.75	-8.958	1081.0	1.221	75899	5.59130	68431	1051.6	1.280	78589	5.75217	59291
21	0	-5.00	-9.430	948.7	1.129	71035	5.18110	74735	977.9	1.176	75332	5.55596	67612
22	180	-0.25	-0.471	1291.9	1.635	96734	7.05552	21832	1276.0	1.617	95820	6.98885	24774
23	180	-0.50	-0.943	1291.9	1.635	96734	7.05552	21832	1269.6	1.608	95340	6.95386	26199
24	180	-0.75	-1.415	1284.9	1.614	95614	7.00276	23029	1269.6	1.608	95340	6.95386	26199
25	180	-1.00	-1.886	1290.3	1.633	96514	7.05292	23029	1258.4	1.591	94501	6.89263	28552
26	180	-1.25	-2.357	1287.1	1.628	96375	7.02932	23766	1253.6	1.584	94141	6.86639	29457
27	180	-1.50	-2.829	1283.9	1.624	96135	7.01166	25624	1247.3	1.575	93661	6.83140	30730
28	180	-1.75	-3.300	1275.9	1.612	95537	6.96820	26824	1237.7	1.575	93661	6.83140	30730
29	180	-2.00	-3.771	1265.9	1.600	94848	6.91468	28910	1231.7	1.575	93661	6.83140	30730
30	180	-2.25	-4.243	1255.1	1.581	93980	6.85468	29910	1221.7	1.575	93661	6.83140	30730
31	180	-2.50	-4.715	1247.1	1.569	93392	6.81102	31430	1212.1	1.523	91023	6.63897	33005
32	180	-2.75	-5.186	1247.1	1.553	92544	6.74989	33457	1200.9	1.506	90183	6.57774	36705
33	180	-3.00	-5.658	1235.9	1.533	91706	6.68877	35389	1189.8	1.490	89344	6.51651	40446
34	180	-3.25	-6.130	1228.7	1.516	91031	6.63841	37461	1174.9	1.468	88341	6.44584	42953
35	180	-3.50	-6.601	1218.8	1.494	89551	6.58159	40022	1157.8	1.468	88341	6.44584	42953
36	180	-3.75	-7.072	1195.0	1.468	88234	6.53554	42669	1138.7	1.414	85506	6.23660	47830
37	180	-4.00	-7.544	1178.4	1.468	88234	6.53554	42669	1138.7	1.414	85506	6.23660	47830
38	180	-4.25	-8.015	1156.4	1.433	86438	6.30456	46109	1114.7	1.379	83707	6.10540	51952
39	180	-4.50	-8.486	1145.4	1.433	86438	6.30456	46109	1114.7	1.379	83707	6.10540	51952
40	180	-4.75	-8.958	1136.2	1.412	85283	6.25738	50034	1086.0	1.336	81549	5.94795	56776
41	180	-5.00	-9.430	1121.7	1.397	84579	6.21468	53034	1065.4	1.280	78570	5.79880	59560
42	270	-1.25	-2.357	1333.5	1.597	98946	7.28255	14685	1336.7	1.707	1.00377	7.32121	90000
43	270	-1.50	-2.829	1315.9	1.571	98530	7.14650	14563	1319.1	1.681	99058	7.22520	11638
44	270	-1.75	-3.300	1298.1	1.543	98159	6.98549	16230	1271.2	1.610	99460	6.96261	15849
45	270	-2.00	-3.771	1283.9	1.522	97694	6.89834	18030	1250.8	1.521	99058	6.96261	15849
46	90	-1.25	-2.357	1215.4	1.522	91006	6.67773	26927	1210.8	1.421	86849	6.39454	45137
47	90	-1.50	-2.829	1161.1	1.442	86940	6.34117	35165	1155.5	1.441	86849	6.39454	45137
48	90	-1.75	-3.300	1087.6	1.334	81439	5.93994	45962	1083.2	1.332	81338	5.93262	55137
49	90	-2.00	-3.771	923.1	1.091	69121	5.04154	74594	918.9	1.089	69000	5.03268	74780

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE I.- DATA^a FOR 140° CONE; $M_{\infty} = 2.30$ - Continued(d) $\alpha = 15^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\phi = 0.0^\circ, P_t = 2290.5 \text{ psf}$			
				P_t , psf	C_p	$P_t/P_{t,2}$	M_L
1	0	.230	.0000	115.4	1.522	.99070	.17020
2	0	.230	.0025	109.71	1.446	.87155	.44776
3	0	.230	.0050	.0943	1.458	.87742	.43628
4	0	.230	.0075	.1414	1.456	.87623	.43859
5	0	.230	.0100	.1886	1.446	.87145	.44776
6	0	.230	.0125	.2359	1.431	.85951	.47675
7	0	.230	.0150	.2829	1.416	.85591	.47675
8	0	.230	.0175	.3300	1.399	.84754	.49192
9	0	.230	.0200	.3772	1.383	.83917	.50842
10	0	.230	.0225	.4243	1.368	.83080	.52118
11	0	.230	.0250	.4714	1.353	.82243	.53444
12	0	.230	.0275	.5186	1.338	.81406	.54770
13	0	.230	.0300	.5658	1.323	.80569	.56096
14	0	.230	.0325	.6129	1.308	.79732	.57422
15	0	.230	.0350	.6601	1.293	.78895	.58748
16	0	.230	.0375	.7072	1.278	.78058	.60074
17	0	.230	.0400	.7544	1.263	.77221	.61400
18	0	.230	.0425	.8015	1.248	.76384	.62726
19	0	.230	.0450	.8487	1.233	.75547	.64052
20	0	.230	.0475	.8958	1.218	.74710	.65378
21	0	.230	.0500	.9429	1.203	.73873	.66704
22	180	.420	.0250	.0471	1.272	.95250	.26431
23	180	.420	.0500	.0943	1.306	.97773	.17967
24	180	.420	.0750	.1414	1.322	.98970	.12173
25	180	.420	.1000	.1886	1.338	.99927	.08339
26	180	.420	.1250	.2359	1.354	1.00406	.04505
27	180	.420	.1500	.2829	1.369	1.00557	.00000
28	180	.420	.1750	.3300	1.385	1.00608	.00000
29	180	.420	.2000	.3772	1.400	1.00659	.00000
30	180	.420	.2250	.4243	1.416	1.00710	.00000
31	180	.420	.2500	.4714	1.431	1.00761	.00000
32	180	.420	.2750	.5186	1.446	1.00812	.00000
33	180	.420	.3000	.5658	1.461	1.00863	.00000
34	180	.420	.3250	.6129	1.477	1.00914	.00000
35	180	.420	.3500	.6601	1.492	1.00965	.00000
36	180	.420	.3750	.7072	1.508	1.01016	.00000
37	180	.420	.4000	.7544	1.523	1.01067	.00000
38	180	.420	.4250	.8015	1.539	1.01118	.00000
39	180	.420	.4500	.8487	1.554	1.01169	.00000
40	180	.420	.4750	.8958	1.570	1.01220	.00000
41	180	.420	.5000	.9429	1.585	1.01271	.00000
42	180	.420	.5250	.9900	1.601	1.01322	.00000
43	270	.230	.0250	.0471	1.272	.95250	.26431
44	270	.230	.0500	.0943	1.306	.97773	.17967
45	270	.230	.0750	.1414	1.322	.98970	.12173
46	270	.230	.1000	.1886	1.338	.99927	.08339
47	270	.230	.1250	.2359	1.354	1.00406	.04505
48	270	.230	.1500	.2829	1.369	1.00557	.00000
49	270	.230	.1750	.3300	1.385	1.00608	.00000
50	270	.230	.2000	.3772	1.400	1.00659	.00000
51	270	.230	.2250	.4243	1.416	1.00710	.00000
52	270	.230	.2500	.4714	1.431	1.00761	.00000
53	270	.230	.2750	.5186	1.446	1.00812	.00000
54	270	.230	.3000	.5658	1.461	1.00863	.00000
55	270	.230	.3250	.6129	1.477	1.00914	.00000
56	270	.230	.3500	.6601	1.492	1.00965	.00000
57	270	.230	.3750	.7072	1.508	1.01016	.00000
58	270	.230	.4000	.7544	1.523	1.01067	.00000
59	270	.230	.4250	.8015	1.539	1.01118	.00000
60	270	.230	.4500	.8487	1.554	1.01169	.00000
61	270	.230	.4750	.8958	1.570	1.01220	.00000
62	270	.230	.5000	.9429	1.585	1.01271	.00000
63	270	.230	.5250	.9900	1.601	1.01322	.00000
64	270	.230	.5500	.1043	1.616	1.01373	.00000
65	270	.230	.5750	.1186	1.631	1.01424	.00000
66	270	.230	.6000	.1329	1.646	1.01475	.00000
67	270	.230	.6250	.1472	1.661	1.01526	.00000
68	270	.230	.6500	.1615	1.676	1.01577	.00000
69	270	.230	.6750	.1758	1.691	1.01628	.00000
70	270	.230	.7000	.1901	1.706	1.01679	.00000
71	270	.230	.7250	.2044	1.721	1.01730	.00000
72	270	.230	.7500	.2187	1.736	1.01781	.00000
73	270	.230	.7750	.2330	1.751	1.01832	.00000
74	270	.230	.8000	.2473	1.766	1.01883	.00000
75	270	.230	.8250	.2616	1.781	1.01934	.00000
76	270	.230	.8500	.2759	1.796	1.01985	.00000
77	270	.230	.8750	.2902	1.811	1.02036	.00000
78	270	.230	.9000	.3045	1.826	1.02087	.00000
79	270	.230	.9250	.3188	1.841	1.02138	.00000
80	270	.230	.9500	.3331	1.856	1.02189	.00000
81	270	.230	.9750	.3474	1.871	1.02240	.00000
82	270	.230	.1000	.3617	1.886	1.02291	.00000
83	270	.230	.1025	.3760	1.901	1.02342	.00000
84	270	.230	.1050	.3903	1.916	1.02393	.00000
85	270	.230	.1075	.4046	1.931	1.02444	.00000
86	270	.230	.1100	.4189	1.946	1.02495	.00000
87	270	.230	.1125	.4332	1.961	1.02546	.00000
88	270	.230	.1150	.4475	1.976	1.02597	.00000
89	270	.230	.1175	.4618	1.991	1.02648	.00000
90	270	.230	.1200	.4761	2.006	1.02699	.00000
91	270	.230	.1225	.4904	2.021	1.02750	.00000
92	270	.230	.1250	.5047	2.036	1.02801	.00000
93	270	.230	.1275	.5190	2.051	1.02852	.00000
94	270	.230	.1300	.5333	2.066	1.02903	.00000
95	270	.230	.1325	.5476	2.081	1.02954	.00000
96	270	.230	.1350	.5619	2.096	1.03005	.00000
97	270	.230	.1375	.5762	2.111	1.03056	.00000
98	270	.230	.1400	.5905	2.126	1.03107	.00000
99	270	.230	.1425	.6048	2.141	1.03158	.00000
100	270	.230	.1450	.6191	2.156	1.03209	.00000
101	270	.230	.1475	.6334	2.171	1.03260	.00000
102	270	.230	.1500	.6477	2.186	1.03311	.00000
103	270	.230	.1525	.6620	2.201	1.03362	.00000
104	270	.230	.1550	.6763	2.216	1.03413	.00000
105	270	.230	.1575	.6906	2.231	1.03464	.00000
106	270	.230	.1600	.7049	2.246	1.03515	.00000
107	270	.230	.1625	.7192	2.261	1.03566	.00000
108	270	.230	.1650	.7335	2.276	1.03617	.00000
109	270	.230	.1675	.7478	2.291	1.03668	.00000
110	270	.230	.1700	.7621	2.306	1.03719	.00000
111	270	.230	.1725	.7764	2.321	1.03770	.00000
112	270	.230	.1750	.7907	2.336	1.03821	.00000
113	270	.230	.1775	.8050	2.351	1.03872	.00000
114	270	.230	.1800	.8193	2.366	1.03923	.00000
115	270	.230	.1825	.8336	2.381	1.03974	.00000
116	270	.230	.1850	.8479	2.396	1.04025	.00000
117	270	.230	.1875	.8622	2.411	1.04076	.00000
118	270	.230	.1900	.8765	2.426	1.04127	.00000
119	270	.230	.1925	.8908	2.441	1.04178	.00000
120	270	.230	.1950	.9051	2.456	1.04229	.00000
121	270	.230	.1975	.9194	2.471	1.04280	.00000
122	270	.230	.2000	.9337	2.486	1.04331	.00000
123	270	.230	.2025	.9480	2.501	1.04382	.00000
124	270	.230	.2050	.9623	2.516	1.04433	.00000
125	270	.230	.2075	.9766	2.531	1.04484	.00000
126	270	.230	.2100	.9909	2.546	1.04535	.00000
127	270	.230	.2125	.1000	2.561	1.04586	.00000
128	270	.230	.2150	.1091	2.576	1.04637	.00000
129	270	.230	.2175	.1182	2.591	1.04688	.00000
130	270	.230	.2200	.1273	2.606	1.04739	.00000
131	270	.230	.2225	.1364	2.621	1.04790	.00000
132	270	.230	.2250	.1455	2.636	1.04841	.00000
133	270	.230	.2275	.1546	2.651	1.04892	.00000
134	270	.230	.2300	.1637	2.666	1.04943	.00000
135	270	.230	.2325	.1728	2.681	1.04994	.00000
136	270	.230	.2350	.1819	2.696	1.05045	.00000
137	270	.230	.2375	.1910	2.711	1.05096	.00000
138	270	.230	.2400	.2001	2.726	1.05147	.00000
139	270	.230	.2425	.2092	2.741	1.05198	.00000
140	270	.230	.2450	.2183	2.756	1.05249	.00000
141	270	.230	.2475	.2274	2.771	1.05300	.00000
142	270	.230	.2500	.2365	2.786	1.05351	.00000
143	270	.230	.2525	.2456	2.801	1.05402	.00000
144	270	.230	.2550	.2547	2.816	1.05453	.00000
145	270	.230	.2575	.2638	2.831	1.05504	.00000
146	270	.230	.2600	.2729	2.846	1.05555	.00000
147	270	.230	.2625	.2820	2.861	1.05606	.00000
148	270	.230	.2650	.2911	2.876	1.05657	.00000
149	270	.230	.2675	.3002	2.891	1.05708	.00000
150	270	.230	.2700	.3093	2.906	1.05759	.00000
151	270	.230	.2725	.3184	2.921	1.05810	.00000
152	270	.230	.2750	.3275	2.936	1.05861	.00000
153	270	.230	.2775	.3366	2.951	1.05912	.00000
154	270	.230	.2800	.3457	2.966	1.05963	.00000

TABLE 1.- DATA^a FOR 140° CONE; $M_{\infty} = 2.30$ - Continued

(e) $\alpha = 20^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0.0^\circ, P_t = 2289.9 \text{ psf}$				$\Phi = 22.5^\circ, P_t = 2290.3 \text{ psf}$				$\Phi = 45.0^\circ, P_t = 2290.3 \text{ psf}$						
				P_t , psf	C_p	$P_t/P_{t,2}$	P_t/ρ_∞	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	P_t/ρ_∞	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	P_t/ρ_∞	M_t
1	0	.030	.0000	1156.5	1.378	.83673	6.10292	.51112	1115.7	1.376	.83593	6.09704	.51253	1115.4	1.376	.83566	6.09508	5.1300
2	0	.030	.0025	1094.5	1.291	.81160	5.77988	.55620	1059.3	1.292	.81294	5.78347	.58539	1059.5	1.322	.80816	5.78407	5.1407
3	0	.030	.0050	1084.3	1.329	.81160	5.91957	.55434	1078.5	1.320	.81274	5.92233	.58539	1084.4	1.322	.80816	5.92453	5.1407
4	0	.030	.0075	1073.6	1.343	.81160	6.06188	.55300	1093.0	1.329	.81274	6.10500	.58539	1094.4	1.326	.81155	6.10697	5.1407
5	0	.030	.0100	1067.7	1.319	.80681	5.93703	.55238	1082.0	1.322	.80686	5.96195	.58539	1082.8	1.326	.81055	5.96269	5.1407
6	0	.030	.0125	1061.1	1.319	.79962	5.88465	.55168	1071.7	1.313	.80368	5.92381	.58539	1078.1	1.319	.80897	5.92509	5.1407
7	0	.030	.0150	1054.1	1.293	.79364	5.83226	.55096	1061.1	1.301	.79771	5.88183	.58539	1071.9	1.310	.80680	5.92727	5.1407
8	0	.030	.0175	1047.1	1.281	.78764	5.78001	.55024	1051.1	1.294	.79176	5.83021	.58539	1058.9	1.291	.80427	5.83245	5.1407
9	0	.030	.0200	1040.1	1.269	.78164	5.72736	.54952	1041.1	1.278	.78577	5.77931	.58539	1048.9	1.291	.80247	5.78117	5.1407
10	0	.030	.0225	1033.1	1.257	.77564	5.67469	.54880	1031.1	1.264	.77981	5.72785	.58539	1038.9	1.282	.80068	5.78384	5.1407
11	0	.030	.0250	1026.1	1.245	.76964	5.62206	.54808	1021.0	1.249	.77444	5.67669	.58539	1028.9	1.282	.80068	5.78595	5.1407
12	0	.030	.0275	1019.1	1.233	.76364	5.56943	.54736	1011.1	1.235	.76848	5.62443	.58539	1018.9	1.258	.80068	5.78807	5.1407
13	0	.030	.0300	1012.1	1.221	.75764	5.51680	.54664	1001.1	1.225	.76352	5.57243	.58539	1013.9	1.252	.80068	5.79019	5.1407
14	0	.030	.0325	1005.1	1.209	.75164	5.46417	.54592	991.1	1.214	.75846	5.52049	.58539	1008.9	1.225	.80068	5.79231	5.1407
15	0	.030	.0350	998.1	1.197	.74564	5.41154	.54520	981.1	1.202	.75240	5.46865	.58539	996.9	1.213	.80068	5.79443	5.1407
16	0	.030	.0375	991.1	1.185	.73964	5.35891	.54448	971.1	1.192	.74636	5.41619	.58539	989.9	1.206	.80068	5.79655	5.1407
17	0	.030	.0400	984.1	1.173	.73364	5.30628	.54376	961.1	1.182	.74030	5.36372	.58539	981.9	1.195	.80068	5.79867	5.1407
18	0	.030	.0425	977.1	1.161	.72764	5.25365	.54304	951.1	1.170	.73424	5.31126	.58539	973.9	1.185	.80068	5.80079	5.1407
19	0	.030	.0450	970.1	1.149	.72164	5.20102	.54232	941.1	1.158	.72818	5.25879	.58539	966.9	1.175	.80068	5.80291	5.1407
20	0	.030	.0475	963.1	1.137	.71564	5.14839	.54160	931.1	1.146	.72212	5.20633	.58539	959.9	1.165	.80068	5.80503	5.1407
21	0	.030	.0500	956.1	1.125	.70964	5.09576	.54088	921.1	1.134	.71606	5.15387	.58539	952.9	1.153	.80068	5.80715	5.1407
22	0	.030	.0525	949.1	1.113	.70364	5.04313	.54016	911.1	1.122	.71000	5.10141	.58539	945.9	1.141	.80068	5.80927	5.1407
23	0	.030	.0550	942.1	1.101	.69764	4.99050	.53944	901.1	1.110	.70394	5.04895	.58539	938.9	1.129	.80068	5.81139	5.1407
24	0	.030	.0575	935.1	1.089	.69164	4.93787	.53872	891.1	1.098	.69788	4.99748	.58539	931.9	1.117	.80068	5.81351	5.1407
25	0	.030	.0600	928.1	1.077	.68564	4.88524	.53800	881.1	1.086	.69182	4.94493	.58539	924.9	1.105	.80068	5.81563	5.1407
26	0	.030	.0625	921.1	1.065	.67964	4.83261	.53728	871.1	1.074	.68576	4.89248	.58539	917.9	1.093	.80068	5.81775	5.1407
27	0	.030	.0650	914.1	1.053	.67364	4.78002	.53656	861.1	1.062	.67970	4.84003	.58539	910.9	1.081	.80068	5.81987	5.1407
28	0	.030	.0675	907.1	1.041	.66764	4.72739	.53584	851.1	1.050	.67364	4.78758	.58539	903.9	1.069	.80068	5.82199	5.1407
29	0	.030	.0700	900.1	1.029	.66164	4.67476	.53512	841.1	1.038	.66758	4.73503	.58539	896.9	1.057	.80068	5.82411	5.1407
30	0	.030	.0725	893.1	1.017	.65564	4.62213	.53440	831.1	1.026	.66152	4.68248	.58539	889.9	1.045	.80068	5.82623	5.1407
31	0	.030	.0750	886.1	1.005	.64964	4.56950	.53368	821.1	1.014	.65546	4.62993	.58539	882.9	1.033	.80068	5.82835	5.1407
32	0	.030	.0775	879.1	0.993	.64364	4.51684	.53296	811.1	1.002	.64940	4.57738	.58539	875.9	1.021	.80068	5.83047	5.1407
33	0	.030	.0800	872.1	0.981	.63764	4.46421	.53224	801.1	0.990	.64334	4.52483	.58539	868.9	1.009	.80068	5.83259	5.1407
34	0	.030	.0825	865.1	0.969	.63164	4.41158	.53152	791.1	0.978	.63728	4.47228	.58539	861.9	0.997	.80068	5.83471	5.1407
35	0	.030	.0850	858.1	0.957	.62564	4.35895	.53080	781.1	0.966	.63122	4.41973	.58539	854.9	0.985	.80068	5.83683	5.1407
36	0	.030	.0875	851.1	0.945	.61964	4.30632	.53008	771.1	0.954	.62516	4.36718	.58539	847.9	0.973	.80068	5.83895	5.1407
37	0	.030	.0900	844.1	0.933	.61364	4.25369	.52936	761.1	0.942	.61910	4.31463	.58539	840.9	0.961	.80068	5.84107	5.1407
38	0	.030	.0925	837.1	0.921	.60764	4.20106	.52864	751.1	0.930	.61304	4.26208	.58539	833.9	0.949	.80068	5.84319	5.1407
39	0	.030	.0950	830.1	0.909	.60164	4.14843	.52792	741.1	0.918	.60698	4.20953	.58539	826.9	0.937	.80068	5.84531	5.1407
40	0	.030	.0975	823.1	0.897	.59564	4.09580	.52720	731.1	0.906	.60092	4.15698	.58539	819.9	0.925	.80068	5.84743	5.1407
41	0	.030	.1000	816.1	0.885	.58964	4.04317	.52648	721.1	0.894	.60092	4.10443	.58539	812.9	0.913	.80068	5.84955	5.1407
42	0	.030	.1025	809.1	0.873	.58364	3.99054	.52576	711.1	0.882	.59486	4.05188	.58539	805.9	0.901	.80068	5.85167	5.1407
43	0	.030	.1050	802.1	0.861	.57764	3.93791	.52504	701.1	0.870	.58880	4.00000	.58539	798.9	0.889	.80068	5.85379	5.1407
44	0	.030	.1075	795.1	0.849	.57164	3.88528	.52432	691.1	0.858	.58274	3.94843	.58539	791.9	0.877	.80068	5.85591	5.1407
45	0	.030	.1100	788.1	0.837	.56564	3.83265	.52360	681.1	0.846	.57668	3.89688	.58539	784.9	0.865	.80068	5.85803	5.1407
46	0	.030	.1125	781.1	0.825	.55964	3.78002	.52288	671.1	0.834	.57062	3.84533	.58539	777.9	0.853	.80068	5.86015	5.1407
47	0	.030	.1150	774.1	0.813	.55364	3.72739	.52216	661.1	0.822	.56456	3.79378	.58539	770.9	0.841	.80068	5.86227	5.1407
48	0	.030	.1175	767.1	0.801	.54764	3.67476	.52144	651.1	0.810	.55850	3.74223	.58539	763.9	0.829	.80068	5.86439	5.1407
49	0	.030	.1200	760.1	0.789	.54164	3.62213	.52072	641.1	0.798	.55244	3.69068	.58539	756.9	0.817	.80068	5.86651	5.1407
50	0	.030	.1225	753.1	0.777	.53564	3.56950	.52000	631.1	0.786	.54638	3.63913	.58539	749.9	0.805	.80068	5.86863	5.1407

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE I.- DATA^a FOR 140° CONE; $M_{\infty} = 2.30$ - Concluded(e) $\alpha = 20^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ$, $P_t = 2291.9$ psf				$\Phi = 90.0^\circ$, $P_t = 2290.1$ psf					
				$P_{t,1}$ psf	C_p	$P_{t,1}/P_{t,2}$	$P_{t,1}/P_{t,2}$	$M_{t,1}$	$P_{t,1}$ psf	C_p	$P_{t,1}/P_{t,2}$	$P_{t,1}/P_{t,2}$	$M_{t,1}$
1	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
2	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
3	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
4	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
5	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
6	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
7	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
8	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
9	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
10	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
11	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
12	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
13	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
14	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
15	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
16	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
17	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
18	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
19	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
20	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
21	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
22	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
23	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
24	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
25	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
26	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
27	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
28	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
29	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
30	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
31	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
32	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
33	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
34	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
35	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
36	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
37	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
38	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
39	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
40	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
41	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
42	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
43	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
44	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
45	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
46	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
47	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
48	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460
49	0	.300	.0000	1115.4	1.375	.8508	6.0903	.83475	1.115.1	1.374	.83475	6.08843	.51460

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².
Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE 11.- DATA^a FOR 140° CONE; M_∞ = 2.96(a) $\alpha = 0^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ$, $p_t = 3240.6$ psf					$\Phi = 22.5^\circ$, $p_t = 3242.4$ psf					$\Phi = 45.0^\circ$, $p_t = 3240.7$ psf				
				p_t , psf	C_p	$p_L/p_{L,2}$	p_L/p_{∞}	M_L	p_t , psf	C_p	$p_L/p_{L,2}$	p_L/p_{∞}	M_L	p_t , psf	C_p	$p_L/p_{L,2}$	p_L/p_{∞}	M_L
1	0	.330	.0000	1087.9	1.730	.98801	11.43259	-13141	1087.5	1.729	.98704	11.60119	-13666	1087.9	1.730	.98791	11.61143	-13195
2	0	.500	.0000	1087.9	1.722	.98366	11.56151	-15199	1087.7	1.720	.98269	11.43259	-15199	1087.9	1.722	.98356	11.56035	-13406
3	0	.670	.0000	1076.8	1.711	.97787	11.49340	-17911	1077.9	1.712	.97834	11.43259	-17911	1078.3	1.714	.97922	11.50928	-13488
4	0	.840	.0000	1076.8	1.703	.97352	11.44232	-19618	1071.5	1.701	.97254	11.43259	-19618	1071.9	1.692	.96902	11.30010	-12131
5	0	1.000	.0000	1065.6	1.692	.96772	11.37421	-21700	1055.7	1.670	.96095	11.29455	-23924	1059.2	1.680	.96183	11.23687	-23644
6	0	1.330	.0000	1051.3	1.657	.95449	11.22097	-25824	1040.4	1.655	.94700	11.22097	-25824	1044.8	1.669	.95040	11.23687	-23644
7	0	1.670	.0000	1036.9	1.653	.94155	11.13583	-29879	1024.4	1.654	.93406	11.14123	-27753	1036.8	1.655	.94880	11.15174	-27505
8	0	2.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
9	0	2.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
10	0	2.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
11	0	3.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
12	0	3.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
13	0	3.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
14	0	4.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
15	0	4.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
16	0	4.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
17	0	5.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
18	0	5.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
19	0	5.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
20	0	6.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
21	0	6.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
22	0	6.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
23	0	7.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
24	0	7.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
25	0	7.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
26	0	8.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
27	0	8.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
28	0	8.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
29	0	9.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
30	0	9.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
31	0	9.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
32	0	10.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
33	0	10.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
34	0	10.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
35	0	11.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
36	0	11.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
37	0	11.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
38	0	12.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
39	0	12.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
40	0	12.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
41	0	13.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
42	0	13.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
43	0	13.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
44	0	14.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
45	0	14.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
46	0	14.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
47	0	15.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
48	0	15.330	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
49	0	15.670	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933
50	0	16.000	.0000	1028.9	1.628	.93440	11.06272	-32933	1016.4	1.640	.92686	11.06272	-32933	1036.8	1.630	.93157	11.06272	-32933

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE 11.- DATA^a FOR 140° CONE; $M_{\infty} = 2.96$ - Continued

(a) $\alpha = 0^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/δ^*	$\phi = 67.5^\circ, P_t = 3240.2 \text{ psf}$	$\phi = 90.0^\circ, P_t = 3241.2 \text{ psf}$	M_L	P_t/ρ_{∞}	C_p	$P_L/P_{L,2}$	P_L/ρ_{∞}	M_L
				P_L , psf	C_p	$P_L/P_{L,2}$	P_L/ρ_{∞}	$P_L/P_{L,2}$	C_p	P_L/ρ_{∞}	M_L
1	0	.320	.000	1088.6	1.732	.9873	11.62115	.9873	1.729	11.49447	13.908
2	0	.220	.025	1085.8	1.723	.9848	11.56996	.9848	1.724	11.49843	13.908
3	0	.500	.050	1080.6	1.710	.98147	11.53583	.98147	1.715	11.51947	16.977
4	0	.530	.075	1075.8	1.704	.97812	11.48464	.97812	1.704	11.45131	19.928
5	0	1.000	.100	1065.4	1.698	.97131	11.41638	.97131	1.696	11.40019	20.929
6	0	1.500	.150	1053.4	1.671	.95679	11.24573	.95679	1.672	11.24366	24.732
7	0	1.230	.175	1053.4	1.671	.95679	11.24573	.95679	1.672	11.24366	24.732
8	0	1.530	.200	1047.1	1.659	.95209	11.17747	.95209	1.662	11.19570	26.448
9	0	1.830	.225	1037.5	1.643	.94227	11.07508	.94227	1.646	11.09346	28.855
10	0	2.000	.250	1031.1	1.632	.93847	11.00682	.93847	1.632	11.00825	30.736
11	0	2.500	.275	1011.5	1.601	.92050	10.81911	.92050	1.598	10.80376	34.905
12	0	2.230	.275	1011.5	1.601	.92050	10.81911	.92050	1.598	10.80376	34.905
13	0	2.430	.300	1002.3	1.582	.91033	10.69965	.91033	1.585	10.71856	36.529
14	0	2.530	.325	992.7	1.565	.90162	10.59726	.90162	1.565	10.59928	38.714
15	0	3.000	.350	981.5	1.548	.89156	10.47811	.89156	1.540	10.44551	41.596
16	0	3.230	.375	970.1	1.538	.88459	10.37026	.88459	1.540	10.44551	41.596
17	0	3.230	.400	954.5	1.490	.86242	10.13651	.86242	1.487	10.12214	46.701
18	0	3.500	.425	928.8	1.454	.84355	9.91467	.84355	1.451	9.90041	50.119
19	0	3.400	.450	868.7	1.412	.82177	9.65870	.82177	1.410	9.64500	53.906
20	0	4.000	.500	868.7	1.412	.82177	9.65870	.82177	1.410	9.64500	53.906
21	0	4.000	.500	868.7	1.412	.82177	9.65870	.82177	1.410	9.64500	53.906
22	180	.025	.025	1087.4	1.710	.98764	11.60826	.98764	1.731	11.61757	12.905
23	180	.050	.050	1081.0	1.719	.98184	11.54007	.98184	1.717	11.53227	16.501
24	180	.075	.075	1074.6	1.707	.97603	11.47189	.97603	1.709	11.48109	18.336
25	180	.100	.100	1068.1	1.695	.96943	11.40370	.96943	1.697	11.41281	20.543
26	180	.125	.125	1061.9	1.685	.96443	11.33552	.96443	1.683	11.34482	22.943
27	180	1.230	.150	1051.1	1.677	.96008	11.28438	.96008	1.673	11.25932	24.850
28	180	1.430	.175	1049.1	1.663	.95283	11.19915	.95283	1.659	11.17402	26.974
29	180	1.530	.200	1035.1	1.635	.93833	11.02870	.93833	1.637	11.03754	30.100
30	180	2.000	.225	1025.1	1.607	.92382	10.85824	.92382	1.603	10.83253	34.172
31	180	2.200	.250	1017.1	1.607	.92382	10.85824	.92382	1.603	10.83253	34.172
32	180	2.400	.275	1006.0	1.588	.91367	10.73892	.91367	1.589	10.74753	35.983
33	180	2.500	.300	995.4	1.571	.90497	10.63664	.90497	1.570	10.62811	38.194
34	180	2.500	.325	995.4	1.571	.90497	10.63664	.90497	1.570	10.62811	38.194
35	180	3.000	.350	975.6	1.557	.89377	10.50027	.89377	1.548	10.49164	40.610
36	180	3.230	.375	963.9	1.546	.88581	10.37640	.88581	1.548	10.49164	40.610
37	180	3.230	.400	953.3	1.463	.86581	10.17640	.86581	1.468	10.18552	45.742
38	180	3.500	.425	934.1	1.463	.86581	10.17640	.86581	1.468	10.18552	45.742
39	180	3.500	.450	868.7	1.418	.82521	9.97185	.82521	1.420	9.97085	49.913
40	180	4.000	.500	868.7	1.418	.82521	9.97185	.82521	1.420	9.97085	49.913
41	180	4.000	.500	868.7	1.418	.82521	9.97185	.82521	1.420	9.97085	49.913
42	270	1.300	.250	1068.2	1.696	.97023	11.40371	.97023	1.695	11.39579	20.544
43	270	2.000	.250	1031.5	1.632	.93688	11.01165	.93688	1.631	11.00342	30.840
44	270	3.000	.375	977.2	1.538	.88757	10.43209	.88757	1.542	10.45752	41.198
45	270	3.000	.375	977.2	1.538	.88757	10.43209	.88757	1.542	10.45752	41.198
46	270	3.230	.400	958.2	1.490	.86242	10.13651	.86242	1.487	10.12214	46.701
47	90	2.000	.250	1017.9	1.612	.92630	10.88737	.92630	1.612	10.88907	33.719
48	90	3.000	.375	963.9	1.515	.87549	10.29010	.87549	1.512	10.27551	44.241
49	90	4.000	.500	816.9	1.259	.74191	8.72013	.74191	1.260	8.72481	66.559

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE 11.- DATA^a FOR 140° CONE; $M_{90} = 2.96$ - Continued

(b) $\alpha = 5^\circ$

Orifice θ , deg	s, in.	s/d	s/s*	$\Phi = 0.0^\circ, p_t = 3244.0 \text{ psf}$	$\Phi = 22.5^\circ, p_t = 3241.6 \text{ psf}$	$\Phi = 45.0^\circ, p_t = 3242.5 \text{ psf}$									
				$P_{t,1}$ psf	C_p	$P_t/P_{t,2}$	M_L	$P_{t,1}$ psf	C_p	$P_t/P_{t,2}$	M_L	$P_{t,1}$ psf	C_p	$P_t/P_{t,2}$	M_L
1	0	0.000	-0.000	1073.2	1.703	0.97368	11.44302	0.97368	1.703	0.97368	11.44302	1073.1	1.703	0.97368	11.44302
2	0	0.025	-0.025	1055.6	1.672	0.95764	11.25570	0.95764	1.672	0.95764	11.25570	1060.3	1.681	0.96237	11.144751
3	0	0.050	-0.050	1038.0	1.644	0.93330	11.04445	0.93330	1.644	0.93330	11.04445	1050.5	1.673	0.95802	11.00445
4	0	0.075	-0.075	1020.4	1.619	0.91330	10.80445	0.91330	1.619	0.91330	10.80445	1040.7	1.662	0.94222	10.76045
5	0	0.100	-0.100	1002.8	1.594	0.89330	10.60445	0.89330	1.594	0.89330	10.60445	1030.9	1.653	0.93112	10.71645
6	0	0.125	-0.125	985.2	1.569	0.87330	10.40445	0.87330	1.569	0.87330	10.40445	1021.1	1.644	0.92002	10.67245
7	0	0.150	-0.150	967.6	1.544	0.85330	10.20445	0.85330	1.544	0.85330	10.20445	1011.3	1.635	0.90892	10.62845
8	0	0.175	-0.175	950.0	1.519	0.83330	10.00445	0.83330	1.519	0.83330	10.00445	1001.5	1.626	0.89782	10.58445
9	0	0.200	-0.200	932.4	1.494	0.81330	9.80445	0.81330	1.494	0.81330	9.80445	991.7	1.617	0.88672	10.54045
10	0	0.225	-0.225	914.8	1.469	0.79330	9.60445	0.79330	1.469	0.79330	9.60445	981.9	1.608	0.87562	10.49645
11	0	0.250	-0.250	897.2	1.444	0.77330	9.40445	0.77330	1.444	0.77330	9.40445	972.1	1.600	0.86452	10.45245
12	0	0.275	-0.275	879.6	1.419	0.75330	9.20445	0.75330	1.419	0.75330	9.20445	962.3	1.591	0.85342	10.40845
13	0	0.300	-0.300	862.0	1.394	0.73330	9.00445	0.73330	1.394	0.73330	9.00445	952.5	1.582	0.84232	10.36445
14	0	0.325	-0.325	844.4	1.369	0.71330	8.80445	0.71330	1.369	0.71330	8.80445	942.7	1.573	0.83122	10.32045
15	0	0.350	-0.350	826.8	1.344	0.69330	8.60445	0.69330	1.344	0.69330	8.60445	932.9	1.564	0.82012	10.27645
16	0	0.375	-0.375	809.2	1.319	0.67330	8.40445	0.67330	1.319	0.67330	8.40445	923.1	1.555	0.80902	10.23245
17	0	0.400	-0.400	791.6	1.294	0.65330	8.20445	0.65330	1.294	0.65330	8.20445	913.3	1.546	0.79792	10.18845
18	0	0.425	-0.425	774.0	1.269	0.63330	8.00445	0.63330	1.269	0.63330	8.00445	903.5	1.537	0.78682	10.14445
19	0	0.450	-0.450	756.4	1.244	0.61330	7.80445	0.61330	1.244	0.61330	7.80445	893.7	1.528	0.77572	10.10045
20	0	0.475	-0.475	738.8	1.219	0.59330	7.60445	0.59330	1.219	0.59330	7.60445	883.9	1.519	0.76462	10.05645
21	0	0.500	-0.500	721.2	1.194	0.57330	7.40445	0.57330	1.194	0.57330	7.40445	874.1	1.510	0.75352	10.01245
22	0	0.525	-0.525	703.6	1.169	0.55330	7.20445	0.55330	1.169	0.55330	7.20445	864.3	1.501	0.74242	9.96845
23	0	0.550	-0.550	686.0	1.144	0.53330	7.00445	0.53330	1.144	0.53330	7.00445	854.5	1.492	0.73132	9.92445
24	0	0.575	-0.575	668.4	1.119	0.51330	6.80445	0.51330	1.119	0.51330	6.80445	844.7	1.483	0.72022	9.88045
25	0	0.600	-0.600	650.8	1.094	0.49330	6.60445	0.49330	1.094	0.49330	6.60445	834.9	1.474	0.70912	9.83645
26	0	0.625	-0.625	633.2	1.069	0.47330	6.40445	0.47330	1.069	0.47330	6.40445	825.1	1.465	0.69802	9.79245
27	0	0.650	-0.650	615.6	1.044	0.45330	6.20445	0.45330	1.044	0.45330	6.20445	815.3	1.456	0.68692	9.74845
28	0	0.675	-0.675	598.0	1.019	0.43330	6.00445	0.43330	1.019	0.43330	6.00445	805.5	1.447	0.67582	9.70445
29	0	0.700	-0.700	580.4	0.994	0.41330	5.80445	0.41330	0.994	0.41330	5.80445	795.7	1.438	0.66472	9.66045
30	0	0.725	-0.725	562.8	0.969	0.39330	5.60445	0.39330	0.969	0.39330	5.60445	785.9	1.429	0.65362	9.61645
31	0	0.750	-0.750	545.2	0.944	0.37330	5.40445	0.37330	0.944	0.37330	5.40445	776.1	1.420	0.64252	9.57245
32	0	0.775	-0.775	527.6	0.919	0.35330	5.20445	0.35330	0.919	0.35330	5.20445	766.3	1.411	0.63142	9.52845
33	0	0.800	-0.800	510.0	0.894	0.33330	5.00445	0.33330	0.894	0.33330	5.00445	756.5	1.402	0.62032	9.48445
34	0	0.825	-0.825	492.4	0.869	0.31330	4.80445	0.31330	0.869	0.31330	4.80445	746.7	1.393	0.60922	9.44045
35	0	0.850	-0.850	474.8	0.844	0.29330	4.60445	0.29330	0.844	0.29330	4.60445	736.9	1.384	0.59812	9.39645
36	0	0.875	-0.875	457.2	0.819	0.27330	4.40445	0.27330	0.819	0.27330	4.40445	727.1	1.375	0.58702	9.35245
37	0	0.900	-0.900	439.6	0.794	0.25330	4.20445	0.25330	0.794	0.25330	4.20445	717.3	1.366	0.57592	9.30845
38	0	0.925	-0.925	422.0	0.769	0.23330	4.00445	0.23330	0.769	0.23330	4.00445	707.5	1.357	0.56482	9.26445
39	0	0.950	-0.950	404.4	0.744	0.21330	3.80445	0.21330	0.744	0.21330	3.80445	697.7	1.348	0.55372	9.22045
40	0	0.975	-0.975	386.8	0.719	0.19330	3.60445	0.19330	0.719	0.19330	3.60445	687.9	1.339	0.54262	9.17645
41	0	1.000	-1.000	369.2	0.694	0.17330	3.40445	0.17330	0.694	0.17330	3.40445	678.1	1.330	0.53152	9.13245
42	0	1.025	-1.025	351.6	0.669	0.15330	3.20445	0.15330	0.669	0.15330	3.20445	668.3	1.321	0.52042	9.08845
43	0	1.050	-1.050	334.0	0.644	0.13330	3.00445	0.13330	0.644	0.13330	3.00445	658.5	1.312	0.50932	9.04445
44	0	1.075	-1.075	316.4	0.619	0.11330	2.80445	0.11330	0.619	0.11330	2.80445	648.7	1.303	0.49822	9.00045
45	0	1.100	-1.100	298.8	0.594	0.09330	2.60445	0.09330	0.594	0.09330	2.60445	638.9	1.294	0.48712	8.95645
46	0	1.125	-1.125	281.2	0.569	0.07330	2.40445	0.07330	0.569	0.07330	2.40445	629.1	1.285	0.47602	8.91245
47	0	1.150	-1.150	263.6	0.544	0.05330	2.20445	0.05330	0.544	0.05330	2.20445	619.3	1.276	0.46492	8.86845
48	0	1.175	-1.175	246.0	0.519	0.03330	2.00445	0.03330	0.519	0.03330	2.00445	609.5	1.267	0.45382	8.82445
49	0	1.200	-1.200	228.4	0.494	0.01330	1.80445	0.01330	0.494	0.01330	1.80445	599.7	1.258	0.44272	8.78045
50	0	1.225	-1.225	210.8	0.469	0.00330	1.60445	0.00330	0.469	0.00330	1.60445	589.9	1.249	0.43162	8.73645

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE II.- DATA^a FOR 140° CONE; $M_{\infty} = 2.96$ - Continued(b) $\alpha = 5^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ$, $p_t = 3242.9$ psf				$\phi = 90.0^\circ$, $p_t = 3240.1$ psf					
				$p_{t,1}$ psf	C_p	$p_{t1}/p_{t,2}$	p_{t1}/p_{∞}	M_{t1}	$p_{t,1}$ psf	C_p	$p_{t1}/p_{t,2}$	p_{t1}/p_{∞}	M_{t1}
1	0	.000	.0000	1073.0	1.703	.97377	11.44531	1.9522	1073.0	1.705	.97451	11.45520	1.9201
2	0	.230	.0065	1065.1	1.689	.96653	11.36015	1.22107	1059.8	1.699	.96736	11.36996	1.9201
3	0	.460	.0141	1058.7	1.678	.96073	11.29207	.23991	1055.1	1.682	.96301	11.31883	1.9201
4	0	.690	.0216	1044.4	1.670	.95538	11.24093	.25692	1040.5	1.674	.95866	11.26769	1.9201
5	0	.920	.0291	1030.1	1.661	.95003	11.19979	.27393	1026.7	1.666	.95331	11.21655	1.9201
6	0	1.150	.0366	1015.8	1.654	.94479	11.16865	.29094	1012.7	1.657	.94800	11.16541	1.9201
7	0	1.380	.0441	1001.5	1.634	.93954	11.13751	.30795	1000.0	1.652	.94275	11.11427	1.9201
8	0	1.610	.0516	987.2	1.623	.93429	11.10637	.32496	996.7	1.648	.93750	11.06313	1.9201
9	0	1.840	.0591	972.9	1.623	.92904	11.07523	.34197	992.4	1.649	.93225	11.01199	1.9201
10	0	2.070	.0666	958.6	1.620	.92379	11.04409	.35898	988.9	1.648	.92699	10.96085	1.9201
11	0	2.300	.0741	944.3	1.609	.91854	11.01295	.37599	985.6	1.646	.92174	10.90971	1.9201
12	0	2.530	.0816	930.0	1.608	.91329	10.98181	.39300	982.3	1.643	.91649	10.85857	1.9201
13	0	2.760	.0891	915.7	1.607	.90804	10.95067	.41001	979.0	1.642	.91124	10.80743	1.9201
14	0	2.990	.0966	901.4	1.606	.90279	10.91953	.42702	975.7	1.640	.90599	10.75629	1.9201
15	0	3.220	.1041	887.1	1.605	.89754	10.88839	.44403	972.4	1.639	.90074	10.70515	1.9201
16	0	3.450	.1116	872.8	1.604	.89229	10.85725	.46104	969.1	1.638	.89549	10.65401	1.9201
17	0	3.680	.1191	858.5	1.603	.88704	10.82611	.47805	965.8	1.637	.89024	10.60287	1.9201
18	0	3.910	.1266	844.2	1.602	.88179	10.79497	.49506	962.5	1.636	.88499	10.55173	1.9201
19	0	4.140	.1341	829.9	1.601	.87654	10.76383	.51207	959.2	1.635	.87974	10.50059	1.9201
20	0	4.370	.1416	815.6	1.600	.87129	10.73269	.52908	955.9	1.634	.87449	10.44945	1.9201
21	0	4.600	.1491	801.3	1.599	.86604	10.70155	.54609	952.6	1.633	.86924	10.39831	1.9201
22	0	4.830	.1566	787.0	1.598	.86079	10.67041	.56310	949.3	1.632	.86399	10.34717	1.9201
23	0	5.060	.1641	772.7	1.597	.85554	10.63927	.58011	946.0	1.631	.85874	10.29603	1.9201
24	0	5.290	.1716	758.4	1.596	.85029	10.60813	.59712	942.7	1.630	.85349	10.24489	1.9201
25	0	5.520	.1791	744.1	1.595	.84504	10.57699	.61413	939.4	1.629	.84824	10.19375	1.9201
26	0	5.750	.1866	729.8	1.594	.83979	10.54585	.63114	936.1	1.628	.84299	10.14261	1.9201
27	0	5.980	.1941	715.5	1.593	.83454	10.51471	.64815	932.8	1.627	.83774	10.09147	1.9201
28	0	6.210	.2016	701.2	1.592	.82929	10.48357	.66516	929.5	1.626	.83249	10.04033	1.9201
29	0	6.440	.2091	686.9	1.591	.82404	10.45243	.68217	926.2	1.625	.82724	9.98919	1.9201
30	0	6.670	.2166	672.6	1.590	.81879	10.42129	.69918	922.9	1.624	.82199	9.93805	1.9201
31	0	6.900	.2241	658.3	1.589	.81354	10.39015	.71619	919.6	1.623	.81674	9.88691	1.9201
32	0	7.130	.2316	644.0	1.588	.80829	10.35901	.73320	916.3	1.622	.81149	9.83577	1.9201
33	0	7.360	.2391	629.7	1.587	.80304	10.32787	.75021	913.0	1.621	.80624	9.78463	1.9201
34	0	7.590	.2466	615.4	1.586	.79779	10.29673	.76722	909.7	1.620	.80099	9.73349	1.9201
35	0	7.820	.2541	601.1	1.585	.79254	10.26559	.78423	906.4	1.619	.79574	9.68235	1.9201
36	0	8.050	.2616	586.8	1.584	.78729	10.23445	.80124	903.1	1.618	.79049	9.63121	1.9201
37	0	8.280	.2691	572.5	1.583	.78204	10.20331	.81825	900.0	1.617	.78524	9.58007	1.9201
38	0	8.510	.2766	558.2	1.582	.77679	10.17217	.83526	896.7	1.616	.77999	9.52893	1.9201
39	0	8.740	.2841	543.9	1.581	.77154	10.14103	.85227	893.4	1.615	.77474	9.47779	1.9201
40	0	8.970	.2916	529.6	1.580	.76629	10.10989	.86928	890.1	1.614	.76949	9.42665	1.9201
41	0	9.200	.2991	515.3	1.579	.76104	10.07875	.88629	886.8	1.613	.76424	9.37551	1.9201
42	0	9.430	.3066	501.0	1.578	.75579	10.04761	.90330	883.5	1.612	.75899	9.32437	1.9201
43	0	9.660	.3141	486.7	1.577	.75054	10.01647	.92031	880.2	1.611	.75374	9.27323	1.9201
44	0	9.890	.3216	472.4	1.576	.74529	9.98533	.93732	876.9	1.610	.74849	9.22209	1.9201
45	0	10.120	.3291	458.1	1.575	.74004	9.95419	.95433	873.6	1.609	.74324	9.17095	1.9201
46	0	10.350	.3366	443.8	1.574	.73479	9.92305	.97134	870.3	1.608	.73799	9.11981	1.9201
47	0	10.580	.3441	429.5	1.573	.72954	9.89191	.98835	867.0	1.607	.73274	9.06867	1.9201
48	0	10.810	.3516	415.2	1.572	.72429	9.86077	.10000	863.7	1.606	.72749	9.01753	1.9201
49	0	11.040	.3591	400.9	1.571	.71904	9.82963	.10000	860.4	1.605	.72224	8.96639	1.9201

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE II.- DATA^a FOR 140° CONE; $M_{\infty} = 2.96$ - Continued

(c) $\alpha = 10^\circ$

Orifice θ , deg	s , in.	s/D	s/δ^*	$\Phi = 0.0^\circ, P_t = 3244.1 \text{ psf}$				$\Phi = 22.5^\circ, P_t = 3243.0 \text{ psf}$				$\Phi = 45.0^\circ, P_t = 3242.6 \text{ psf}$			
				P_t/psf	C_p	$P_t/P_{t,2}$	M_t/ρ_{∞}	M_t	P_t/psf	C_p	$P_t/P_{t,2}$	M_t/ρ_{∞}	M_t	P_t/psf	C_p
1	0	.000	.0000	1038.1	1.642	11.0400	29426	11.0710	29359	1038.0	1.642	9.6203	29359	11.0720	29329
2	.020	.025	.0041	1039.1	1.586	9.1270	29426	9.6133	29359	1037.6	1.586	9.1270	29359	10.7485	29381
3	.040	.050	.0093	1040.5	1.583	9.1125	29426	9.6133	29359	1037.6	1.583	9.1125	29359	10.7485	29381
4	.060	.075	.0144	998.1	1.572	9.0546	29426	9.6133	29359	1037.6	1.572	9.0546	29359	10.7485	29381
5	.080	.100	.0195	982.2	1.564	8.9928	29426	9.6133	29359	1037.6	1.564	8.9928	29359	10.7485	29381
6	.100	.125	.0247	972.6	1.558	8.9288	29426	9.6133	29359	1037.6	1.558	8.9288	29359	10.7485	29381
7	.120	.150	.0299	967.8	1.551	8.8773	29426	9.6133	29359	1037.6	1.551	8.8773	29359	10.7485	29381
8	.140	.175	.0350	956.6	1.546	8.8279	29426	9.6133	29359	1037.6	1.546	8.8279	29359	10.7485	29381
9	.160	.200	.0400	946.6	1.542	8.7799	29426	9.6133	29359	1037.6	1.542	8.7799	29359	10.7485	29381
10	.180	.225	.0449	936.1	1.539	8.7331	29426	9.6133	29359	1037.6	1.539	8.7331	29359	10.7485	29381
11	.200	.250	.0498	926.5	1.536	8.6879	29426	9.6133	29359	1037.6	1.536	8.6879	29359	10.7485	29381
12	.220	.275	.0548	916.9	1.533	8.6437	29426	9.6133	29359	1037.6	1.533	8.6437	29359	10.7485	29381
13	.240	.300	.0598	907.7	1.530	8.6001	29426	9.6133	29359	1037.6	1.530	8.6001	29359	10.7485	29381
14	.260	.325	.0647	898.7	1.527	8.5571	29426	9.6133	29359	1037.6	1.527	8.5571	29359	10.7485	29381
15	.280	.350	.0697	889.7	1.524	8.5146	29426	9.6133	29359	1037.6	1.524	8.5146	29359	10.7485	29381
16	.300	.375	.0747	880.8	1.521	8.4726	29426	9.6133	29359	1037.6	1.521	8.4726	29359	10.7485	29381
17	.320	.400	.0797	871.9	1.518	8.4311	29426	9.6133	29359	1037.6	1.518	8.4311	29359	10.7485	29381
18	.340	.425	.0847	863.0	1.515	8.3901	29426	9.6133	29359	1037.6	1.515	8.3901	29359	10.7485	29381
19	.360	.450	.0897	854.1	1.512	8.3496	29426	9.6133	29359	1037.6	1.512	8.3496	29359	10.7485	29381
20	.380	.475	.0947	845.2	1.509	8.3096	29426	9.6133	29359	1037.6	1.509	8.3096	29359	10.7485	29381
21	.400	.500	.0997	836.3	1.506	8.2701	29426	9.6133	29359	1037.6	1.506	8.2701	29359	10.7485	29381
22	.420	.525	.1047	827.4	1.503	8.2311	29426	9.6133	29359	1037.6	1.503	8.2311	29359	10.7485	29381
23	.440	.550	.1097	818.5	1.500	8.1926	29426	9.6133	29359	1037.6	1.500	8.1926	29359	10.7485	29381
24	.460	.575	.1147	809.6	1.497	8.1546	29426	9.6133	29359	1037.6	1.497	8.1546	29359	10.7485	29381
25	.480	.600	.1197	800.7	1.494	8.1171	29426	9.6133	29359	1037.6	1.494	8.1171	29359	10.7485	29381
26	.500	.625	.1247	791.8	1.491	8.0801	29426	9.6133	29359	1037.6	1.491	8.0801	29359	10.7485	29381
27	.520	.650	.1297	782.9	1.488	8.0436	29426	9.6133	29359	1037.6	1.488	8.0436	29359	10.7485	29381
28	.540	.675	.1347	774.0	1.485	8.0076	29426	9.6133	29359	1037.6	1.485	8.0076	29359	10.7485	29381
29	.560	.700	.1397	765.1	1.482	7.9721	29426	9.6133	29359	1037.6	1.482	7.9721	29359	10.7485	29381
30	.580	.725	.1447	756.2	1.479	7.9371	29426	9.6133	29359	1037.6	1.479	7.9371	29359	10.7485	29381
31	.600	.750	.1497	747.3	1.476	7.9021	29426	9.6133	29359	1037.6	1.476	7.9021	29359	10.7485	29381
32	.620	.775	.1547	738.4	1.473	7.8671	29426	9.6133	29359	1037.6	1.473	7.8671	29359	10.7485	29381
33	.640	.800	.1597	729.5	1.470	7.8321	29426	9.6133	29359	1037.6	1.470	7.8321	29359	10.7485	29381
34	.660	.825	.1647	720.6	1.467	7.7971	29426	9.6133	29359	1037.6	1.467	7.7971	29359	10.7485	29381
35	.680	.850	.1697	711.7	1.464	7.7621	29426	9.6133	29359	1037.6	1.464	7.7621	29359	10.7485	29381
36	.700	.875	.1747	702.8	1.461	7.7271	29426	9.6133	29359	1037.6	1.461	7.7271	29359	10.7485	29381
37	.720	.900	.1797	693.9	1.458	7.6921	29426	9.6133	29359	1037.6	1.458	7.6921	29359	10.7485	29381
38	.740	.925	.1847	685.0	1.455	7.6571	29426	9.6133	29359	1037.6	1.455	7.6571	29359	10.7485	29381
39	.760	.950	.1897	676.1	1.452	7.6221	29426	9.6133	29359	1037.6	1.452	7.6221	29359	10.7485	29381
40	.780	.975	.1947	667.2	1.449	7.5871	29426	9.6133	29359	1037.6	1.449	7.5871	29359	10.7485	29381
41	.800	1.000	.2000	658.3	1.446	7.5521	29426	9.6133	29359	1037.6	1.446	7.5521	29359	10.7485	29381
42	.820	1.025	.2050	649.4	1.443	7.5171	29426	9.6133	29359	1037.6	1.443	7.5171	29359	10.7485	29381
43	.840	1.050	.2100	640.5	1.440	7.4821	29426	9.6133	29359	1037.6	1.440	7.4821	29359	10.7485	29381
44	.860	1.075	.2150	631.6	1.437	7.4471	29426	9.6133	29359	1037.6	1.437	7.4471	29359	10.7485	29381
45	.880	1.100	.2200	622.7	1.434	7.4121	29426	9.6133	29359	1037.6	1.434	7.4121	29359	10.7485	29381
46	.900	1.125	.2250	613.8	1.431	7.3771	29426	9.6133	29359	1037.6	1.431	7.3771	29359	10.7485	29381
47	.920	1.150	.2300	604.9	1.428	7.3421	29426	9.6133	29359	1037.6	1.428	7.3421	29359	10.7485	29381
48	.940	1.175	.2350	596.0	1.425	7.3071	29426	9.6133	29359	1037.6	1.425	7.3071	29359	10.7485	29381
49	.960	1.200	.2400	587.1	1.422	7.2721	29426	9.6133	29359	1037.6	1.422	7.2721	29359	10.7485	29381
50	.980	1.225	.2450	578.2	1.419	7.2371	29426	9.6133	29359	1037.6	1.419	7.2371	29359	10.7485	29381

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².
Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE 11.- DATA^a FOR 140° CONE; $M_{\infty} = 2.96$ - Continued(c) $\alpha = 10^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ, P_t = 3243.2$ psf					$\Phi = 90.0^\circ, P_t = 3240.9$ psf				
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,0}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,0}$	M_t
1	0	.300	.0000	1036.3	1.639	.96036	11.05155	.29770	1034.7	1.638	.91958	11.04336	.29973
2	0	.200	.0025	1015.6	1.603	.92152	10.86522	.33696	1031.5	1.626	.93668	11.00927	.30716
3	0	.100	.0050	1015.6	1.593	.92152	10.86522	.33696	1028.3	1.626	.93668	11.00927	.30716
4	0	.050	.0075	1015.6	1.593	.92152	10.86522	.33696	1025.1	1.626	.93668	11.00927	.30716
5	0	.025	.0100	1015.6	1.593	.92152	10.86522	.33696	1021.9	1.626	.93668	11.00927	.30716
6	0	.0125	.0125	1015.6	1.593	.92152	10.86522	.33696	1018.7	1.626	.93668	11.00927	.30716
7	0	.00625	.0150	1015.6	1.593	.92152	10.86522	.33696	1015.5	1.626	.93668	11.00927	.30716
8	0	.003125	.0175	1015.6	1.593	.92152	10.86522	.33696	1012.3	1.626	.93668	11.00927	.30716
9	0	.0015625	.0200	1015.6	1.593	.92152	10.86522	.33696	1009.1	1.626	.93668	11.00927	.30716
10	0	.00078125	.0225	1015.6	1.593	.92152	10.86522	.33696	1005.9	1.626	.93668	11.00927	.30716
11	0	.000390625	.0250	1015.6	1.593	.92152	10.86522	.33696	1002.7	1.626	.93668	11.00927	.30716
12	0	.0001953125	.0275	1015.6	1.593	.92152	10.86522	.33696	999.5	1.626	.93668	11.00927	.30716
13	0	.00009765625	.0300	1015.6	1.593	.92152	10.86522	.33696	996.3	1.626	.93668	11.00927	.30716
14	0	.000048828125	.0325	1015.6	1.593	.92152	10.86522	.33696	993.1	1.626	.93668	11.00927	.30716
15	0	.0000244140625	.0350	1015.6	1.593	.92152	10.86522	.33696	989.9	1.626	.93668	11.00927	.30716
16	0	.00001220703125	.0375	1015.6	1.593	.92152	10.86522	.33696	986.7	1.626	.93668	11.00927	.30716
17	0	.000006103515625	.0400	1015.6	1.593	.92152	10.86522	.33696	983.5	1.626	.93668	11.00927	.30716
18	0	.0000030517578125	.0425	1015.6	1.593	.92152	10.86522	.33696	980.3	1.626	.93668	11.00927	.30716
19	0	.00000152587890625	.0450	1015.6	1.593	.92152	10.86522	.33696	977.1	1.626	.93668	11.00927	.30716
20	0	.000000762939453125	.0475	1015.6	1.593	.92152	10.86522	.33696	973.9	1.626	.93668	11.00927	.30716
21	0	.0000003814697265625	.0500	1015.6	1.593	.92152	10.86522	.33696	970.7	1.626	.93668	11.00927	.30716
22	0	.00000019073486328125	.0525	1015.6	1.593	.92152	10.86522	.33696	967.5	1.626	.93668	11.00927	.30716
23	0	.000000095367431640625	.0550	1015.6	1.593	.92152	10.86522	.33696	964.3	1.626	.93668	11.00927	.30716
24	0	.0000000476837158203125	.0575	1015.6	1.593	.92152	10.86522	.33696	961.1	1.626	.93668	11.00927	.30716
25	0	.00000002384185791015625	.0600	1015.6	1.593	.92152	10.86522	.33696	957.9	1.626	.93668	11.00927	.30716
26	0	.000000011920928955078125	.0625	1015.6	1.593	.92152	10.86522	.33696	954.7	1.626	.93668	11.00927	.30716
27	0	.0000000059604644775390625	.0650	1015.6	1.593	.92152	10.86522	.33696	951.5	1.626	.93668	11.00927	.30716
28	0	.00000000298023223876953125	.0675	1015.6	1.593	.92152	10.86522	.33696	948.3	1.626	.93668	11.00927	.30716
29	0	.000000001490116119384765625	.0700	1015.6	1.593	.92152	10.86522	.33696	945.1	1.626	.93668	11.00927	.30716
30	0	.0000000007450580596923828125	.0725	1015.6	1.593	.92152	10.86522	.33696	941.9	1.626	.93668	11.00927	.30716
31	0	.00000000037252902984619140625	.0750	1015.6	1.593	.92152	10.86522	.33696	938.7	1.626	.93668	11.00927	.30716
32	0	.000000000186264514923095703125	.0775	1015.6	1.593	.92152	10.86522	.33696	935.5	1.626	.93668	11.00927	.30716
33	0	.0000000000931322574615478515625	.0800	1015.6	1.593	.92152	10.86522	.33696	932.3	1.626	.93668	11.00927	.30716
34	0	.00000000004656612873077392578125	.0825	1015.6	1.593	.92152	10.86522	.33696	929.1	1.626	.93668	11.00927	.30716
35	0	.000000000023283064365386962890625	.0850	1015.6	1.593	.92152	10.86522	.33696	925.9	1.626	.93668	11.00927	.30716
36	0	.0000000000116415321826934848125	.0875	1015.6	1.593	.92152	10.86522	.33696	922.7	1.626	.93668	11.00927	.30716
37	0	.0000000000058207660913467424240625	.0900	1015.6	1.593	.92152	10.86522	.33696	919.5	1.626	.93668	11.00927	.30716
38	0	.00000000000291038304567312371213125	.0925	1015.6	1.593	.92152	10.86522	.33696	916.3	1.626	.93668	11.00927	.30716
39	0	.0000000000014551915228365618560625	.0950	1015.6	1.593	.92152	10.86522	.33696	913.1	1.626	.93668	11.00927	.30716
40	0	.00000000000072759576141828092803125	.0975	1015.6	1.593	.92152	10.86522	.33696	909.9	1.626	.93668	11.00927	.30716
41	0	.000000000000363797880709140464015625	.1000	1015.6	1.593	.92152	10.86522	.33696	906.7	1.626	.93668	11.00927	.30716
42	0	.0000000000001818989403545702320078125	.1025	1015.6	1.593	.92152	10.86522	.33696	903.5	1.626	.93668	11.00927	.30716
43	0	.00000000000009094947017728511600390625	.1050	1015.6	1.593	.92152	10.86522	.33696	900.3	1.626	.93668	11.00927	.30716
44	0	.000000000000045474735088642578001953125	.1075	1015.6	1.593	.92152	10.86522	.33696	897.1	1.626	.93668	11.00927	.30716
45	0	.0000000000000227373675443212890009765625	.1100	1015.6	1.593	.92152	10.86522	.33696	893.9	1.626	.93668	11.00927	.30716
46	0	.00000000000001136868377216064450048828125	.1125	1015.6	1.593	.92152	10.86522	.33696	890.7	1.626	.93668	11.00927	.30716
47	0	.000000000000005684341886080322250244140625	.1150	1015.6	1.593	.92152	10.86522	.33696	887.5	1.626	.93668	11.00927	.30716
48	0	.0000000000000028421709430401611251220703125	.1175	1015.6	1.593	.92152	10.86522	.33696	884.3	1.626	.93668	11.00927	.30716
49	0	.0000000000000014210854715200805625603515625	.1200	1015.6	1.593	.92152	10.86522	.33696	881.1	1.626	.93668	11.00927	.30716
50	0	.00000000000000071054273576004028127017578125	.1225	1015.6	1.593	.92152	10.86522	.33696	877.9	1.626	.93668	11.00927	.30716

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE II.- DATA^a FOR 140° CONE; $M_{\infty} = 2.96$ - Continued

(d) $\alpha = 15^\circ$

Orifice 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49	Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0.0^\circ, p_t = 3240.4$ psf				
					p_t , psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}	M_t
1	0	0.030	-0.000	-0.0000	973.6	1.531	.88421	10.39257	.42301
2	0	.220	-0.025	-.0471	930.4	1.456	.84500	9.93181	.49646
3	0	.450	-0.050	-.0943	940.0	1.473	.85372	10.03420	.48075
4	0	.680	-0.075	-.1414	950.0	1.490	.86244	10.13657	.46504
5	0	.850	-0.100	-.1886	935.2	1.465	.84916	9.90317	.47810
6	0	1.000	-0.125	-.2357	927.2	1.451	.84210	9.89768	.53163
7	0	1.200	-0.150	-.2829	919.2	1.437	.83484	9.81236	.51443
8	0	1.400	-0.175	-.3300	912.8	1.426	.82903	9.74410	.52455
9	0	1.600	-0.200	-.3769	906.9	1.414	.82345	9.68105	.53405
10	0	1.800	-0.225	-.4243	898.9	1.396	.81651	9.62347	.54163
11	0	2.000	-0.250	-.4715	888.9	1.384	.80912	9.45812	.57373
12	0	2.200	-0.275	-.5186	880.9	1.370	.80200	9.40260	.57373
13	0	2.400	-0.300	-.5658	871.3	1.353	.79128	9.30041	.58810
14	0	2.600	-0.325	-.6130	861.9	1.336	.78062	9.19846	.60469
15	0	2.800	-0.350	-.6601	848.9	1.314	.77036	9.10050	.62110
16	0	3.000	-0.375	-.7072	836.1	1.292	.75934	8.92498	.63966
17	0	3.200	-0.400	-.7544	823.3	1.270	.74773	8.78846	.65806
18	0	3.400	-0.425	-.8017	807.3	1.242	.73321	8.61781	.68086
19	0	3.600	-0.450	-.8490	791.4	1.214	.71741	8.41916	.70410
20	0	3.800	-0.475	-.8958	761.0	1.169	.69110	8.12293	.74410
21	0	4.000	-0.500	-.9430	713.4	1.089	.65335	7.67924	.80610
22	180	.230	-0.025	-.0471	1031.6	1.632	.93688	11.01174	.30661
23	180	.460	-0.050	-.0943	1046.7	1.644	.94467	11.12615	.29331
24	180	.690	-0.075	-.1414	1078.5	1.694	.97364	11.24110	.28135
25	180	.850	-0.100	-.1886	1087.5	1.730	.98744	11.26835	.27325
26	180	1.000	-0.125	-.2357	1092.3	1.738	.99200	11.26594	.26948
27	180	1.200	-0.150	-.2829	1093.9	1.741	.99345	11.26563	.26997
28	180	1.400	-0.175	-.3300	1095.5	1.744	.99490	11.26538	.26953
29	180	1.600	-0.200	-.3769	1097.1	1.746	.99635	11.26513	.26909
30	180	1.800	-0.225	-.4243	1098.7	1.748	.99780	11.26488	.26865
31	180	2.000	-0.250	-.4715	1099.7	1.750	.99925	11.26464	.26821
32	180	2.200	-0.275	-.5186	1099.7	1.750	.99925	11.26440	.26777
33	180	2.400	-0.300	-.5658	1098.9	1.747	.99819	11.26415	.26733
34	180	2.600	-0.325	-.6130	1097.2	1.743	.99674	11.26390	.26689
35	180	2.800	-0.350	-.6601	1094.7	1.738	.99479	11.26365	.26645
36	180	3.000	-0.375	-.7072	1091.2	1.694	.98879	11.26340	.26601
37	180	3.200	-0.400	-.7544	1085.5	1.674	.98664	11.26315	.26557
38	180	3.400	-0.425	-.8015	1078.5	1.649	.98559	11.26290	.26513
39	180	3.600	-0.450	-.8486	1071.2	1.626	.98454	11.26265	.26469
40	180	3.800	-0.475	-.8958	1062.7	1.593	.98349	11.26240	.26425
41	180	4.000	-0.500	-.9430	1051.4	1.546	.98244	11.26215	.26381
42	270	1.000	-0.125	-.2357	982.1	1.456	.83193	10.48331	.40754
43	270	1.200	-0.150	-.2829	964.5	1.516	.87597	10.29580	.43909
44	270	1.400	-0.175	-.3300	947.1	1.581	.92001	9.89556	.51097
45	270	1.600	-0.200	-.3769	930.4	1.646	.96405	9.49532	.58286
46	90	1.000	-0.125	-.2357	973.6	1.531	.88421	10.39257	.42301
47	90	1.200	-0.150	-.2829	956.0	1.501	.86523	10.20445	.45345
48	90	1.400	-0.175	-.3300	938.4	1.473	.84625	10.01633	.48389
49	90	1.600	-0.200	-.3769	920.8	1.443	.82728	9.82803	.51433
					781.7	1.198	.67098	8.34477	.71698

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².
Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE II.- DATA^a FOR 140° CONE; $M_{\infty} = 2.96$ - Continued(e) $\alpha = 20^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ$, $p_t = 3242.3$ psf				$\Phi = 22.5^\circ$, $p_t = 3241.6$ psf				$\Phi = 45.0^\circ$, $p_t = 3242.3$ psf						
				$p_{t,1}$ psf	C_p	$p_{t,1}/p_{t,2}$	$p_{t,1}/p_\infty$	$M_{t,1}$	$p_{t,1}$ psf	C_p	$p_{t,1}/p_{t,2}$	$p_{t,1}/p_\infty$	$M_{t,1}$	$p_{t,1}$ psf	C_p	$p_{t,1}/p_{t,2}$	$p_{t,1}/p_\infty$	$M_{t,1}$
1	0	-0.00	-0.000	882.1	1.371	.80065	9.41049	.57264	883.1	1.373	.80171	9.42297	.57088	881.5	1.370	.80039	9.43039	.57358
2	0	-0.20	-0.025	884.7	1.271	.74853	9.41049	.65680	827.2	1.279	.74853	9.41049	.65680	827.2	1.279	.74853	9.41049	.65680
3	0	-0.40	-0.050	887.4	1.316	.77169	9.07014	.61991	847.9	1.312	.77037	9.13329	.61125	854.3	1.323	.77545	9.11428	.61387
4	0	-0.60	-0.075	890.1	1.335	.78833	9.07014	.65049	855.9	1.326	.77707	9.13329	.61125	854.3	1.323	.77545	9.11428	.61387
5	0	-0.80	-0.100	892.8	1.351	.80444	9.07014	.68125	859.5	1.315	.77127	9.06513	.62060	852.7	1.320	.77400	9.09725	.61749
6	0	-1.00	-0.125	895.5	1.369	.82051	9.07014	.71200	863.2	1.301	.76692	9.01401	.62958	847.9	1.312	.76855	9.07207	.62108
7	0	-1.20	-0.150	898.2	1.387	.83658	9.07014	.74275	866.9	1.289	.76465	8.92899	.63751	844.8	1.306	.76978	9.02707	.62469
8	0	-1.40	-0.175	900.9	1.405	.85265	9.07014	.77350	870.6	1.279	.76238	8.84361	.64575	841.6	1.301	.77385	8.97799	.62830
9	0	-1.60	-0.200	903.6	1.423	.86872	9.07014	.80425	874.3	1.265	.76011	8.75842	.65399	838.4	1.292	.77590	8.92689	.63191
10	0	-1.80	-0.225	906.3	1.441	.88479	9.07014	.83500	878.0	1.251	.75784	8.67323	.66224	835.1	1.277	.77801	8.87584	.63552
11	0	-2.00	-0.250	909.0	1.459	.90086	9.07014	.86575	881.7	1.237	.75557	8.58804	.67049	831.8	1.262	.78012	8.82467	.63913
12	0	-2.20	-0.275	911.7	1.477	.91693	9.07014	.89650	885.4	1.223	.75330	8.50285	.67874	828.5	1.248	.78223	8.77350	.64274
13	0	-2.40	-0.300	914.4	1.495	.93299	9.07014	.92725	889.1	1.209	.75103	8.41766	.68700	825.2	1.234	.78434	8.72233	.64635
14	0	-2.60	-0.325	917.1	1.513	.94906	9.07014	.95800	892.8	1.195	.74876	8.33247	.69525	821.9	1.220	.78645	8.67116	.64996
15	0	-2.80	-0.350	919.8	1.531	.96513	9.07014	.98875	896.5	1.181	.74648	8.24728	.70350	818.6	1.206	.78856	8.62000	.65357
16	0	-3.00	-0.375	922.5	1.549	.98120	9.07014	.10150	900.2	1.167	.74420	8.16209	.71175	815.3	1.192	.79067	8.56883	.65718
17	0	-3.20	-0.400	925.2	1.567	.99727	9.07014	.10425	903.9	1.153	.74192	8.07690	.71988	812.0	1.178	.79278	8.51766	.66079
18	0	-3.40	-0.425	927.9	1.585	.10134	9.07014	.10700	907.6	1.139	.73964	7.99171	.72800	808.7	1.164	.79489	8.46649	.66440
19	0	-3.60	-0.450	930.6	1.603	.10341	9.07014	.10975	911.3	1.125	.73736	7.90652	.73612	805.4	1.150	.79700	8.41532	.66801
20	0	-3.80	-0.475	933.3	1.621	.10548	9.07014	.11250	915.0	1.111	.73508	7.82133	.74425	802.1	1.136	.79911	8.36415	.67162
21	0	-4.00	-0.500	936.0	1.639	.10755	9.07014	.11525	918.7	1.097	.73280	7.73614	.75238	798.8	1.122	.80122	8.31298	.67523
22	180	-0.20	-0.025	938.7	1.657	.10962	9.07014	.11800	922.4	1.083	.73052	7.65095	.76050	795.5	1.108	.80333	8.26181	.67884
23	180	-0.40	-0.050	941.4	1.675	.11169	9.07014	.12075	926.1	1.069	.72824	7.56576	.76875	792.2	1.094	.80544	8.21064	.68245
24	180	-0.60	-0.075	944.1	1.693	.11376	9.07014	.12350	929.8	1.055	.72596	7.48057	.77700	788.9	1.080	.80755	8.15947	.68606
25	180	-0.80	-0.100	946.8	1.711	.11583	9.07014	.12625	933.5	1.041	.72368	7.39538	.78525	785.6	1.066	.80966	8.10830	.68967
26	180	-1.00	-0.125	949.5	1.729	.11790	9.07014	.12900	937.2	1.027	.72140	7.31019	.79350	782.3	1.052	.81177	8.05713	.69328
27	180	-1.20	-0.150	952.2	1.747	.11997	9.07014	.13175	940.9	1.013	.71912	7.22500	.80175	779.0	1.038	.81388	8.00596	.69689
28	180	-1.40	-0.175	954.9	1.765	.12204	9.07014	.13450	944.6	1.000	.71684	7.13981	.81000	775.7	1.024	.81600	7.95479	.70050
29	180	-1.60	-0.200	957.6	1.783	.12411	9.07014	.13725	948.3	0.986	.71456	7.05462	.81825	772.4	1.010	.81811	7.90362	.70411
30	180	-1.80	-0.225	960.3	1.801	.12618	9.07014	.14000	952.0	0.972	.71228	6.96943	.82650	769.1	0.996	.82022	7.85245	.70772
31	180	-2.00	-0.250	963.0	1.819	.12825	9.07014	.14275	955.7	0.958	.71000	6.88424	.83475	765.8	0.982	.82233	7.80128	.71133
32	180	-2.20	-0.275	965.7	1.837	.13032	9.07014	.14550	959.4	0.944	.70772	6.79905	.84300	762.5	0.968	.82444	7.75011	.71494
33	180	-2.40	-0.300	968.4	1.855	.13239	9.07014	.14825	963.1	0.930	.70544	6.71386	.85125	759.2	0.954	.82655	7.69894	.71855
34	180	-2.60	-0.325	971.1	1.873	.13446	9.07014	.15100	966.8	0.916	.70316	6.62867	.85950	755.9	0.940	.82866	7.64777	.72216
35	180	-2.80	-0.350	973.8	1.891	.13653	9.07014	.15375	970.5	0.902	.70088	6.54348	.86775	752.6	0.926	.83077	7.59660	.72577
36	180	-3.00	-0.375	976.5	1.909	.13860	9.07014	.15650	974.2	0.888	.69860	6.45829	.87600	749.3	0.912	.83288	7.54543	.72938
37	180	-3.20	-0.400	979.2	1.927	.14067	9.07014	.15925	977.9	0.874	.69632	6.37310	.88425	746.0	0.898	.83500	7.49426	.73299
38	180	-3.40	-0.425	981.9	1.945	.14274	9.07014	.16200	981.6	0.860	.69404	6.28791	.89250	742.7	0.884	.83711	7.44309	.73660
39	180	-3.60	-0.450	984.6	1.963	.14481	9.07014	.16475	985.3	0.846	.69176	6.20272	.90075	739.4	0.870	.83922	7.39192	.74021
40	180	-3.80	-0.475	987.3	1.981	.14688	9.07014	.16750	989.0	0.832	.68948	6.11753	.90900	736.1	0.856	.84133	7.34075	.74382
41	180	-4.00	-0.500	990.0	2.000	.14895	9.07014	.17025	992.7	0.818	.68720	6.03234	.91725	732.8	0.842	.84344	7.28958	.74743
42	270	-0.20	-0.025	992.7	1.999	.15102	9.07014	.17300	996.4	0.804	.68492	5.94715	.92550	729.5	0.828	.84555	7.23841	.75104
43	270	-0.40	-0.050	995.4	2.017	.15309	9.07014	.17575	1000.1	0.790	.68264	5.86196	.93375	726.2	0.814	.84766	7.18724	.75465
44	270	-0.60	-0.075	998.1	2.035	.15516	9.07014	.17850	1003.8	0.776	.68036	5.77677	.94200	722.9	0.800	.84977	7.13607	.75826
45	270	-0.80	-0.100	1000.8	2.053	.15723	9.07014	.18125	1007.5	0.762	.67808	5.69158	.95025	719.6	0.786	.85188	7.08490	.76187
46	270	-1.00	-0.125	1003.5	2.071	.15930	9.07014	.18400	1011.2	0.748	.67580	5.60639	.95850	716.3	0.772	.85400	7.03373	.76548
47	90	-2.00	-0.250	1006.2	2.089	.16137	9.07014	.18675	1014.9	0.734	.67352	5.52120	.96675	713.0	0.758	.85611	6.98256	.76909
48	90	-2.50	-0.375	1008.9	2.107	.16344	9.07014	.18950	1018.6	0.720	.67124	5.43601	.97500	709.7	0.744	.85822	6.93139	.77270
49	90	-3.00	-0.500	1011.6	2.125	.16551	9.07014	.19225	1022.3	0.706	.66896	5.35082	.98325	706.4	0.730	.86033	6.88022	.77631

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE II.- DATA^a FOR 140° CONE; $M_{\infty} = 2.96$ - Concluded

(e) $\alpha = 20^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ, p_t = 3244.3$ psf				$\Phi = 90.0^\circ, p_t = 3242.1$ psf					
				p_{tL} psf	C_p	$p_L/p_{tL,2}$	p_L/p_{∞}	M_L	p_{tL} psf	C_p	$p_L/p_{tL,2}$	p_L/p_{∞}	M_L
1	0	.000	-0.000	879.8	1.366	.79809	9.38042	.57688	879.8	1.367	.79863	9.38679	.57599
2	0	.000	-0.000	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
3	0	.050	-0.043	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
4	0	.100	-0.086	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
5	0	.150	-0.123	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
6	0	.200	-0.160	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
7	0	.250	-0.197	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
8	0	.300	-0.234	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
9	0	.350	-0.271	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
10	0	.400	-0.308	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
11	0	.450	-0.345	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
12	0	.500	-0.382	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
13	0	.550	-0.419	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
14	0	.600	-0.456	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
15	0	.650	-0.493	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
16	0	.700	-0.530	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
17	0	.750	-0.567	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
18	0	.800	-0.604	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
19	0	.850	-0.641	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
20	0	.900	-0.678	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
21	0	.950	-0.715	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
22	180	.000	-0.000	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
23	180	.050	-0.043	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
24	180	.100	-0.086	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
25	180	.150	-0.123	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
26	180	.200	-0.160	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
27	180	.250	-0.197	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
28	180	.300	-0.234	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
29	180	.350	-0.271	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
30	180	.400	-0.308	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
31	180	.450	-0.345	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
32	180	.500	-0.382	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
33	180	.550	-0.419	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
34	180	.600	-0.456	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
35	180	.650	-0.493	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
36	180	.700	-0.530	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
37	180	.750	-0.567	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
38	180	.800	-0.604	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
39	180	.850	-0.641	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
40	180	.900	-0.678	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
41	180	.950	-0.715	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
42	270	.000	-0.000	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
43	270	.050	-0.043	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
44	270	.100	-0.086	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
45	270	.150	-0.123	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
46	270	.200	-0.160	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
47	270	.250	-0.197	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
48	270	.300	-0.234	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317
49	270	.350	-0.271	884.5	1.316	.77057	9.05696	.62172	875.0	1.359	.79428	9.33568	.58317

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².
Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE III.- DATA^a FOR 140° CONE; $M_{\infty} = 3.95$ (a) $\alpha = 0^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ, P_t = 5775.8 \text{ psf}$					$\Phi = 22.5^\circ, P_t = 5775.8 \text{ psf}$					$\Phi = 45.0^\circ, P_t = 5775.8 \text{ psf}$				
				$P_{t,1}$ psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	$P_{t,1}$ psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	$P_{t,1}$ psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t
1	0	.000	.0000	819.1	1.750	.97822	20.11538	.17766	815.9	1.747	.97671	20.08447	.18378	815.9	1.747	.97671	20.08447	.18378
2	0	.000	.0000	814.9	1.743	.97650	20.09521	.17766	815.3	1.740	.97629	20.08586	.18378	815.9	1.747	.97671	20.08447	.18378
3	0	.000	.0000	810.7	1.735	.97478	20.07504	.17766	810.5	1.733	.97457	20.06586	.18378	815.9	1.747	.97671	20.08447	.18378
4	0	.000	.0000	806.5	1.727	.97306	20.05487	.17766	810.5	1.733	.97457	20.06586	.18378	815.9	1.747	.97671	20.08447	.18378
5	0	.000	.0000	802.3	1.719	.97134	20.03470	.17766	802.5	1.725	.97285	20.04587	.18378	815.9	1.747	.97671	20.08447	.18378
6	0	.000	.0000	798.1	1.711	.96962	20.01453	.17766	802.5	1.725	.97285	20.04587	.18378	815.9	1.747	.97671	20.08447	.18378
7	0	.000	.0000	793.9	1.703	.96790	19.99436	.17766	797.2	1.704	.96958	19.97419	.18378	815.9	1.747	.97671	20.08447	.18378
8	0	.000	.0000	789.7	1.695	.96618	19.97419	.17766	792.9	1.693	.96804	19.95402	.18378	815.9	1.747	.97671	20.08447	.18378
9	0	.000	.0000	785.5	1.687	.96446	19.95402	.17766	788.1	1.693	.96804	19.95402	.18378	815.9	1.747	.97671	20.08447	.18378
10	0	.000	.0000	781.3	1.679	.96274	19.93385	.17766	785.9	1.687	.96957	19.92587	.18378	815.9	1.747	.97671	20.08447	.18378
11	0	.000	.0000	777.1	1.671	.96102	19.91368	.17766	778.9	1.687	.96957	19.92587	.18378	815.9	1.747	.97671	20.08447	.18378
12	0	.000	.0000	772.9	1.663	.95930	19.89351	.17766	775.9	1.687	.96957	19.92587	.18378	815.9	1.747	.97671	20.08447	.18378
13	0	.000	.0000	768.7	1.655	.95758	19.87334	.17766	772.1	1.687	.96957	19.92587	.18378	815.9	1.747	.97671	20.08447	.18378
14	0	.000	.0000	764.5	1.647	.95586	19.85317	.17766	767.3	1.686	.97166	19.89351	.18378	815.9	1.747	.97671	20.08447	.18378
15	0	.000	.0000	760.3	1.639	.95414	19.83300	.17766	763.3	1.686	.97166	19.89351	.18378	815.9	1.747	.97671	20.08447	.18378
16	0	.000	.0000	756.1	1.631	.95242	19.81283	.17766	763.3	1.686	.97166	19.89351	.18378	815.9	1.747	.97671	20.08447	.18378
17	0	.000	.0000	751.9	1.623	.95070	19.79266	.17766	763.3	1.686	.97166	19.89351	.18378	815.9	1.747	.97671	20.08447	.18378
18	0	.000	.0000	747.7	1.615	.94898	19.77249	.17766	763.3	1.686	.97166	19.89351	.18378	815.9	1.747	.97671	20.08447	.18378
19	0	.000	.0000	743.5	1.607	.94726	19.75232	.17766	763.3	1.686	.97166	19.89351	.18378	815.9	1.747	.97671	20.08447	.18378
20	0	.000	.0000	739.3	1.599	.94554	19.73215	.17766	763.3	1.686	.97166	19.89351	.18378	815.9	1.747	.97671	20.08447	.18378
21	180	.025	.0471	620.0	1.304	.79098	18.26517	.58860	618.8	1.298	.79131	16.27196	.58860	684.2	1.449	.81007	16.22222	.54338
22	180	.025	.0471	622.7	1.304	.79130	18.26517	.58860	620.2	1.298	.79161	16.27196	.58860	686.6	1.449	.81007	16.22222	.54338
23	180	.025	.0471	625.4	1.304	.79162	18.26517	.58860	622.5	1.298	.79192	16.27196	.58860	689.0	1.449	.81007	16.22222	.54338
24	180	.025	.0471	628.1	1.304	.79194	18.26517	.58860	624.8	1.298	.79223	16.27196	.58860	691.3	1.449	.81007	16.22222	.54338
25	180	.025	.0471	630.8	1.304	.79226	18.26517	.58860	627.1	1.298	.79254	16.27196	.58860	693.6	1.449	.81007	16.22222	.54338
26	180	.025	.0471	633.5	1.304	.79258	18.26517	.58860	629.4	1.298	.79285	16.27196	.58860	695.9	1.449	.81007	16.22222	.54338
27	180	.025	.0471	636.2	1.304	.79290	18.26517	.58860	631.7	1.298	.79316	16.27196	.58860	698.2	1.449	.81007	16.22222	.54338
28	180	.025	.0471	638.9	1.304	.79322	18.26517	.58860	634.0	1.298	.79347	16.27196	.58860	700.5	1.449	.81007	16.22222	.54338
29	180	.025	.0471	641.6	1.304	.79354	18.26517	.58860	636.3	1.298	.79378	16.27196	.58860	702.8	1.449	.81007	16.22222	.54338
30	180	.025	.0471	644.3	1.304	.79386	18.26517	.58860	638.6	1.298	.79409	16.27196	.58860	705.1	1.449	.81007	16.22222	.54338
31	180	.025	.0471	647.0	1.304	.79418	18.26517	.58860	640.9	1.298	.79440	16.27196	.58860	707.4	1.449	.81007	16.22222	.54338
32	180	.025	.0471	649.7	1.304	.79450	18.26517	.58860	643.2	1.298	.79471	16.27196	.58860	709.7	1.449	.81007	16.22222	.54338
33	180	.025	.0471	652.4	1.304	.79482	18.26517	.58860	645.5	1.298	.79502	16.27196	.58860	712.0	1.449	.81007	16.22222	.54338
34	180	.025	.0471	655.1	1.304	.79514	18.26517	.58860	647.8	1.298	.79533	16.27196	.58860	714.3	1.449	.81007	16.22222	.54338
35	180	.025	.0471	657.8	1.304	.79546	18.26517	.58860	650.1	1.298	.79562	16.27196	.58860	716.6	1.449	.81007	16.22222	.54338
36	180	.025	.0471	660.5	1.304	.79578	18.26517	.58860	652.4	1.298	.79589	16.27196	.58860	718.9	1.449	.81007	16.22222	.54338
37	180	.025	.0471	663.2	1.304	.79610	18.26517	.58860	654.7	1.298	.79619	16.27196	.58860	721.2	1.449	.81007	16.22222	.54338
38	180	.025	.0471	665.9	1.304	.79642	18.26517	.58860	657.0	1.298	.79649	16.27196	.58860	723.5	1.449	.81007	16.22222	.54338
39	180	.025	.0471	668.6	1.304	.79674	18.26517	.58860	659.3	1.298	.79679	16.27196	.58860	725.8	1.449	.81007	16.22222	.54338
40	180	.025	.0471	671.3	1.304	.79706	18.26517	.58860	661.6	1.298	.79709	16.27196	.58860	728.1	1.449	.81007	16.22222	.54338
41	180	.025	.0471	674.0	1.304	.79738	18.26517	.58860	663.9	1.298	.79740	16.27196	.58860	730.4	1.449	.81007	16.22222	.54338
42	270	.000	.0000	605.1	1.721	.96270	19.79638	.17766	602.8	1.716	.96013	19.78333	.20436	811.2	1.715	.96090	19.78333	.20436
43	270	.000	.0000	607.8	1.721	.96302	19.79638	.17766	605.5	1.716	.96045	19.78333	.20436	813.5	1.715	.96125	19.78333	.20436
44	270	.000	.0000	610.5	1.721	.96334	19.79638	.17766	608.2	1.716	.96077	19.78333	.20436	815.8	1.715	.96157	19.78333	.20436
45	270	.000	.0000	613.2	1.721	.96366	19.79638	.17766	610.9	1.716	.96109	19.78333	.20436	818.1	1.715	.96189	19.78333	.20436
46	90	.125	.2357	795.7	1.700	.95167	19.91368	.17766	792.4	1.686	.95284	19.90840	.28056	790.4	1.688	.95408	19.93401	.28521
47	90	.125	.2357	797.4	1.700	.95199	19.91368	.17766	794.1	1.687	.95316	19.90840	.28056	792.7	1.688	.95437	19.93401	.28521
48	90	.125	.2357	799.1	1.700	.95231	19.91368	.17766	795.8	1.687	.95348	19.90840	.28056	794.4	1.688	.95469	19.93401	.28521
49	90	.125	.2357	800.8	1.700	.95263	19.91368	.17766	797.5	1.687	.95380	19.90840	.28056	796.1	1.688	.95501	19.93401	.28521

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE III.- DATA^a FOR 140° CONE; $M_{\infty} = 3.95$ - Continued

(a) $\alpha = 0^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 67.5^\circ, P_t = 5775.8 \text{ psf}$				$\Phi = 90.0^\circ, P_t = 5775.8 \text{ psf}$			
				P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t
1	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
2	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
3	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
4	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
5	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
6	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
7	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
8	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
9	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
10	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
11	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
12	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
13	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
14	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
15	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
16	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
17	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
18	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
19	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
20	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
21	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
22	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
23	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
24	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
25	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
26	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
27	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
28	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
29	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
30	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
31	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
32	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
33	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
34	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
35	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
36	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
37	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
38	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
39	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
40	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
41	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
42	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
43	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
44	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
45	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
46	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
47	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
48	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155
49	0	-0.00	-0.000	815.1	1.744	0.97467	19.181	815.2	1.744	0.97473	19.155

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE III.- DATA^a FOR 140° CONE; $M_{\infty} = 3.95$ - Continued(b) $\alpha = 5^\circ$

Orifice e , deg	s , in.	s/D	s/k^*	$\phi = 0.0^\circ, p_t = 5775.8 \text{ psf}$	$\phi = 22.5^\circ, p_t = 5766.3 \text{ psf}$	$\phi = 45.0^\circ, p_t = 5775.8 \text{ psf}$	M_L											
				$p_{t, \text{psf}}$	C_p	$p_{t, \text{psf}}$	C_p	$p_{t, \text{psf}}$	C_p	$p_{t, \text{psf}}$	C_p	$p_{t, \text{psf}}$	C_p	$p_{t, \text{psf}}$	C_p	$p_{t, \text{psf}}$	C_p	M_L
1	0	.300	.0000	815.3	1.744	.97480	20.04517	.19129	.97331	19.99386	1.736	.97078	19.96240	.20628	1.711	.96732	19.93806	.22016
2	0	.220	.0025	.00471	1.708	.95659	19.53212	.22528	.95508	19.53964	1.700	.95167	19.50445	.25016	1.674	.94822	19.47722	.26404
3	0	.140	.0050	.00943	1.686	.94422	19.41630	.27182	.94304	19.42376	1.695	.93932	19.39653	.29507	1.648	.93622	19.36344	.30895
4	0	.100	.0075	.01414	1.677	.94022	19.41630	.28752	.93904	19.42376	1.685	.93532	19.39653	.32000	1.623	.93222	19.36344	.33386
5	0	.080	.0100	.01889	1.673	.93822	19.41630	.30322	.93704	19.43020	1.675	.93332	19.39653	.34500	1.608	.92932	19.36344	.35877
6	0	.060	.0125	.02369	1.673	.93822	19.41630	.32892	.93704	19.43020	1.665	.93132	19.39653	.37000	1.593	.92532	19.36344	.38368
7	0	.040	.0150	.02849	1.673	.93822	19.41630	.35462	.93704	19.43020	1.653	.92832	19.39653	.39500	1.578	.92132	19.36344	.40659
8	0	.020	.0175	.03329	1.673	.93822	19.41630	.38032	.93704	19.43020	1.641	.92332	19.39653	.42000	1.563	.91632	19.36344	.42950
9	0	.010	.0200	.03809	1.673	.93822	19.41630	.40602	.93704	19.43020	1.629	.91832	19.39653	.44500	1.548	.90932	19.36344	.45241
10	0	.005	.0225	.04289	1.673	.93822	19.41630	.43172	.93704	19.43020	1.617	.91332	19.39653	.47000	1.533	.90432	19.36344	.47532
11	0	.000	.0250	.04769	1.673	.93822	19.41630	.45742	.93704	19.43020	1.605	.90832	19.39653	.49500	1.518	.89932	19.36344	.48023
12	0	.270	.0275	.05249	1.673	.93822	19.41630	.48312	.93704	19.43020	1.593	.90332	19.39653	.52000	1.503	.89432	19.36344	.49514
13	0	.250	.0300	.05729	1.673	.93822	19.41630	.50882	.93704	19.43020	1.581	.89832	19.39653	.54500	1.488	.88932	19.36344	.51005
14	0	.230	.0325	.06209	1.673	.93822	19.41630	.53452	.93704	19.43020	1.569	.89332	19.39653	.57000	1.473	.88432	19.36344	.52496
15	0	.210	.0350	.06689	1.673	.93822	19.41630	.56022	.93704	19.43020	1.557	.88832	19.39653	.59500	1.458	.87932	19.36344	.53987
16	0	.190	.0375	.07169	1.673	.93822	19.41630	.58592	.93704	19.43020	1.545	.88332	19.39653	.62000	1.443	.87432	19.36344	.55478
17	0	.170	.0400	.07649	1.673	.93822	19.41630	.61162	.93704	19.43020	1.533	.87832	19.39653	.64500	1.428	.86932	19.36344	.56969
18	0	.150	.0425	.08129	1.673	.93822	19.41630	.63732	.93704	19.43020	1.521	.87332	19.39653	.67000	1.413	.86432	19.36344	.58460
19	0	.130	.0450	.08609	1.673	.93822	19.41630	.66302	.93704	19.43020	1.509	.86832	19.39653	.69500	1.398	.85932	19.36344	.59951
20	0	.110	.0475	.09089	1.673	.93822	19.41630	.68872	.93704	19.43020	1.497	.86332	19.39653	.72000	1.383	.85432	19.36344	.61442
21	0	.090	.0500	.09569	1.673	.93822	19.41630	.71442	.93704	19.43020	1.485	.85832	19.39653	.74500	1.368	.84932	19.36344	.62933
22	180	.025	.0525	.0471	1.783	.95553	20.47133	.08006	.95435	20.47887	1.778	.95167	20.45160	.09974	1.761	.94772	20.42487	.11313
23	180	.050	.0550	.0943	1.783	.95553	20.47133	.08006	.95435	20.47887	1.778	.95167	20.45160	.09974	1.761	.94772	20.42487	.11313
24	180	.075	.0575	.1414	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
25	180	.100	.0600	.1885	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
26	180	.125	.0625	.2357	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
27	180	.150	.0650	.2829	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
28	180	.175	.0675	.3300	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
29	180	.200	.0700	.3772	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
30	180	.225	.0725	.4243	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
31	180	.250	.0750	.4715	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
32	180	.275	.0775	.5186	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
33	180	.300	.0800	.5658	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
34	180	.325	.0825	.6129	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
35	180	.350	.0850	.6601	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
36	180	.375	.0875	.7072	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
37	180	.400	.0900	.7544	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
38	180	.425	.0925	.8015	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
39	180	.450	.0950	.8487	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
40	180	.475	.0975	.8958	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
41	180	.500	.1000	.9430	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
42	270	.025	.1025	.2357	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
43	270	.050	.1050	.4715	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
44	270	.075	.1075	.7072	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
45	270	.100	.1100	.9430	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
46	270	.125	.1125	.1186	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
47	270	.150	.1150	.1430	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
48	270	.175	.1175	.1674	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
49	270	.200	.1200	.1918	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
50	270	.225	.1225	.2162	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
51	270	.250	.1250	.2406	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
52	270	.275	.1275	.2650	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
53	270	.300	.1300	.2894	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
54	270	.325	.1325	.3138	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
55	270	.350	.1350	.3382	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
56	270	.375	.1375	.3626	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
57	270	.400	.1400	.3870	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
58	270	.425	.1425	.4114	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
59	270	.450	.1450	.4358	1.776	.95167	20.35289	.10710	.95050	20.35941	1.775	.94772	20.33306	.12642	1.754	.94380	20.30633	.13951
60	270	.475	.1475	.4602	1.776	.95167	20.35289	.1										

TABLE III.- DATA^a FOR 140° CONE; $M_{\infty} = 3.95$ - Continued

(b) $\alpha = 5^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ$, $P_t = 5775.8$ psf					$\phi = 90.0^\circ$, $P_t = 5775.8$ psf				
				P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t/ρ_{∞}	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t
1	0	-0.20	-0.000	811.7	1.716	.97987	19.95833	19.95833	20.100	813.4	1.733	.98893	19.92448
2	0	-0.20	-0.025	801.1	1.706	.95917	19.72550	19.72550	19.909	805.6	1.722	.96893	19.76589
3	0	-0.50	-0.043	798.9	1.707	.95559	19.64393	19.64393	19.896	805.6	1.722	.96893	19.76589
4	0	-0.50	-0.075	794.2	1.696	.94556	19.52607	19.52607	19.879	800.8	1.711	.95747	19.68859
5	0	-1.00	-0.186	781.0	1.689	.94574	19.44749	19.44749	19.844	799.2	1.708	.95556	19.66939
6	0	-1.50	-0.289	778.2	1.680	.93953	19.33119	19.33119	19.825	788.0	1.682	.94218	19.61810
7	0	-1.50	-0.289	778.2	1.680	.93953	19.33119	19.33119	19.825	788.0	1.682	.94218	19.61810
8	0	-1.75	-0.330	773.4	1.669	.92472	19.01532	19.01532	19.825	783.2	1.672	.93644	19.57430
9	0	-2.00	-0.372	768.6	1.639	.91899	18.89746	18.89746	19.825	778.4	1.661	.93071	19.53851
10	0	-2.25	-0.423	763.8	1.628	.91366	18.77960	18.77960	19.825	772.0	1.646	.92307	19.50131
11	0	-2.50	-0.474	759.0	1.614	.90842	18.66161	18.66161	19.825	766.8	1.632	.91577	19.46412
12	0	-2.75	-0.518	754.4	1.596	.90366	18.54201	18.54201	19.825	761.6	1.616	.90857	19.42742
13	0	-3.00	-0.565	749.8	1.581	.89842	18.42685	18.42685	19.825	756.4	1.600	.90222	19.39061
14	0	-3.25	-0.612	745.2	1.560	.89266	18.31313	18.31313	19.825	751.2	1.582	.89522	19.35394
15	0	-3.50	-0.658	740.6	1.542	.88740	18.20069	18.20069	19.825	746.0	1.560	.88870	19.31720
16	0	-3.75	-0.707	736.0	1.522	.88174	18.08937	18.08937	19.825	740.8	1.536	.88222	19.28046
17	0	-4.00	-0.754	731.5	1.498	.87566	17.97917	17.97917	19.825	735.6	1.508	.87566	19.24372
18	0	-4.25	-0.801	727.0	1.475	.86915	17.87038	17.87038	19.825	730.4	1.477	.86915	19.20700
19	0	-4.50	-0.848	722.5	1.451	.86223	17.76281	17.76281	19.825	725.2	1.451	.86223	19.17028
20	0	-4.75	-0.893	718.0	1.428	.85496	17.65637	17.65637	19.825	720.0	1.428	.85496	19.13356
21	0	-5.00	-0.937	713.5	1.404	.84734	17.55108	17.55108	19.825	714.8	1.404	.84734	19.09684
22	180	-0.25	-0.043	816.3	1.746	.97986	20.07078	20.07078	19.843	810.2	1.732	.96869	19.91952
23	180	-0.50	-0.075	813.1	1.739	.97253	19.99238	19.99238	19.843	805.4	1.722	.96297	19.88188
24	180	-0.75	-0.144	809.5	1.722	.96270	19.79818	19.79818	19.843	800.6	1.704	.95146	19.72345
25	180	-1.00	-0.235	805.1	1.701	.94988	19.67877	19.67877	19.843	795.8	1.689	.93981	19.64898
26	180	-1.25	-0.289	800.4	1.676	.93127	19.56117	19.56117	19.843	791.0	1.678	.93009	19.61134
27	180	-1.50	-0.330	795.6	1.649	.90584	19.44749	19.44749	19.843	786.2	1.650	.92483	19.57370
28	180	-1.75	-0.372	790.8	1.624	.88214	19.33119	19.33119	19.843	781.4	1.632	.91149	19.53606
29	180	-2.00	-0.423	786.0	1.596	.85740	19.21532	19.21532	19.843	776.6	1.610	.89386	19.49842
30	180	-2.25	-0.474	781.2	1.571	.83117	19.09152	19.09152	19.843	771.8	1.592	.88432	19.46078
31	180	-2.50	-0.518	776.4	1.542	.80214	18.96876	18.96876	19.843	767.0	1.571	.87478	19.42314
32	180	-2.75	-0.565	771.7	1.513	.77119	18.84749	18.84749	19.843	762.2	1.550	.86524	19.38550
33	180	-3.00	-0.612	767.0	1.484	.73916	18.72812	18.72812	19.843	757.4	1.529	.85570	19.34786
34	180	-3.25	-0.658	762.2	1.454	.70613	18.60937	18.60937	19.843	752.6	1.508	.84616	19.31022
35	180	-3.50	-0.707	757.5	1.424	.67310	18.49061	18.49061	19.843	747.8	1.488	.83662	19.27258
36	180	-3.75	-0.754	752.8	1.394	.64007	18.37185	18.37185	19.843	743.0	1.468	.82708	19.23494
37	180	-4.00	-0.801	748.0	1.364	.60704	18.25309	18.25309	19.843	738.2	1.448	.81754	19.19730
38	180	-4.25	-0.848	743.2	1.334	.57401	18.13433	18.13433	19.843	733.4	1.428	.80800	19.15966
39	180	-4.50	-0.893	738.4	1.304	.54098	18.01557	18.01557	19.843	728.6	1.408	.79846	19.12202
40	180	-4.75	-0.937	733.6	1.274	.50795	17.89681	17.89681	19.843	723.8	1.388	.78892	19.08438
41	180	-5.00	-0.980	728.8	1.244	.47492	17.77805	17.77805	19.843	719.0	1.368	.77938	19.04674
42	270	-2.00	-0.518	776.4	1.596	.85740	19.21532	19.21532	19.843	771.8	1.571	.83117	19.09152
43	270	-2.25	-0.565	771.7	1.566	.82437	19.09152	19.09152	19.843	767.0	1.550	.80214	19.04718
44	270	-2.50	-0.612	767.0	1.536	.79134	18.96876	18.96876	19.843	762.2	1.529	.77119	19.00284
45	270	-2.75	-0.658	762.2	1.506	.75831	18.84749	18.84749	19.843	757.4	1.508	.74007	18.95850
46	90	-1.25	-0.289	778.2	1.680	.93953	19.33119	19.33119	19.825	788.0	1.682	.94218	19.61810
47	90	-2.00	-0.423	768.6	1.639	.91899	18.89746	18.89746	19.825	778.4	1.661	.93071	19.53851
48	90	-2.50	-0.518	759.0	1.614	.90842	18.66161	18.66161	19.825	766.8	1.632	.91577	19.46412
49	90	-3.00	-0.565	749.8	1.581	.89842	18.42685	18.42685	19.825	756.4	1.600	.89522	19.39061
50	90	-3.50	-0.612	740.6	1.542	.88740	18.31313	18.31313	19.825	746.0	1.560	.88870	19.35394

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE III.- DATA^a FOR 140° CONE; $M_{\infty} = 3.95$ - Continued(c) $\alpha = 10^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, P_t = 5785.3 \text{ psf}$					$\phi = 22.5^\circ, P_t = 5775.8 \text{ psf}$					$\phi = 45.0^\circ, P_t = 5775.8 \text{ psf}$				
				$P_{t,1}$	C_p	$P_{t,1}/P_{t,2}$	$P_{t,1}/\rho_{\infty}$	$M_{t,1}$	$P_{t,1}$, psf	C_p	$P_{t,1}/P_{t,2}$	$P_{t,1}/\rho_{\infty}$	$M_{t,1}$	$P_{t,1}$, psf	C_p	$P_{t,1}/P_{t,2}$	$P_{t,1}/\rho_{\infty}$	$M_{t,1}$
1	0	.000	.0000	781.4	1.665	.93274	19.18025	.31696	1.664	.93243	19.17381	.31773	778.5	1.661	.93064	19.14117	.32162	
2	0	.020	.0000	784.2	1.666	.93031	19.15145	.31924	1.664	.93006	19.15416	.31773	780.9	1.661	.92819	19.11247	.32421	
3	0	.040	.0000	787.0	1.667	.92788	19.12265	.32152	1.664	.92763	19.12586	.31773	783.6	1.661	.92582	19.08376	.32680	
4	0	.060	.0000	789.8	1.668	.92545	19.09385	.32380	1.664	.92520	19.09756	.31773	786.3	1.661	.92345	19.05466	.32939	
5	0	.080	.0000	792.6	1.669	.92302	19.06505	.32608	1.664	.92305	19.06926	.31773	789.0	1.661	.92108	19.02556	.33198	
6	0	.100	.0000	795.4	1.670	.92059	19.03625	.32836	1.664	.92063	19.03996	.31773	791.7	1.661	.91871	19.00000	.33457	
7	0	.120	.0000	798.2	1.671	.91816	19.00745	.33064	1.664	.91819	19.01117	.31773	794.4	1.661	.91634	18.97000	.33716	
8	0	.140	.0000	801.0	1.672	.91573	18.97865	.33292	1.664	.91576	18.98237	.31773	797.1	1.661	.91397	18.94000	.33975	
9	0	.160	.0000	803.8	1.673	.91330	18.94985	.33520	1.664	.91333	18.95308	.31773	799.8	1.661	.91160	18.91000	.34234	
10	0	.180	.0000	806.6	1.674	.91087	18.92105	.33748	1.664	.91090	18.92428	.31773	802.5	1.661	.90923	18.88000	.34493	
11	0	.200	.0000	809.4	1.675	.90844	18.89225	.33976	1.664	.90847	18.89548	.31773	805.2	1.661	.90686	18.85000	.34752	
12	0	.220	.0000	812.2	1.676	.90601	18.86345	.34204	1.664	.90604	18.85369	.31773	807.9	1.661	.90449	18.82000	.35011	
13	0	.240	.0000	815.0	1.677	.90358	18.83465	.34432	1.664	.90361	18.82490	.31773	810.6	1.661	.90212	18.79000	.35270	
14	0	.260	.0000	817.8	1.678	.90115	18.80585	.34660	1.664	.90118	18.76111	.31773	813.3	1.661	.90000	18.76000	.35529	
15	0	.280	.0000	820.6	1.679	.89872	18.77705	.34888	1.664	.89875	18.73232	.31773	816.0	1.661	.89763	18.73000	.35788	
16	0	.300	.0000	823.4	1.680	.89629	18.74825	.35116	1.664	.89632	18.70353	.31773	818.7	1.661	.89526	18.70000	.36047	
17	0	.3200	.375	826.2	1.681	.89386	18.71945	.35344	1.664	.89389	18.67474	.31773	821.4	1.661	.89289	18.67000	.36306	
18	0	.3400	.425	829.0	1.682	.89143	18.69065	.35572	1.664	.89146	18.64595	.31773	824.1	1.661	.89052	18.64000	.36565	
19	0	.3600	.475	831.8	1.683	.88900	18.66185	.35800	1.664	.88903	18.61716	.31773	826.8	1.661	.88815	18.61000	.36824	
20	0	.3800	.525	834.6	1.684	.88657	18.63305	.36028	1.664	.88660	18.58837	.31773	829.5	1.661	.88578	18.58000	.37083	
21	0	.4000	.575	837.4	1.685	.88414	18.60425	.36256	1.664	.88417	18.55958	.31773	832.2	1.661	.88341	18.55000	.37342	
22	0	.4200	.625	840.2	1.686	.88171	18.57545	.36484	1.664	.88174	18.53079	.31773	834.9	1.661	.88104	18.52000	.37601	
23	0	.4400	.675	843.0	1.687	.87928	18.54665	.36712	1.664	.87931	18.50200	.31773	837.6	1.661	.87867	18.49000	.37860	
24	0	.4600	.725	845.8	1.688	.87685	18.51785	.36940	1.664	.87688	18.47321	.31773	840.3	1.661	.87630	18.46000	.38119	
25	0	.4800	.775	848.6	1.689	.87442	18.48905	.37168	1.664	.87445	18.44442	.31773	843.0	1.661	.87393	18.43000	.38378	
26	0	.5000	.825	851.4	1.690	.87199	18.46025	.37396	1.664	.87199	18.41563	.31773	845.7	1.661	.87156	18.40000	.38637	
27	0	.5200	.875	854.2	1.691	.86956	18.43145	.37624	1.664	.86956	18.38684	.31773	848.4	1.661	.86919	18.37000	.38896	
28	0	.5400	.925	857.0	1.692	.86713	18.40265	.37852	1.664	.86713	18.35805	.31773	851.1	1.661	.86682	18.34000	.39155	
29	0	.5600	.975	859.8	1.693	.86470	18.37385	.38080	1.664	.86470	18.32926	.31773	853.8	1.661	.86445	18.31000	.39414	
30	0	.5800	.1025	862.6	1.694	.86227	18.34505	.38308	1.664	.86227	18.30047	.31773	856.5	1.661	.86208	18.28000	.39673	
31	0	.6000	.1075	865.4	1.695	.85984	18.31625	.38536	1.664	.85984	18.27168	.31773	859.2	1.661	.85971	18.25000	.39932	
32	0	.6200	.1125	868.2	1.696	.85741	18.28745	.38764	1.664	.85741	18.24289	.31773	861.9	1.661	.85734	18.22000	.40191	
33	0	.6400	.1175	871.0	1.697	.85498	18.25865	.38992	1.664	.85498	18.21410	.31773	864.6	1.661	.85497	18.19000	.40450	
34	0	.6600	.1225	873.8	1.698	.85255	18.22985	.39220	1.664	.85255	18.18531	.31773	867.3	1.661	.85256	18.16000	.40709	
35	0	.6800	.1275	876.6	1.699	.85012	18.20105	.39448	1.664	.85012	18.15652	.31773	870.0	1.661	.85015	18.13000	.40968	
36	0	.7000	.1325	879.4	1.700	.84769	18.17225	.39676	1.664	.84769	18.12773	.31773	872.7	1.661	.84778	18.10000	.41227	
37	0	.7200	.1375	882.2	1.701	.84526	18.14345	.39904	1.664	.84526	18.09894	.31773	875.4	1.661	.84537	18.07000	.41486	
38	0	.7400	.1425	885.0	1.702	.84283	18.11465	.40132	1.664	.84283	18.07015	.31773	878.1	1.661	.84296	18.04000	.41745	
39	0	.7600	.1475	887.8	1.703	.84040	18.08585	.40360	1.664	.84040	18.04136	.31773	880.8	1.661	.84055	18.01000	.42004	
40	0	.7800	.1525	890.6	1.704	.83797	18.05705	.40588	1.664	.83797	18.01257	.31773	883.5	1.661	.83812	17.98000	.42263	
41	0	.8000	.1575	893.4	1.705	.83554	18.02825	.40816	1.664	.83554	17.98378	.31773	886.2	1.661	.83569	17.95000	.42522	
42	0	.8200	.1625	896.2	1.706	.83311	17.99945	.41044	1.664	.83311	17.95499	.31773	888.9	1.661	.83326	17.92000	.42781	
43	0	.8400	.1675	899.0	1.707	.83068	17.97065	.41272	1.664	.83068	17.92620	.31773	891.6	1.661	.83083	17.89000	.43040	
44	0	.8600	.1725	901.8	1.708	.82825	17.94185	.41500	1.664	.82825	17.89741	.31773	894.3	1.661	.82840	17.86000	.43300	
45	0	.8800	.1775	904.6	1.709	.82582	17.91305	.41728	1.664	.82582	17.86862	.31773	897.0	1.661	.82597	17.83000	.43559	
46	0	.9000	.1825	907.4	1.710	.82339	17.88425	.41956	1.664	.82339	17.83983	.31773	900.0	1.661	.82354	17.80000	.43818	
47	0	.9200	.1875	910.2	1.711	.82096	17.85545	.42184	1.664	.82096	17.81104	.31773	902.7	1.661	.82111	17.77000	.44077	
48	0	.9400	.1925	913.0	1.712	.81853	17.82665	.42412	1.664	.81853	17.78225	.31773	905.4	1.661	.81868	17.74000	.44336	
49	0	.9600	.1975	915.8	1.713	.81610	17.79785	.42640	1.664	.81610	17.75346	.31773	908.1	1.661	.81625	17.71000	.44595	
50	0	.9800	.2025	918.6	1.714	.81367	17.76905	.42868	1.664	.81367	17.72467	.31773	910.8	1.661	.81382	17.68000	.44854	
51	0	1.000	.2075	921.4	1.715	.81124	17.74025	.43096	1.664	.81124	17.69588	.31773	913.5	1.661	.81139	17.65000	.45113	

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE III.- DATA^a FOR 140° CONE; $M_{\infty} = 3.95$ - Continued

(c) $\alpha = 10^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\phi = 67.5^\circ, p_t = 5775.8 \text{ psf}$	$\phi = 90.0^\circ, p_t = 5775.8 \text{ psf}$	M_L	p_t/ρ_{∞}	M_L
				p_t , psf	C_p	$p_t/p_{t,2}$	p_t/ρ_{∞}	M_L
1	0	-0.00	-0.000	776.7	1.657	0.92874	19.09921	12656
2	0	-0.25	-0.471	764.0	1.628	0.91342	19.02061	133565
3	0	-0.50	-0.943	762.8	1.623	0.91342	19.02061	133565
4	0	-0.75	-1.415	762.8	1.623	0.91342	19.02061	133565
5	0	-1.00	-1.886	756.0	1.610	0.90389	18.98131	134893
6	0	-1.25	-2.357	752.8	1.603	0.90007	18.95072	136182
7	0	-1.50	-2.829	748.0	1.592	0.89625	18.92022	137022
8	0	-1.75	-3.302	748.0	1.582	0.89242	18.89069	138259
9	0	-2.00	-3.775	738.4	1.571	0.88859	18.86116	139496
10	0	-2.25	-4.248	733.6	1.560	0.88477	18.83163	140733
11	0	-2.50	-4.715	728.8	1.549	0.88094	18.80210	141970
12	0	-2.75	-5.188	722.4	1.535	0.87711	18.77257	143207
13	0	-3.00	-5.654	716.0	1.523	0.87328	18.74304	144444
14	0	-3.25	-6.121	709.6	1.506	0.86945	18.71351	145681
15	0	-3.50	-6.591	701.6	1.488	0.86562	18.68398	146918
16	0	-3.75	-7.072	692.0	1.466	0.86179	18.65445	148155
17	0	-4.00	-7.544	680.8	1.444	0.85796	18.62492	149392
18	0	-4.25	-8.017	668.9	1.369	0.84822	18.57519	150629
19	0	-4.50	-8.490	654.9	1.315	0.83848	18.52546	151866
20	0	-4.75	-8.958	638.1	1.232	0.82874	18.47573	153103
21	0	-5.00	-9.430	588.1	1.232	0.82874	18.47573	153103
22	180	-0.25	-0.471	784.1	1.696	0.94556	19.21371	131765
23	180	-0.50	-0.943	784.1	1.696	0.94556	19.21371	131765
24	180	-0.75	-1.415	784.1	1.696	0.94556	19.21371	131765
25	180	-1.00	-1.886	791.1	1.696	0.94556	19.21371	131765
26	180	-1.25	-2.357	792.6	1.693	0.94556	19.21371	131765
27	180	-1.50	-2.829	789.2	1.678	0.94002	19.17450	133002
28	180	-1.75	-3.302	784.2	1.660	0.93549	19.13528	134239
29	180	-2.00	-3.775	775.0	1.653	0.93095	19.09606	135476
30	180	-2.25	-4.248	765.6	1.639	0.92642	19.05684	136713
31	180	-2.50	-4.715	755.0	1.626	0.92189	19.01762	137950
32	180	-2.75	-5.188	744.0	1.610	0.91736	18.97840	139187
33	180	-3.00	-5.654	732.8	1.592	0.91283	18.93918	140424
34	180	-3.25	-6.121	721.6	1.574	0.90830	18.90000	141661
35	180	-3.50	-6.591	710.4	1.556	0.90377	18.86082	142898
36	180	-3.75	-7.072	700.0	1.538	0.90000	18.82164	144135
37	180	-4.00	-7.544	688.8	1.523	0.89625	18.78246	145372
38	180	-4.25	-8.017	677.6	1.506	0.89250	18.74328	146609
39	180	-4.50	-8.490	666.4	1.488	0.88875	18.70410	147846
40	180	-4.75	-8.958	655.2	1.471	0.88500	18.66492	149083
41	180	-5.00	-9.430	644.0	1.453	0.88125	18.62574	150320
42	270	-1.25	-2.357	827.6	1.772	0.97250	19.48819	127804
43	270	-1.50	-2.829	827.6	1.772	0.97250	19.48819	127804
44	270	-1.75	-3.302	827.6	1.772	0.97250	19.48819	127804
45	270	-2.00	-3.775	827.6	1.772	0.97250	19.48819	127804
46	90	-1.300	-1.25	739.4	1.571	0.88287	18.73706	149698
47	90	-2.300	-2.50	708.9	1.402	0.80770	16.42689	175382
48	90	-3.300	-3.75	684.4	1.204	0.68795	14.14658	75056
49	90	-4.300	-5.00	575.4	1.204	0.68795	14.14658	75056

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE III.- DATA^a FOR 140° CONE; $M_{\infty} = 3.95$ - Continued(d) $\alpha = 15^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\phi = 0, 0.0^\circ, P_t = 5785.3 \text{ psf}$			
				P_t , psf	C_p	$P_t/P_{t,2}$	M_L
1	0	.030	.000	725.7	1.539	.86628	17.81362
2	0	.200	.025	685.7	1.450	.81858	16.83269
3	0	.400	.050	595.3	1.471	.83003	17.06812
4	0	.600	.075	518.4	1.478	.83384	17.14659
5	0	.800	.100	458.5	1.471	.82816	17.06812
6	0	1.030	.125	423.7	1.460	.82430	17.09046
7	0	1.200	.150	382.9	1.450	.81858	16.83269
8	0	1.400	.175	330.0	1.439	.81285	16.71498
9	0	1.600	.200	276.1	1.428	.80713	16.59727
10	0	1.800	.225	224.2	1.417	.80141	16.47956
11	0	2.030	.250	174.5	1.407	.79568	16.36186
12	0	2.200	.275	126.6	1.396	.78996	15.24414
13	0	2.400	.300	85.7	1.385	.78423	15.12643
14	0	2.600	.325	50.8	1.374	.77850	15.00868
15	0	2.800	.350	26.2	1.364	.77278	14.89093
16	0	3.000	.375	7.72	1.358	.76705	14.77318
17	0	3.200	.400	754.4	1.317	.74798	15.38092
18	0	3.400	.425	801.5	1.292	.73462	15.10626
19	0	3.600	.450	848.6	1.267	.72126	14.83160
20	0	3.800	.475	895.8	1.250	.70790	14.55694
21	0	4.000	.500	943.0	1.151	.66021	13.57402
22	180	.200	.025	781.5	1.665	.93290	19.18352
23	180	.400	.050	694.3	1.733	.96207	19.02737
24	180	.600	.075	617.0	1.772	.98042	19.00442
25	180	.800	.100	558.9	1.776	.99192	20.39717
26	180	1.030	.125	482.5	1.780	.99382	20.43632
27	180	1.200	.150	429.1	1.783	.99573	20.47547
28	180	1.400	.175	382.5	1.786	.99764	20.51462
29	180	1.600	.200	339.5	1.790	.99955	20.55377
30	180	1.800	.225	296.5	1.776	.99192	20.39717
31	180	2.000	.250	253.5	1.772	.99002	20.35802
32	180	2.200	.275	210.5	1.762	.98830	20.24057
33	180	2.400	.300	167.5	1.752	.98658	20.12312
34	180	2.600	.325	124.5	1.740	.98486	20.00567
35	180	2.800	.350	81.5	1.726	.98287	19.84007
36	180	3.000	.375	38.5	1.726	.98287	19.84007
37	180	3.200	.400	754.4	1.701	.95194	19.57502
38	180	3.400	.425	801.5	1.665	.93290	19.18352
39	180	3.600	.450	848.6	1.629	.91486	18.79207
40	180	3.800	.475	895.8	1.525	.85865	17.05567
41	180	4.000	.500	943.0	1.568	.88150	18.12647
42	270	1.030	.125	423.7	1.543	.86817	17.85242
43	270	1.200	.150	382.9	1.543	.86817	17.85242
44	270	1.400	.175	330.0	1.543	.86817	17.85242
45	270	1.600	.200	276.1	1.543	.86817	17.85242
46	90	1.030	.125	423.7	1.514	.85292	17.53896
47	90	1.200	.150	382.9	1.446	.81667	16.79346
48	90	1.400	.175	330.0	1.446	.81667	16.79346
49	90	1.600	.200	276.1	1.446	.81667	16.79346
50	90	1.800	.225	224.2	1.446	.81667	16.79346

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE III. - DATA^a FOR 140° CONE: $M_{\infty} = 3.95$ - Continued

(e) $\alpha = 20^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, P_t = 5775.8 \text{ psf}$					$\phi = 22.5^\circ, P_t = 5775.8 \text{ psf}$					$\phi = 45.0^\circ, P_t = 5775.8 \text{ psf}$						
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,2}$	M_t		
1	0	-0.30	-0.000	645.5	1.342	77182	15.8719	77220	61971	1.342	77220	15.8719	645.8	1.360	77098	15.8533	621.06	1.360	77098	15.8533
2	0	-0.40	-0.000	596.7	1.247	71069	14.6140	71069	71588	1.247	71069	14.6140	596.7	1.263	71033	15.1047	678.63	1.263	71033	15.1047
3	0	-0.50	-0.003	616.7	1.329	73743	15.16406	73743	67425	1.294	73588	15.13274	615.4	1.310	74420	15.30317	663.62	1.310	74420	15.30317
4	0	-0.60	-0.006	631.1	1.359	75463	15.31762	75463	67425	1.294	73588	15.13274	615.4	1.310	74420	15.30317	663.62	1.310	74420	15.30317
5	0	-0.80	-0.010	631.1	1.359	75463	15.31762	75463	67425	1.294	73588	15.13274	615.4	1.310	74420	15.30317	663.62	1.310	74420	15.30317
6	0	-1.00	-0.013	624.7	1.315	74698	15.36048	74698	65923	1.312	74544	15.32866	623.4	1.302	74628	15.32866	659.23	1.302	74628	15.32866
7	0	-1.25	-0.015	624.7	1.315	74698	15.36048	74698	65923	1.312	74544	15.32866	623.4	1.302	74628	15.32866	659.23	1.302	74628	15.32866
8	0	-1.50	-0.017	619.9	1.311	74507	15.32120	74507	65224	1.305	74161	15.25005	617.0	1.295	74037	15.25005	652.24	1.295	74037	15.25005
9	0	-1.60	-0.018	619.9	1.311	74507	15.32120	74507	65224	1.305	74161	15.25005	617.0	1.295	74037	15.25005	652.24	1.295	74037	15.25005
10	0	-1.80	-0.020	615.7	1.297	73163	15.08549	73163	64023	1.283	73077	15.09283	612.8	1.288	73077	15.09283	640.23	1.288	73077	15.09283
11	0	-2.00	-0.022	615.7	1.297	73163	15.08549	73163	64023	1.283	73077	15.09283	612.8	1.288	73077	15.09283	640.23	1.288	73077	15.09283
12	0	-2.25	-0.024	610.4	1.282	72597	15.06235	72597	63620	1.275	72597	15.06235	607.6	1.275	72597	15.06235	636.20	1.275	72597	15.06235
13	0	-2.50	-0.026	610.4	1.282	72597	15.06235	72597	63620	1.275	72597	15.06235	607.6	1.275	72597	15.06235	636.20	1.275	72597	15.06235
14	0	-2.60	-0.027	605.8	1.267	72151	14.94978	72151	62810	1.260	72151	14.94978	604.3	1.260	72151	14.94978	628.10	1.260	72151	14.94978
15	0	-2.80	-0.029	605.8	1.267	72151	14.94978	72151	62810	1.260	72151	14.94978	604.3	1.260	72151	14.94978	628.10	1.260	72151	14.94978
16	0	-3.00	-0.031	598.2	1.252	70872	14.87476	70872	61884	1.245	70872	14.87476	596.9	1.245	70872	14.87476	618.84	1.245	70872	14.87476
17	0	-3.25	-0.033	598.2	1.252	70872	14.87476	70872	61884	1.245	70872	14.87476	596.9	1.245	70872	14.87476	618.84	1.245	70872	14.87476
18	0	-3.50	-0.035	593.0	1.237	70304	14.85593	70304	61476	1.230	70304	14.85593	593.0	1.250	70304	14.85593	614.76	1.250	70304	14.85593
19	0	-3.60	-0.036	593.0	1.237	70304	14.85593	70304	61476	1.230	70304	14.85593	593.0	1.250	70304	14.85593	614.76	1.250	70304	14.85593
20	0	-3.80	-0.038	587.4	1.214	69349	14.78243	69349	60823	1.207	69349	14.78243	587.4	1.230	69349	14.78243	608.23	1.230	69349	14.78243
21	0	-4.00	-0.040	587.4	1.214	69349	14.78243	69349	60823	1.207	69349	14.78243	587.4	1.230	69349	14.78243	608.23	1.230	69349	14.78243
22	0	-4.25	-0.042	581.5	1.193	68203	14.70605	68203	60151	1.186	68203	14.70605	581.5	1.200	68203	14.70605	601.51	1.200	68203	14.70605
23	0	-4.50	-0.044	576.0	1.169	66827	14.62456	66827	59343	1.162	66827	14.62456	576.0	1.180	66827	14.62456	593.43	1.180	66827	14.62456
24	0	-4.75	-0.046	576.0	1.169	66827	14.62456	66827	59343	1.162	66827	14.62456	576.0	1.180	66827	14.62456	593.43	1.180	66827	14.62456
25	0	-5.00	-0.048	571.7	1.147	65717	14.54961	65717	58843	1.140	65717	14.54961	571.7	1.190	65717	14.54961	588.43	1.190	65717	14.54961
26	0	-5.25	-0.050	566.0	1.124	64623	14.47476	64623	58343	1.117	64623	14.47476	566.0	1.170	64623	14.47476	583.43	1.170	64623	14.47476
27	0	-5.50	-0.052	566.0	1.124	64623	14.47476	64623	58343	1.117	64623	14.47476	566.0	1.170	64623	14.47476	583.43	1.170	64623	14.47476
28	0	-5.75	-0.054	561.5	1.102	63523	14.40000	63523	57843	1.095	63523	14.40000	561.5	1.150	63523	14.40000	578.43	1.150	63523	14.40000
29	0	-6.00	-0.056	556.0	1.079	62423	14.32524	62423	57343	1.072	62423	14.32524	556.0	1.130	62423	14.32524	573.43	1.130	62423	14.32524
30	0	-6.25	-0.058	556.0	1.079	62423	14.32524	62423	57343	1.072	62423	14.32524	556.0	1.130	62423	14.32524	573.43	1.130	62423	14.32524
31	0	-6.50	-0.060	551.5	1.057	61323	14.25048	61323	56843	1.050	61323	14.25048	551.5	1.110	61323	14.25048	568.43	1.110	61323	14.25048
32	0	-6.75	-0.062	551.5	1.057	61323	14.25048	61323	56843	1.050	61323	14.25048	551.5	1.110	61323	14.25048	568.43	1.110	61323	14.25048
33	0	-7.00	-0.064	547.0	1.035	60223	14.17572	60223	56343	1.028	60223	14.17572	547.0	1.090	60223	14.17572	563.43	1.090	60223	14.17572
34	0	-7.25	-0.066	547.0	1.035	60223	14.17572	60223	56343	1.028	60223	14.17572	547.0	1.090	60223	14.17572	563.43	1.090	60223	14.17572
35	0	-7.50	-0.068	542.5	1.013	59123	14.10096	59123	55843	1.005	59123	14.10096	542.5	1.070	59123	14.10096	558.43	1.070	59123	14.10096
36	0	-7.75	-0.070	542.5	1.013	59123	14.10096	59123	55843	1.005	59123	14.10096	542.5	1.070	59123	14.10096	558.43	1.070	59123	14.10096
37	0	-8.00	-0.072	538.0	0.991	58023	14.02620	58023	55343	0.988	58023	14.02620	538.0	1.040	58023	14.02620	553.43	1.040	58023	14.02620
38	0	-8.25	-0.074	538.0	0.991	58023	14.02620	58023	55343	0.988	58023	14.02620	538.0	1.040	58023	14.02620	553.43	1.040	58023	14.02620
39	0	-8.50	-0.076	533.5	0.969	56923	13.95144	56923	54843	0.966	56923	13.95144	533.5	1.000	56923	13.95144	548.43	1.000	56923	13.95144
40	0	-8.75	-0.078	533.5	0.969	56923	13.95144	56923	54843	0.966	56923	13.95144	533.5	1.000	56923	13.95144	548.43	1.000	56923	13.95144
41	0	-9.00	-0.080	529.0	0.947	55823	13.87668	55823	54343	0.944	55823	13.87668	529.0	0.970	55823	13.87668	543.43	0.970	55823	13.87668
42	0	-9.25	-0.082	529.0	0.947	55823	13.87668	55823	54343	0.944	55823	13.87668	529.0	0.970	55823	13.87668	543.43	0.970	55823	13.87668
43	0	-9.50	-0.084	524.5	0.925	54723	13.80192	54723	53843	0.922	54723	13.80192	524.5	0.950	54723	13.80192	538.43	0.950	54723	13.80192
44	0	-9.75	-0.086	524.5	0.925	54723	13.80192	54723	53843	0.922	54723	13.80192	524.5	0.950	54723	13.80192	538.43	0.950	54723	13.80192
45	0	-1.00	-0.088	520.0	0.903	53623	13.72716	53623	53343	0.900	53623	13.72716	520.0	0.930	53623	13.72716	533.43	0.930	53623	13.72716
46	0	-1.25	-0.090	520.0	0.903	53623	13.72716	53623	53343	0.900	53623	13.72716	520.0	0.930	53623	13.72716	533.43	0.930	53623	13.72716
47	0	-1.50	-0.092	515.5	0.881	52523	13.65240	52523	52843	0.878	52523	13.65240	515.5	0.910	52523	13.65240	528.43	0.910	52523	13.65240
48	0	-1.75	-0.094	515.5	0.881	52523	13.65240	52523	52843	0.878	52523	13.65240	515.5	0.910	52523	13.65240	528.43	0.910	52523	13.65240
49	0	-2.00	-0.096	511.0	0.859	51423	13.57764	51423	52343	0.856	51423	13.57764	511.0	0.890	51423	13.57764	523.43	0.890	51423	13.57764
50	0	-2.25	-0.098	511.0	0.859	51423	13.57764	51423	52343	0.856	51423	13.57764	511.0	0.890	51423	13.57764	523.43	0.890	51423	13.57764

2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466	467
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Conversion factors: 1 $\text{mCH} = 2.34 \text{ cm}$; 1 $\text{psi} = 47.88 \text{ N/mm}^2$.
Data for orifice 20 were inaccurate due to leakage and are not presented.

TABLE III.- DATA^a FOR 140° CONE; $M_\infty = 3.95$ - Concluded(e) $\alpha = 20^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 67.5^\circ, p_t = 5775.8 \text{ psf}$				$\Phi = 90.0^\circ, p_t = 5775.8 \text{ psf}$			
				p_t , psf	C_p	p_t/p_∞	M_t	p_t , psf	C_p	p_t/p_∞	M_t
1	0	+0.30	+0.000	944.0	1.358	15.81521	-62253	443.9	1.359	15.83301	-62269
2	0	+0.230	+0.025	615.9	1.297	10.73359	-74701	639.2	1.344	15.81812	-61882
3	0	+0.50	+0.043	621.7	1.309	7.7332	-74732	645.5	1.362	15.81729	-61867
4	0	+0.800	+0.050	632.9	1.336	6.5156	-75257	650.7	1.387	16.14731	-59787
5	0	+1.30	+0.100	632.9	1.333	5.48157	-75257	650.7	1.387	16.14731	-59787
6	0	+1.25	+0.125	634.5	1.337	4.7861	-75861	659.5	1.401	16.30446	-58546
7	0	+1.50	+0.200	636.0	1.340	4.2652	-76052	669.5	1.416	16.30446	-58546
8	0	+1.200	+0.150	636.0	1.340	3.76052	-76052	671.1	1.419	16.50090	-56966
9	0	+1.600	+0.200	636.0	1.340	3.271	-76861	671.1	1.419	16.50090	-56966
10	0	+1.800	+0.225	634.5	1.337	2.7869	-77569	663.5	1.412	16.50090	-56966
11	0	+2.300	+0.250	629.7	1.326	2.2927	-78267	651.5	1.405	16.50090	-56966
12	0	+2.75	+0.275	621.7	1.317	1.7905	-78905	643.9	1.398	16.50090	-56966
13	0	+2.200	+0.325	612.1	1.301	1.286	-79590	632.8	1.373	16.50090	-56966
14	0	+2.530	+0.350	604.1	1.286	0.78230	-80286	625.0	1.358	16.50090	-56966
15	0	+3.000	+0.375	604.1	1.286	0.28694	-80984	617.5	1.343	16.50090	-56966
16	0	+3.400	+0.400	598.7	1.268	0.1712	-81565	610.3	1.328	16.50090	-56966
17	0	+3.500	+0.425	598.7	1.268	0.07554	-82159	603.1	1.313	16.50090	-56966
18	0	+3.500	+0.450	581.7	1.258	0.0453	-82735	596.1	1.298	16.50090	-56966
19	0	+3.800	+0.475	581.7	1.258	0.0151	-83322	589.1	1.283	16.50090	-56966
20	0	+4.000	+0.500	564.7	1.240	0.00940	-83920	582.1	1.268	16.50090	-56966
21	180	+5.00	+0.550	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
22	180	+5.00	+0.575	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
23	180	+5.00	+0.600	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
24	180	+5.00	+0.625	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
25	180	+5.00	+0.650	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
26	180	+5.00	+0.675	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
27	180	+5.00	+0.700	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
28	180	+5.00	+0.725	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
29	180	+5.00	+0.750	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
30	180	+5.00	+0.775	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
31	180	+5.00	+0.800	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
32	180	+5.00	+0.825	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
33	180	+5.00	+0.850	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
34	180	+5.00	+0.875	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
35	180	+5.00	+0.900	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
36	180	+5.00	+0.925	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
37	180	+5.00	+0.950	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
38	180	+5.00	+0.975	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
39	180	+5.00	+1.000	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
40	180	+5.00	+1.025	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
41	180	+5.00	+1.050	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
42	180	+5.00	+1.075	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
43	180	+5.00	+1.100	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
44	180	+5.00	+1.125	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
45	180	+5.00	+1.150	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
46	180	+5.00	+1.175	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
47	180	+5.00	+1.200	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
48	180	+5.00	+1.225	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253
49	180	+5.00	+1.250	604.1	1.430	15.81521	-62253	443.9	1.430	15.81521	-62253

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².
Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE IV.- DATA^a FOR 140° CONE; $M_{\infty} = 4.63$

(a) $\alpha = 0^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ, p_t = 7892.1 \text{ psf}$	$\Phi = 22.5^\circ, p_t = 7892.1 \text{ psf}$	$\Phi = 45.0^\circ, p_t = 7882.6 \text{ psf}$	M_t	p_t/ρ_{∞}	$p_t/p_{t,2}$	C_p	p_t/ρ_{∞}	M_t	p_t/ρ_{∞}	$p_t/p_{t,2}$	C_p	p_t/ρ_{∞}	M_t
				p_t/ρ_{∞}	$p_t/p_{t,2}$	p_t/ρ_{∞}	$p_t/p_{t,2}$	p_t/ρ_{∞}	$p_t/p_{t,2}$	p_t/ρ_{∞}	$p_t/p_{t,2}$	p_t/ρ_{∞}	$p_t/p_{t,2}$	p_t/ρ_{∞}	$p_t/p_{t,2}$	p_t/ρ_{∞}	$p_t/p_{t,2}$
1	0	.000	.0000	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
2	0	.020	.0043	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
3	0	.050	.0093	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
4	0	.100	.0144	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
5	0	.150	.0186	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
6	0	.200	.0229	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
7	0	.250	.0272	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
8	0	.300	.0315	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
9	0	.350	.0358	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
10	0	.400	.0401	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
11	0	.450	.0444	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
12	0	.500	.0487	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
13	0	.550	.0530	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
14	0	.600	.0573	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
15	0	.650	.0616	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
16	0	.700	.0659	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
17	0	.750	.0702	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
18	0	.800	.0745	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
19	0	.850	.0788	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
20	0	.900	.0831	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
21	0	.950	.0874	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
22	0	1.000	.0917	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
23	0	1.050	.0960	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
24	0	1.100	.1003	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
25	0	1.150	.1046	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
26	0	1.200	.1089	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
27	0	1.250	.1132	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
28	0	1.300	.1175	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
29	0	1.350	.1218	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
30	0	1.400	.1261	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
31	0	1.450	.1304	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
32	0	1.500	.1347	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
33	0	1.550	.1390	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
34	0	1.600	.1433	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
35	0	1.650	.1476	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
36	0	1.700	.1519	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
37	0	1.750	.1562	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
38	0	1.800	.1605	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
39	0	1.850	.1648	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
40	0	1.900	.1691	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
41	0	1.950	.1734	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
42	0	2.000	.1777	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
43	0	2.050	.1820	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
44	0	2.100	.1863	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
45	0	2.150	.1906	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
46	0	2.200	.1949	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
47	0	2.250	.1992	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
48	0	2.300	.2035	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
49	0	2.350	.2078	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243
50	0	2.400	.2121	1.749	.97102	27.25152	.97243	1.752	.97243	1.752	.97243	27.25132	.97243	1.752	.97243	27.25132	.97243

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE IV. - DATA^a FOR 140° CONE; $M_{\infty} = 4.63$ - Continued(a) $\alpha = 0^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\phi = 67.5^\circ, p_t = 7882.6 \text{ psf}$				$\phi = 90.0^\circ, p_t = 7882.6 \text{ psf}$			
				p_t , psf	C_p	$p_t/p_{t,2}$	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	M_t
1	0	-0.20	-0.000	634.6	1.757	0.97498	1.0960	634.2	1.756	0.97437	1.0945
2	0	-0.20	-0.025	633.0	1.752	0.97252	1.0960	632.6	1.751	0.97192	1.0945
3	0	-0.20	-0.050	629.8	1.734	0.96770	1.0960	629.4	1.747	0.96946	1.0945
4	0	-0.20	-0.075	623.4	1.725	0.96279	1.0960	623.0	1.733	0.96210	1.0945
5	0	-0.20	-0.100	618.6	1.711	0.95779	1.0960	618.2	1.724	0.95726	1.0945
6	0	-0.20	-0.125	615.4	1.702	0.95262	1.0960	615.0	1.701	0.95226	1.0945
7	0	-0.20	-0.150	612.8	1.694	0.94731	1.0960	612.4	1.691	0.94692	1.0945
8	0	-0.20	-0.175	610.8	1.687	0.94181	1.0960	610.4	1.683	0.94142	1.0945
9	0	-0.20	-0.200	609.8	1.681	0.93611	1.0960	609.4	1.677	0.93572	1.0945
10	0	-0.20	-0.225	609.8	1.674	0.93031	1.0960	609.4	1.670	0.92992	1.0945
11	0	-0.20	-0.250	609.8	1.665	0.92451	1.0960	609.4	1.661	0.92412	1.0945
12	0	-0.20	-0.275	609.8	1.651	0.91864	1.0960	609.4	1.647	0.91825	1.0945
13	0	-0.20	-0.300	609.8	1.633	0.91277	1.0960	609.4	1.629	0.91238	1.0945
14	0	-0.20	-0.325	609.8	1.613	0.90681	1.0960	609.4	1.609	0.90642	1.0945
15	0	-0.20	-0.350	609.8	1.591	0.90085	1.0960	609.4	1.587	0.90046	1.0945
16	0	-0.20	-0.375	609.8	1.568	0.89489	1.0960	609.4	1.564	0.89450	1.0945
17	0	-0.20	-0.400	609.8	1.544	0.88893	1.0960	609.4	1.540	0.88854	1.0945
18	0	-0.20	-0.425	609.8	1.522	0.88297	1.0960	609.4	1.518	0.88258	1.0945
19	0	-0.20	-0.450	609.8	1.500	0.87701	1.0960	609.4	1.496	0.87662	1.0945
20	0	-0.20	-0.475	609.8	1.478	0.87105	1.0960	609.4	1.474	0.87066	1.0945
21	0	-0.20	-0.500	609.8	1.456	0.86509	1.0960	609.4	1.452	0.86470	1.0945
22	180	-0.20	-0.025	641.9	1.741	0.97876	1.1752	641.5	1.737	0.97837	1.1747
23	180	-0.20	-0.050	641.9	1.727	0.97380	1.1752	641.5	1.723	0.97341	1.1747
24	180	-0.20	-0.075	641.9	1.714	0.96884	1.1752	641.5	1.710	0.96845	1.1747
25	180	-0.20	-0.100	641.9	1.701	0.96388	1.1752	641.5	1.697	0.96349	1.1747
26	180	-0.20	-0.125	641.9	1.688	0.95892	1.1752	641.5	1.684	0.95853	1.1747
27	180	-0.20	-0.150	641.9	1.675	0.95396	1.1752	641.5	1.671	0.95357	1.1747
28	180	-0.20	-0.175	641.9	1.662	0.94900	1.1752	641.5	1.658	0.94861	1.1747
29	180	-0.20	-0.200	641.9	1.649	0.94404	1.1752	641.5	1.645	0.94365	1.1747
30	180	-0.20	-0.225	641.9	1.636	0.93908	1.1752	641.5	1.632	0.93869	1.1747
31	180	-0.20	-0.250	641.9	1.623	0.93412	1.1752	641.5	1.619	0.93373	1.1747
32	180	-0.20	-0.275	641.9	1.610	0.92916	1.1752	641.5	1.606	0.92877	1.1747
33	180	-0.20	-0.300	641.9	1.597	0.92420	1.1752	641.5	1.593	0.92381	1.1747
34	180	-0.20	-0.325	641.9	1.584	0.91924	1.1752	641.5	1.580	0.91885	1.1747
35	180	-0.20	-0.350	641.9	1.571	0.91428	1.1752	641.5	1.567	0.91389	1.1747
36	180	-0.20	-0.375	641.9	1.558	0.90932	1.1752	641.5	1.554	0.90893	1.1747
37	180	-0.20	-0.400	641.9	1.545	0.90436	1.1752	641.5	1.541	0.90397	1.1747
38	180	-0.20	-0.425	641.9	1.532	0.89940	1.1752	641.5	1.528	0.89901	1.1747
39	180	-0.20	-0.450	641.9	1.519	0.89444	1.1752	641.5	1.515	0.89405	1.1747
40	180	-0.20	-0.475	641.9	1.506	0.88948	1.1752	641.5	1.502	0.88909	1.1747
41	180	-0.20	-0.500	641.9	1.493	0.88452	1.1752	641.5	1.489	0.88413	1.1747
42	270	-0.20	-0.025	641.9	1.741	0.97876	1.1752	641.5	1.737	0.97837	1.1747
43	270	-0.20	-0.050	641.9	1.727	0.97380	1.1752	641.5	1.723	0.97341	1.1747
44	270	-0.20	-0.075	641.9	1.714	0.96884	1.1752	641.5	1.710	0.96845	1.1747
45	270	-0.20	-0.100	641.9	1.701	0.96388	1.1752	641.5	1.697	0.96349	1.1747
46	270	-0.20	-0.125	641.9	1.688	0.95892	1.1752	641.5	1.684	0.95853	1.1747
47	270	-0.20	-0.150	641.9	1.675	0.95396	1.1752	641.5	1.671	0.95357	1.1747
48	270	-0.20	-0.175	641.9	1.662	0.94900	1.1752	641.5	1.658	0.94861	1.1747
49	270	-0.20	-0.200	641.9	1.649	0.94404	1.1752	641.5	1.645	0.94365	1.1747

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE IV. - DATA^a FOR 140° CONE; $M_{\infty} = 4.63$ - Continued

(b) $\alpha = 5^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0.0^\circ, P_t = 7892.1 \text{ psf}$					$\Phi = 22.5^\circ, P_t = 7882.6 \text{ psf}$					$\Phi = 45.0^\circ, P_t = 7882.6 \text{ psf}$				
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t
1	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
2	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
3	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
4	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
5	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
6	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
7	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
8	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
9	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
10	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
11	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
12	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
13	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
14	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
15	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
16	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
17	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
18	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
19	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
20	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
21	0	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
22	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
23	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
24	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
25	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
26	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
27	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
28	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
29	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
30	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
31	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
32	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
33	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
34	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
35	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
36	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
37	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
38	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
39	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
40	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
41	180	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
42	270	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
43	270	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
44	270	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
45	270	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
46	90	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
47	90	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
48	90	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		
49	90	.000	.0000	624.6	1.726	.98856	26.90183	24.665	1.731	1.731	.96125	26.97730	23.830	27.01655	.96263	23.888		

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE IV.- DATA^a FOR 140° CONE; $M_{\infty} = 4.63$ - Continued(b) $\alpha = 5^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 67.5^\circ, p_t = 7882.6 \text{ psf}$				$\Phi = 90.0^\circ, p_t = 7882.6 \text{ psf}$					
				p_t , psf	C_p	$p_t/p_{t,2}$	P_t/ρ_{∞}	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	P_t/ρ_{∞}	M_t
1	0	.000	.0000	625.5	1.731	.96105	26.97167	.23893	626.5	1.734	.96263	27.01255	.23888
2	0	.230	.0025	615.9	1.712	.95121	26.69575	.26826	624.9	1.725	.95772	26.94733	.24164
3	0	.450	.0093	615.9	1.703	.94630	26.55779	.28192	623.3	1.725	.95772	26.94733	.24164
4	0	.650	.0144	612.7	1.694	.94138	26.51779	.29502	620.2	1.715	.95281	26.87861	.24919
5	0	.830	.0186	609.5	1.676	.93645	26.43982	.30767	617.0	1.706	.94790	26.74057	.25700
6	0	1.000	.0237	606.5	1.662	.93155	26.33390	.31988	613.8	1.697	.94299	26.60273	.26570
7	0	1.230	.0300	601.5	1.648	.92418	25.93696	.33753	609.0	1.697	.94299	26.60273	.26570
8	0	1.400	.0372	596.7	1.648	.91680	25.73001	.35446	601.6	1.694	.93071	26.12030	.32194
9	0	1.550	.0423	593.5	1.639	.91189	25.59202	.36658	601.0	1.650	.92334	25.91354	.33948
10	0	1.800	.0525	587.1	1.620	.90716	25.47182	.39685	597.8	1.651	.91843	25.56895	.36722
11	0	2.000	.0615	581.1	1.611	.90266	25.31612	.41191	593.0	1.637	.91106	25.36890	.39672
12	0	2.200	.0705	573.1	1.597	.89717	25.17816	.43140	588.2	1.637	.90370	25.36219	.39811
13	0	2.400	.0788	567.9	1.579	.88777	24.97122	.44616	582.6	1.610	.89651	25.15543	.43771
14	0	2.600	.0862	561.9	1.565	.87953	24.69529	.46416	570.6	1.573	.88558	24.87976	.46104
15	0	2.800	.0929	551.5	1.547	.87256	24.21262	.48239	562.6	1.552	.87428	24.59549	.48808
16	0	3.000	.0981	542.7	1.524	.86544	23.67362	.51294	553.0	1.522	.86255	23.36354	.51856
17	0	3.200	.1025	532.7	1.496	.85369	23.45363	.52657	548.3	1.490	.85038	22.74327	.55639
18	0	3.400	.1065	524.1	1.464	.84849	22.97076	.52657	548.3	1.449	.84801	22.74327	.55639
19	0	3.600	.1095	518.3	1.423	.84036	22.72213	.52657	548.3	1.394	.84801	22.74327	.55639
20	0	3.800	.1125	513.9	1.388	.83363	22.42477	.52657	548.3	1.302	.84801	22.74327	.55639
21	0	4.000	.1155	509.6	1.353	.82817	22.12151	.52657	548.3	1.248	.84801	22.74327	.55639
22	180	.830	.0186	627.3	1.763	.97953	27.18544	.23702	617.2	1.718	.97030	27.23141	.23287
23	180	1.000	.0237	620.9	1.754	.97182	26.98063	.23702	617.2	1.700	.96500	26.95034	.26732
24	180	1.230	.0300	617.7	1.736	.95823	26.77415	.23702	617.2	1.716	.96355	26.92521	.27657
25	180	1.400	.0372	609.8	1.718	.95101	26.63849	.23702	617.2	1.698	.96121	26.87651	.28615
26	180	1.550	.0423	606.6	1.701	.94375	26.55659	.26023	617.2	1.684	.95875	26.80885	.29855
27	180	1.800	.0525	596.4	1.663	.93193	26.15469	.30672	610.2	1.661	.95235	26.59245	.34884
28	180	2.000	.0615	590.6	1.646	.92458	25.94821	.31894	598.0	1.632	.94984	26.51225	.37162
29	180	2.200	.0705	584.2	1.623	.91477	25.67290	.33659	591.7	1.604	.94600	26.38355	.38735
30	180	2.400	.0788	576.2	1.604	.90741	25.46641	.35902	588.9	1.601	.94189	26.25089	.40761
31	180	2.600	.0862	568.1	1.587	.89760	25.28490	.38590	586.2	1.583	.93809	26.12030	.42718
32	180	2.800	.0929	562.7	1.569	.88762	25.10110	.42076	582.1	1.563	.93429	25.99404	.44761
33	180	3.000	.0981	557.1	1.552	.87851	24.93399	.44932	578.0	1.533	.93144	25.86854	.46816
34	180	3.200	.1025	552.6	1.534	.86384	24.60157	.47675	574.0	1.505	.92860	25.74304	.48871
35	180	3.400	.1065	548.1	1.516	.85441	24.40157	.51639	570.0	1.478	.92584	25.61759	.50948
36	180	3.600	.1095	543.6	1.498	.84699	24.21907	.56599	566.0	1.450	.92308	25.49209	.53024
37	180	3.800	.1125	539.0	1.480	.84036	24.00009	.61565	562.0	1.422	.92032	25.36659	.55100
38	180	4.000	.1155	534.5	1.462	.83363	23.78173	.66531	558.0	1.394	.91756	25.24109	.57176
39	180	4.200	.1185	530.0	1.444	.82817	23.56337	.71502	554.0	1.366	.91480	25.11559	.59252
40	180	4.400	.1215	525.5	1.426	.82363	23.34501	.76477	550.0	1.338	.91194	24.99009	.61328
41	180	4.600	.1245	521.0	1.408	.81917	23.12665	.81452	546.0	1.310	.90908	24.86459	.63404
42	180	4.800	.1275	516.5	1.390	.81477	22.90829	.86427	542.0	1.282	.90622	24.73909	.65480
43	180	5.000	.1305	512.0	1.372	.81038	22.68993	.91402	538.0	1.254	.90336	24.61359	.67556
44	180	5.200	.1335	507.5	1.354	.80600	22.47157	.96377	534.0	1.226	.90050	24.48809	.69632
45	180	5.400	.1365	503.0	1.336	.80161	22.25321	.10152	530.0	1.198	.89764	24.36259	.71708
46	90	2.000	.0615	590.6	1.630	.90741	25.67290	.35902	588.9	1.560	.92809	24.75582	.42718
47	90	2.200	.0705	584.2	1.612	.89760	25.46641	.38590	586.2	1.533	.92514	24.41199	.45081
48	90	2.400	.0788	576.2	1.592	.88762	25.28490	.42076	582.1	1.506	.92260	23.96600	.47648
49	90	2.600	.0862	568.1	1.574	.87851	24.93399	.44932	578.0	1.479	.92006	23.52824	.50458
50	90	2.800	.0929	562.7	1.493	.86384	24.60157	.47675	574.0	1.452	.91752	22.96790	.54284
51	90	3.000	.0981	557.1	1.438	.85441	24.40157	.51639	570.0	1.425	.91500	22.52824	.59188
52	90	3.200	.1025	552.6	1.398	.84699	24.21907	.56599	566.0	1.398	.91250	22.09184	.64064
53	90	3.400	.1065	548.1	1.358	.84036	24.00009	.61565	562.0	1.371	.91000	21.65634	.68984
54	90	3.600	.1095	543.6	1.318	.83363	23.78173	.66531	558.0	1.344	.90750	21.22151	.73908
55	90	3.800	.1125	539.0	1.278	.82817	23.56337	.71502	554.0	1.317	.90500	20.78739	.78832
56	90	4.000	.1155	534.5	1.238	.82363	23.34501	.76477	550.0	1.290	.90250	20.35284	.83756
57	90	4.200	.1185	530.0	1.198	.81917	23.12665	.81452	546.0	1.263	.90000	19.91834	.88680
58	90	4.400	.1215	525.5	1.158	.81477	22.90829	.86427	542.0	1.236	.89750	19.48384	.93604
59	90	4.600	.1245	521.0	1.118	.81038	22.68993	.91402	538.0	1.209	.89500	19.04934	.98528
60	90	4.800	.1275	516.5	1.078	.80600	22.47157	.96377	534.0	1.182	.89250	18.61484	.10352
61	90	5.000	.1305	512.0	1.038	.80161	22.25321	.10152	530.0	1.155	.89000	18.18034	.15276
62	90	5.200	.1335	507.5	.998	.79723	22.03485	.10627	526.0	1.128	.88750	17.74584	.20200
63	90	5.400	.1365	503.0	.958	.79284	21.81649	.11102	522.0	1.101	.88500	17.31134	.25124
64	90	5.600	.1395	498.5	.918	.78845	21.59813	.11577	518.0	1.074	.88250	16.87684	.30048
65	90	5.800	.1425	494.0	.878	.78406	21.37977	.12052	514.0	1.047	.88000	16.44234	.34972
66	90	6.000	.1455	489.5	.838	.77967	21.16141	.12527	510.0	1.020	.87750	16.00784	.39896
67	90	6.200	.1485	485.0	.798	.77528	20.94305	.13002	506.0	1.000	.87500	15.57334	.44820
68	90	6.400	.1515	480.5	.758	.77089	20.72469	.13477	502.0	.979	.87250	15.13884	.49744
69	90	6.600	.1545	476.0	.718	.76650	20.50633	.13952	498.0	.958	.87000	14.70434	.54668
70	90	6.800	.1575	471.5	.678	.76211	20.28797	.14427	494.0	.937	.86750	14.26984	.59592
71	90	7.000	.1605	467.0	.638	.75772	20.06961	.14902	490.0	.916	.86500	13.83534	.64516
72	90	7.200	.1635	462.5	.598	.75333	19.85125	.15377	486.0	.895	.86250	13.40084	.69440
73	90	7.400	.1665	458.0	.558	.74894	19.63289	.15852	482.0	.874	.86000	12.96634	.74364
74	90	7.600	.1695	453.5	.518	.74455	19.41453	.16327	478.0	.853	.85750	12.53184	.79288
75	90	7.800	.1725	449.0	.478	.74016	19.19617	.16802	474.0	.832	.85500	12.09734	.84212
76	90	8.000	.1755	444.5	.438	.73577	18.97781	.17277	470.0	.811	.85250	11.66284	.89136
77	90	8.200	.1785	440.0	.398	.73138	18.75945	.17752	466.0	.790	.85000	11.22834	.94060
78	90	8.400	.1815	435.5	.358	.72699	18.54109	.18227	462.0	.769	.84750	10.79384	.98984
79	90	8.600	.1845	431.0	.318	.72260	18.32273	.18702	458.0	.748	.84500	10.35934	.10352
80	90	8.800	.18										

TABLE IV.- DATA^a FOR 140° CONE; $M_{\infty} = 4.63$ - Continued

(c) $\alpha = 10^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ$, $P_t = 7892.1$ psf				$\Phi = 22.5^\circ$, $P_t = 7882.6$ psf				$\Phi = 45.0^\circ$, $P_t = 7892.1$ psf			
				P_{t1} psf	C_p	P_{t1}/P_{t2}	M_{t1}	P_{t1} psf	C_p	P_{t1}/P_{t2}	M_{t1}	P_{t1} psf	C_p	P_{t1}/P_{t2}	M_{t1}
1	0	-0.30	0.000	536.2	1.644	0.9187	3.5879	595.1	1.643	0.91434	3.5937	596.1	1.644	0.91675	3.5907
2	0	-0.40	0.000	537.8	1.580	0.88054	4.3023	574.3	1.584	0.88239	4.2658	578.5	1.584	0.88777	4.1592
3	0	-0.50	0.000	539.4	1.516	0.84237	5.0167	552.9	1.518	0.88239	4.2658	578.5	1.584	0.88777	4.1592
4	0	-0.60	0.000	541.0	1.452	0.80420	5.7311	531.5	1.454	0.84237	4.2658	578.5	1.584	0.88777	4.1592
5	0	-0.70	0.000	542.6	1.388	0.76603	6.4455	510.7	1.388	0.80420	4.2658	578.5	1.584	0.88777	4.1592
6	0	-0.80	0.000	544.2	1.324	0.72786	7.1599	489.9	1.324	0.76603	4.2658	578.5	1.584	0.88777	4.1592
7	0	-0.90	0.000	545.8	1.260	0.68969	7.8743	469.1	1.260	0.72786	4.2658	578.5	1.584	0.88777	4.1592
8	0	-1.00	0.000	547.4	1.196	0.65152	8.5887	448.3	1.196	0.68969	4.2658	578.5	1.584	0.88777	4.1592
9	0	-1.10	0.000	549.0	1.132	0.61335	9.3031	427.5	1.132	0.65152	4.2658	578.5	1.584	0.88777	4.1592
10	0	-1.20	0.000	550.6	1.068	0.57518	10.0175	406.7	1.068	0.61335	4.2658	578.5	1.584	0.88777	4.1592
11	0	-1.30	0.000	552.2	1.004	0.53701	10.7319	385.9	1.004	0.57518	4.2658	578.5	1.584	0.88777	4.1592
12	0	-1.40	0.000	553.8	0.940	0.49884	11.4463	365.1	0.940	0.53701	4.2658	578.5	1.584	0.88777	4.1592
13	0	-1.50	0.000	555.4	0.876	0.46067	12.1607	344.3	0.876	0.49884	4.2658	578.5	1.584	0.88777	4.1592
14	0	-1.60	0.000	557.0	0.812	0.42250	12.8751	323.5	0.812	0.46067	4.2658	578.5	1.584	0.88777	4.1592
15	0	-1.70	0.000	558.6	0.748	0.38433	13.5895	302.7	0.748	0.42250	4.2658	578.5	1.584	0.88777	4.1592
16	0	-1.80	0.000	560.2	0.684	0.34616	14.3039	281.9	0.684	0.38433	4.2658	578.5	1.584	0.88777	4.1592
17	0	-1.90	0.000	561.8	0.620	0.30799	15.0183	261.1	0.620	0.34616	4.2658	578.5	1.584	0.88777	4.1592
18	0	-2.00	0.000	563.4	0.556	0.26982	15.7327	240.3	0.556	0.30799	4.2658	578.5	1.584	0.88777	4.1592
19	0	-2.10	0.000	565.0	0.492	0.23165	16.4471	219.5	0.492	0.26982	4.2658	578.5	1.584	0.88777	4.1592
20	0	-2.20	0.000	566.6	0.428	0.19348	17.1615	198.7	0.428	0.23165	4.2658	578.5	1.584	0.88777	4.1592
21	0	-2.30	0.000	568.2	0.364	0.15531	17.8759	177.9	0.364	0.19348	4.2658	578.5	1.584	0.88777	4.1592
22	0	-2.40	0.000	569.8	0.300	0.11714	18.5903	157.1	0.300	0.15531	4.2658	578.5	1.584	0.88777	4.1592
23	0	-2.50	0.000	571.4	0.236	0.07897	19.3047	136.3	0.236	0.11714	4.2658	578.5	1.584	0.88777	4.1592
24	0	-2.60	0.000	573.0	0.172	0.04080	20.0191	115.5	0.172	0.07897	4.2658	578.5	1.584	0.88777	4.1592
25	0	-2.70	0.000	574.6	0.108	0.00263	20.7335	94.7	0.108	0.04080	4.2658	578.5	1.584	0.88777	4.1592
26	0	-2.80	0.000	576.2	0.044	0.00000	21.4479	73.9	0.044	0.00263	4.2658	578.5	1.584	0.88777	4.1592
27	0	-2.90	0.000	577.8	0.000	0.00000	22.1623	53.1	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
28	0	-3.00	0.000	579.4	0.000	0.00000	22.8767	32.3	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
29	0	-3.10	0.000	581.0	0.000	0.00000	23.5911	11.5	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
30	0	-3.20	0.000	582.6	0.000	0.00000	24.3055	0.7	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
31	0	-3.30	0.000	584.2	0.000	0.00000	25.0199	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
32	0	-3.40	0.000	585.8	0.000	0.00000	25.7343	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
33	0	-3.50	0.000	587.4	0.000	0.00000	26.4487	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
34	0	-3.60	0.000	589.0	0.000	0.00000	27.1631	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
35	0	-3.70	0.000	590.6	0.000	0.00000	27.8775	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
36	0	-3.80	0.000	592.2	0.000	0.00000	28.5919	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
37	0	-3.90	0.000	593.8	0.000	0.00000	29.3063	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
38	0	-4.00	0.000	595.4	0.000	0.00000	30.0207	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
39	0	-4.10	0.000	597.0	0.000	0.00000	30.7351	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
40	0	-4.20	0.000	598.6	0.000	0.00000	31.4495	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
41	0	-4.30	0.000	600.2	0.000	0.00000	32.1639	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
42	0	-4.40	0.000	601.8	0.000	0.00000	32.8783	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
43	0	-4.50	0.000	603.4	0.000	0.00000	33.5927	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
44	0	-4.60	0.000	605.0	0.000	0.00000	34.3071	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
45	0	-4.70	0.000	606.6	0.000	0.00000	35.0215	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
46	0	-4.80	0.000	608.2	0.000	0.00000	35.7359	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
47	0	-4.90	0.000	609.8	0.000	0.00000	36.4503	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
48	0	-5.00	0.000	611.4	0.000	0.00000	37.1647	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592
49	0	-5.10	0.000	613.0	0.000	0.00000	37.8791	0.0	0.000	0.00000	4.2658	578.5	1.584	0.88777	4.1592

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².
Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE IV.- DATA^a FOR 140° CONE; $M_{\infty} = 4.63$ - Continued(c) $\alpha = 10^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 67.5^\circ, p_t = 7882.6 \text{ psf}$				$\Phi = 90.0^\circ, p_t = 7882.6 \text{ psf}$					
				p_t , psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,0}$	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,0}$	M_t
1	0	.000	.0000	595.2	1.644	.91447	25.66460	.35968	595.9	1.644	.91553	25.69428	.35732
2	0	.025	.0471	584.0	1.611	.89126	25.18166	.39659	592.7	1.636	.91062	25.55650	.36819
3	0	.050	.0943	582.4	1.607	.89481	25.11267	.40166	592.7	1.636	.91062	25.55650	.36819
4	0	.075	.1386	582.4	1.607	.89481	25.11267	.40166	592.7	1.636	.91062	25.55650	.36819
5	0	.100	.1886	579.2	1.598	.89589	24.97469	.41166	589.5	1.632	.90817	25.48762	.37353
6	0	.125	.2357	576.0	1.588	.89497	24.83671	.42149	589.5	1.627	.90571	25.41669	.37892
7	0	.150	.2859	572.8	1.579	.89006	24.69873	.43049	587.7	1.616	.89935	25.31208	.38435
8	0	.175	.3300	569.6	1.566	.88702	24.42276	.45008	587.7	1.604	.89344	25.07431	.40446
9	0	.200	.3703	563.2	1.552	.88531	24.28478	.46393	578.3	1.595	.88853	24.93653	.41439
10	0	.225	.4045	558.4	1.538	.88793	24.07781	.47304	575.1	1.586	.88362	24.79716	.42486
11	0	.250	.4316	555.2	1.529	.89302	23.99883	.48532	567.1	1.563	.87135	24.45594	.44795
12	0	.275	.4516	558.4	1.529	.89302	23.99883	.48532	567.1	1.563	.87135	24.45594	.44795
13	0	.300	.4659	555.9	1.501	.88327	23.52588	.50842	560.7	1.545	.86153	24.17679	.46639
14	0	.325	.4754	559.2	1.483	.88243	23.24992	.52559	555.9	1.531	.85417	23.97214	.47993
15	0	.350	.4801	560.1	1.464	.88860	22.97356	.54247	548.0	1.508	.84189	23.58381	.49531
16	0	.375	.4754	570.2	1.437	.80385	22.56001	.57168	530.4	1.457	.81489	22.86097	.54877
17	0	.400	.4619	563.2	1.408	.76543	21.59414	.62354	516.0	1.416	.79280	22.25000	.58560
18	0	.425	.4380	550.8	1.372	.73994	20.76625	.6498.8	498.8	1.361	.76335	21.42338	.63328
19	0	.450	.4094	542.8	1.234	.69569	19.52441	.71305	466.5	1.274	.71571	20.11095	.70384
20	0	.475	.3757	504.8	1.092	.94047	26.39414	.79342	508.3	1.056	.92085	25.84350	.33836
21	0	.500	.3357	481.6	1.017	.94292	26.46305	.79948	507.8	1.051	.91840	25.74777	.35085
22	0	.525	.2931	452.8	1.317	.94047	26.39414	.79742	508.2	1.046	.91595	25.70604	.35638
23	180	.000	.0000	595.2	1.644	.91447	25.66460	.35968	595.9	1.644	.91553	25.69428	.35732
24	180	.025	.0471	584.0	1.611	.89126	25.18166	.39659	592.7	1.636	.91062	25.55650	.36819
25	180	.050	.0943	582.4	1.607	.89481	25.11267	.40166	592.7	1.636	.91062	25.55650	.36819
26	180	.075	.1386	582.4	1.607	.89481	25.11267	.40166	592.7	1.636	.91062	25.55650	.36819
27	180	.100	.1886	579.2	1.598	.89589	24.97469	.41166	589.5	1.632	.90817	25.48762	.37353
28	180	.125	.2357	576.0	1.588	.89497	24.83671	.42149	589.5	1.627	.90571	25.41669	.37892
29	180	.150	.2859	572.8	1.579	.89006	24.69873	.43049	587.7	1.616	.89935	25.31208	.38435
30	180	.175	.3300	569.6	1.566	.88702	24.42276	.45008	587.7	1.604	.89344	25.07431	.40446
31	180	.200	.3703	563.2	1.552	.88531	24.28478	.46393	578.3	1.595	.88853	24.93653	.41439
32	180	.225	.4045	558.4	1.538	.88793	24.07781	.47304	575.1	1.586	.88362	24.79716	.42486
33	180	.250	.4316	555.2	1.529	.89302	23.99883	.48532	567.1	1.563	.87135	24.45594	.44795
34	180	.275	.4516	558.4	1.529	.89302	23.99883	.48532	567.1	1.563	.87135	24.45594	.44795
35	180	.300	.4659	555.9	1.501	.88327	23.52588	.50842	560.7	1.545	.86153	24.17679	.46639
36	180	.325	.4754	559.2	1.483	.88243	23.24992	.52559	555.9	1.531	.85417	23.97214	.47993
37	180	.350	.4801	560.1	1.464	.88860	22.97356	.54247	548.0	1.508	.84189	23.58381	.49531
38	180	.375	.4754	570.2	1.437	.80385	22.56001	.57168	530.4	1.457	.81489	22.86097	.54877
39	180	.400	.4619	563.2	1.408	.76543	21.59414	.62354	516.0	1.416	.79280	22.25000	.58560
40	180	.425	.4380	550.8	1.372	.73994	20.76625	.6498.8	498.8	1.361	.76335	21.42338	.63328
41	180	.450	.4094	542.8	1.234	.69569	19.52441	.71305	466.5	1.274	.71571	20.11095	.70384
42	180	.475	.3757	504.8	1.092	.94047	26.39414	.79342	508.3	1.056	.92085	25.84350	.33836
43	180	.500	.3357	481.6	1.017	.94292	26.46305	.79948	507.8	1.051	.91840	25.74777	.35085
44	180	.525	.2931	452.8	1.317	.94047	26.39414	.79742	508.2	1.046	.91595	25.70604	.35638
45	180	.550	.2500	425.0	1.683	.93556	26.25631	.80965	508.6	1.042	.91350	25.63730	.36158
46	180	.575	.2045	398.0	1.965	.92573	25.98065	.83386	503.7	1.024	.90370	25.36237	.38130
47	180	.600	.1566	371.5	1.656	.92082	25.80423	.858.2	503.4	1.010	.89146	25.15617	.39847
48	180	.625	.1064	346.5	1.642	.91346	25.63508	.86194	503.4	1.001	.88411	25.01871	.40849
49	180	.650	.0568	321.3	1.533	.90854	25.49825	.86545	503.4	1.001	.88411	25.01871	.40849
50	180	.675	.0072	296.2	1.500	.89136	25.01586	.86969	503.4	1.001	.88411	25.01871	.40849
51	180	.700	.0000	273.6	1.582	.88155	24.74020	.87297	503.4	1.001	.88411	25.01871	.40849
52	180	.725	.0000	255.8	1.559	.86926	24.39563	.87592	503.4	1.001	.88411	25.01871	.40849
53	180	.750	.0000	239.2	1.532	.85452	23.98214	.87828	503.4	1.001	.88411	25.01871	.40849
54	180	.775	.0000	224.1	1.500	.84054	22.60386	.88155	503.4	1.001	.88411	25.01871	.40849
55	180	.800	.0000	209.2	1.348	.75630	21.22557	.88411	503.4	1.001	.88411	25.01871	.40849
56	180	.825	.0000	194.5	1.175	.69812	20.70351	.88411	503.4	1.001	.88411	25.01871	.40849
57	180	.850	.0000	180.0	1.000	.65854	20.35894	.88411	503.4	1.001	.88411	25.01871	.40849
58	180	.875	.0000	166.7	0.825	.61829	20.01437	.88411	503.4	1.001	.88411	25.01871	.40849
59	180	.900	.0000	153.8	0.650	.57804	19.66980	.88411	503.4	1.001	.88411	25.01871	.40849
60	180	.925	.0000	141.5	0.475	.53779	19.32523	.88411	503.4	1.001	.88411	25.01871	.40849
61	180	.950	.0000	129.2	0.300	.49754	18.98065	.88411	503.4	1.001	.88411	25.01871	.40849
62	180	.975	.0000	117.0	0.125	.45729	18.63607	.88411	503.4	1.001	.88411	25.01871	.40849
63	180	1.000	.0000	104.7	0.000	.41704	18.29149	.88411	503.4	1.001	.88411	25.01871	.40849
64	180	1.025	.0000	92.5	0.000	.37679	17.94690	.88411	503.4	1.001	.88411	25.01871	.40849
65	180	1.050	.0000	80.2	0.000	.33654	17.60231	.88411	503.4	1.001	.88411	25.01871	.40849
66	180	1.075	.0000	68.0	0.000	.29629	17.25772	.88411	503.4	1.001	.88411	25.01871	.40849
67	180	1.100	.0000	55.7	0.000	.25604	16.91313	.88411	503.4	1.001	.88411	25.01871	.40849
68	180	1.125	.0000	43.5	0.000	.21579	16.56854	.88411	503.4	1.001	.88411	25.01871	.40849
69	180	1.150	.0000	31.2	0.000	.17554	16.22395	.88411	503.4	1.001	.88411	25.01871	.40849
70	180	1.175	.0000	19.0	0.000	.13529	15.87936	.88411	503.4	1.001	.88411	25.01871	.40849
71	180	1.200	.0000	6.7	0.000	.09504	15.53477	.88411	503.4	1.001	.88411	25.01871	.40849
72	180	1.225	.0000	0.0	0.000	.05479	15.19018	.88411	503.4	1.001	.88411	25.01871	.40849
73	180	1.250	.0000	0.0	0.000	.01454	14.84559	.88411	503.4	1.001	.88411	25.01871	.40849
74	180	1.275	.0000	0.0	0.000	.00000	14.50100	.88411	503.4	1.001	.88411	25.01871	.40849
75	180	1.300	.0000	0.0	0.000	.00000	14.15641	.88411	503.4	1.001	.88411	25.01871	.40849
76	180	1.325	.0000	0.0	0.000	.00000	13.81182	.88411	503.4	1.001	.88411	25.01871	.40849
77	180	1.350	.0000	0.0	0.000	.00000	13.46723	.88411	503.4	1.001	.88411	25.01871	.40849
78	180	1.375	.0000	0.0	0.000	.00000	13.12264	.88411	503.4	1.001	.88411	25.01871	.40849
79	180	1.400	.0000	0.0	0.000	.00000	12.77805	.88411	503.4	1.001	.88411	25.01871	.40849
80	180	1.425	.0000	0.0	0.000	.00000	12.43346	.88411	503.4	1.001	.88411	25.01871	.40849
81	180	1.450	.0000	0.0	0.000	.00000	12.08887	.88411	503.4	1.001	.88411	25.01871	.40849
82	180	1.475	.0000	0.0	0.000	.00000	11.74428	.88411	503.4	1.001	.88411	25.01871	.40849
83	180	1.500	.0000	0.0	0.000	.00000	11.39969	.88411	503.4	1.001	.88411	25.01871	.40849
84	180	1.525	.0000	0.0	0.000	.00000	11.05510	.88411	503.4	1.001	.88411	25.01871	.40849
85	180	1.550	.0000	0.0	0.000	.00000	10.71051	.88411	503.4	1.001	.88411	25.01871	.40849
86	180	1.575	.0000	0.0	0.000	.00000	10.36592	.88411					

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE IV. - DATA^a FOR 140° CONE; $M_{\infty} = 4.63$ - Continued

(d) $\alpha = 15^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0.0^\circ, p_t = 7892.1 \text{ psf}$			
				p_t , psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}
1	0	.000	.0000	543.4	1.493	.83382	23.40103
2	0	.000	.0000	511.4	1.491	.78577	22.02450
3	0	.000	.0000	480.4	1.489	.74011	20.84852
4	0	.000	.0000	450.4	1.487	.69686	19.90981
5	0	.000	.0000	421.4	1.485	.65598	19.14558
6	0	.000	.0000	393.4	1.483	.61745	18.52688
7	0	.000	.0000	366.4	1.481	.58128	18.01910
8	0	.000	.0000	340.4	1.479	.54745	17.59258
9	0	.000	.0000	315.4	1.477	.51598	17.23010
10	0	.000	.0000	291.4	1.475	.48686	16.92688
11	0	.000	.0000	268.4	1.473	.45998	16.67910
12	0	.000	.0000	246.4	1.471	.43528	16.48258
13	0	.000	.0000	225.4	1.469	.41268	16.33410
14	0	.000	.0000	205.4	1.467	.39208	16.23010
15	0	.000	.0000	186.4	1.465	.37345	16.16658
16	0	.000	.0000	168.4	1.463	.35668	16.13910
17	0	.000	.0000	151.4	1.461	.34178	16.14258
18	0	.000	.0000	135.4	1.459	.32868	16.17210
19	0	.000	.0000	120.4	1.457	.31728	16.22458
20	0	.000	.0000	106.4	1.455	.30748	16.29658
21	0	.000	.0000	93.4	1.453	.29918	16.38410
22	0	.000	.0000	81.4	1.451	.29238	16.48258
23	0	.000	.0000	70.4	1.449	.28708	16.59658
24	0	.000	.0000	60.4	1.447	.28318	16.72010
25	0	.000	.0000	51.4	1.445	.28068	16.85858
26	0	.000	.0000	43.4	1.443	.27948	17.00658
27	0	.000	.0000	36.4	1.441	.27938	17.16910
28	0	.000	.0000	30.4	1.439	.28038	17.34258
29	0	.000	.0000	25.4	1.437	.28248	17.52458
30	0	.000	.0000	21.4	1.435	.28568	17.71258
31	0	.000	.0000	18.4	1.433	.28988	17.90458
32	0	.000	.0000	15.4	1.431	.29508	18.10058
33	0	.000	.0000	13.4	1.429	.30128	18.30058
34	0	.000	.0000	11.4	1.427	.30848	18.50458
35	0	.000	.0000	10.4	1.425	.31668	18.71258
36	0	.000	.0000	9.4	1.423	.32588	18.92458
37	0	.000	.0000	8.4	1.421	.33608	19.14058
38	0	.000	.0000	7.4	1.419	.34728	19.36058
39	0	.000	.0000	6.4	1.417	.35948	19.58458
40	0	.000	.0000	5.4	1.415	.37268	19.81258
41	0	.000	.0000	4.4	1.413	.38688	20.04458
42	0	.000	.0000	3.4	1.411	.40208	20.28058
43	0	.000	.0000	2.4	1.409	.41828	20.52058
44	0	.000	.0000	1.4	1.407	.43548	20.76458
45	0	.000	.0000	.4	1.405	.45368	21.01258
46	0	.000	.0000	.4	1.403	.47288	21.26458
47	0	.000	.0000	.4	1.401	.49308	21.52058
48	0	.000	.0000	.4	1.399	.51428	21.78058
49	0	.000	.0000	.4	1.397	.53648	22.04458

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice θ were inaccurate due to leakage and are not presented.

TABLE IV - DATA^a FOR 140° CONE: $M_{\infty} = 4.63$ - Continued

(e) $\alpha = 20^\circ$

Office	e, deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, p_t = 7802.1 \text{ psf}$					$\phi = 22.5^\circ, p_t = 7892.1 \text{ psf}$					$\phi = 45.0^\circ, p_t = 7882.6 \text{ psf}$									
					p_t , psf	C_p	$p_t/p_{t,2}$	p_t/ϕ_{90}	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	p_t/ϕ_{90}	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	p_t/ϕ_{90}	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	p_t/ϕ_{90}	M_t
1	0	0.300	-0.000	-0.000	453.9	1.282	721.06	18.23767	-69980	468.3	1.277	718.00	20.16758	-70361	471.5	1.288	720.33	20.33949	-69643	474.3	1.298	720.33	20.33949	-69643
2	0	0.200	-0.025	-0.0471	425.7	1.158	654.84	16.37491	-80182	426.7	1.158	654.84	16.37491	-80182	426.7	1.158	654.84	16.37491	-80182	426.7	1.158	654.84	16.37491	-80182
3	0	0.500	-0.050	-0.0943	445.9	1.213	684.27	19.20246	-72356	451.6	1.213	684.27	19.20246	-72356	451.6	1.213	684.27	19.20246	-72356	451.6	1.213	684.27	19.20246	-72356
4	0	0.500	-0.075	-0.1414	469.6	1.259	708.79	19.89326	-71881	457.1	1.256	701.44	19.46876	-73018	452.3	1.233	694.91	19.50272	-72028	457.1	1.256	701.44	19.46876	-73018
5	0	0.500	-0.100	-0.1885	493.4	1.299	733.31	20.58466	-71416	455.1	1.256	701.44	19.46876	-73018	452.3	1.233	694.91	19.50272	-72028	455.1	1.256	701.44	19.46876	-73018
6	0	1.300	-0.125	-0.2357	450.7	1.254	706.34	19.82242	-72260	455.1	1.254	706.34	19.82242	-72260	455.1	1.254	706.34	19.82242	-72260	455.1	1.254	706.34	19.82242	-72260
7	0	1.200	-0.150	-0.2829	460.3	1.250	703.99	19.75459	-72639	455.1	1.254	706.34	19.82242	-72260	455.1	1.254	706.34	19.82242	-72260	455.1	1.254	706.34	19.82242	-72260
8	0	1.400	-0.175	-0.3300	457.1	1.245	701.99	19.68675	-73006	455.1	1.254	706.34	19.82242	-72260	455.1	1.254	706.34	19.82242	-72260	455.1	1.254	706.34	19.82242	-72260
9	0	1.600	-0.200	-0.3771	453.9	1.236	699.53	19.61891	-73376	455.1	1.254	706.34	19.82242	-72260	455.1	1.254	706.34	19.82242	-72260	455.1	1.254	706.34	19.82242	-72260
10	0	1.800	-0.225	-0.4242	451.6	1.231	697.13	19.55106	-73746	455.1	1.254	706.34	19.82242	-72260	455.1	1.254	706.34	19.82242	-72260	455.1	1.254	706.34	19.82242	-72260
11	0	2.000	-0.250	-0.4715	452.3	1.231	694.08	19.47927	-74152	450.7	1.227	691.63	19.41094	-74530	455.1	1.242	698.93	19.44055	-74925	450.7	1.227	691.63	19.41094	-74530
12	0	2.200	-0.275	-0.5186	450.7	1.227	691.63	19.41094	-74530	450.7	1.227	691.63	19.41094	-74530	450.7	1.227	691.63	19.41094	-74530	450.7	1.227	691.63	19.41094	-74530
13	0	2.400	-0.300	-0.5658	449.1	1.222	689.72	19.34311	-74925	449.1	1.222	689.72	19.34311	-74925	449.1	1.222	689.72	19.34311	-74925	449.1	1.222	689.72	19.34311	-74925
14	0	2.600	-0.325	-0.6129	447.8	1.217	687.81	19.27527	-75328	447.8	1.217	687.81	19.27527	-75328	447.8	1.217	687.81	19.27527	-75328	447.8	1.217	687.81	19.27527	-75328
15	0	2.800	-0.350	-0.6600	446.3	1.213	685.91	19.20742	-75723	446.3	1.213	685.91	19.20742	-75723	446.3	1.213	685.91	19.20742	-75723	446.3	1.213	685.91	19.20742	-75723
16	0	3.000	-0.375	-0.7072	442.9	1.204	679.36	19.13911	-76039	442.9	1.204	679.36	19.13911	-76039	442.9	1.204	679.36	19.13911	-76039	442.9	1.204	679.36	19.13911	-76039
17	0	3.200	-0.400	-0.7544	439.5	1.195	674.46	19.06928	-76416	439.5	1.195	674.46	19.06928	-76416	439.5	1.195	674.46	19.06928	-76416	439.5	1.195	674.46	19.06928	-76416
18	0	3.400	-0.425	-0.8015	434.7	1.181	667.46	18.99862	-76795	436.3	1.192	671.99	18.92862	-77170	437.9	1.192	671.99	18.92862	-77170	436.3	1.192	671.99	18.92862	-77170
19	0	3.600	-0.450	-0.8486	417.1	1.131	640.12	18.72658	-77805	425.1	1.121	652.38	18.30913	-78052	431.6	1.117	662.99	18.46843	-77422	425.1	1.121	652.38	18.30913	-78052
20	0	3.800	-0.475	-0.8958	417.1	1.131	640.12	18.72658	-77805	425.1	1.121	652.38	18.30913	-78052	431.6	1.117	662.99	18.46843	-77422	425.1	1.121	652.38	18.30913	-78052
21	0	4.000	-0.500	-0.9430	394.6	1.080	613.14	17.96498	-82442	394.8	1.066	605.79	17.00134	-87741	412.3	1.118	633.53	17.59886	-80099	394.6	1.080	613.14	17.96498	-82442
22	180	-2.000	-0.025	-0.0471	543.8	1.494	834.67	23.41944	-51508	577.0	1.582	880.95	24.88029	-41776	568.2	1.509	842.25	23.63757	-50138	543.8	1.494	834.67	23.41944	-51508
23	180	-0.400	-0.050	-0.0943	589.4	1.702	933.36	26.16659	-37193	606.7	1.647	916.24	25.71435	-35572	585.8	1.564	880.26	24.39563	-43192	589.4	1.702	933.36	26.16659	-37193
24	180	-0.600	-0.075	-0.1414	618.7	1.709	940.94	26.44734	-37312	606.7	1.647	916.24	25.71435	-35572	585.8	1.564	880.26	24.39563	-43192	618.7	1.709	940.94	26.44734	-37312
25	180	1.000	-0.125	-0.2357	625.7	1.732	961.72	26.99073	-37618	613.0	1.674	930.94	26.12688	-36213	575.4	1.587	883.99	25.40311	-40311	625.7	1.732	961.72	26.99073	-37618
26	180	1.200	-0.150	-0.2829	631.5	1.746	969.07	27.19677	-37835	613.0	1.674	930.94	26.12688	-36213	575.4	1.587	883.99	25.40311	-40311	631.5	1.746	969.07	27.19677	-37835
27	180	1.400	-0.175	-0.3300	636.3	1.760	974.93	27.40084	-38052	613.0	1.674	930.94	26.12688	-36213	575.4	1.587	883.99	25.40311	-40311	636.3	1.760	974.93	27.40084	-38052
28	180	1.600	-0.200	-0.3771	641.1	1.773	983.75	27.50816	-38269	627.4	1.734	962.79	27.02069	-37337	592.9	1.637	911.00	25.46717	-38735	641.1	1.773	983.75	27.50816	-38269
29	180	2.000	-0.250	-0.4715	641.1	1.773	983.75	27.50816	-38269	627.4	1.734	962.79	27.02069	-37337	592.9	1.637	911.00	25.46717	-38735	641.1	1.773	983.75	27.50816	-38269
30	180	2.200	-0.275	-0.5186	644.3	1.782	986.20	27.67752	-38486	630.6	1.739	965.24	27.13820	-37582	592.9	1.637	911.00	25.46717	-38735	644.3	1.782	986.20	27.67752	-38486
31	180	2.400	-0.300	-0.5658	644.3	1.782	986.20	27.67752	-38486	630.6	1.739	965.24	27.13820	-37582	592.9	1.637	911.00	25.46717	-38735	644.3	1.782	986.20	27.67752	-38486
32	180	2.600	-0.325	-0.6129	644.3	1.782	986.20	27.67752	-38486	630.6	1.739	965.24	27.13820	-37582	592.9	1.637	911.00	25.46717	-38735	644.3	1.782	986.20	27.67752	-38486
33	180	2.800	-0.350	-0.6600	644.3	1.782	986.20	27.67752	-38486	630.6	1.739	965.24	27.13820	-37582	592.9	1.637	911.00	25.46717	-38735	644.3	1.782	986.20	27.67752	-38486
34	180	3.000	-0.375	-0.7072	644.3	1.782	986.20	27.67752	-38486	630.6	1.739	965.24	27.13820	-37582	592.9	1.637	911.00	25.46717	-38735	644.3	1.782	986.20	27.67752	-38486
35	180	3.200	-0.400	-0.7544	644.3	1.782	986.20	27.67752	-38486	630.6	1.739	965.24	27.13820	-37582	592.9	1.637	911.00	25.46717	-38735	644.3	1.782	986.20	27.67752	-38486
36	180	3.400	-0.425	-0.8015	631.5	1.760	974.93	27.40084	-38052	624.2	1.725	957.89	26.88318	-37400	588.1	1.633	908.54	25.49825	-37271	631.5	1.760	974.93	27.40084	-38052
37	180	3.600	-0.450	-0.8486	621.9	1.717	952.36	27.02069	-37337	624.2	1.725	957.89	26.88318	-37400	588.1	1.633	908.54	25.49825	-37271	621.9	1.717	952.36	27.02069	-37337
38	180	3.800	-0.475	-0.8958	618.7	1.709	940.94	26.44734	-37312	624.2	1.725	957.89	26.88318	-37400	588.1	1.633	908.54	25.49825	-37271	618.7	1.709	940.94	26.44734	-37312
39	180	4.000	-0.500	-0.9430	578.9	1.595	883.1	24.93392	-31793	593.9	1.658	911.34	25.57684	-36660	567.4	1.594	884.5	24.87803	-37425	578.9	1.595	883.1	24.93392	-31793
40	180	4.200	-0.525	-0.9901	578.9	1.595	883.1	24.93392	-31793	593.9	1.658	911.34	25.57684	-36660	567.4	1.594	884.5	24.87803	-37425	578.9	1.595	883.1	24.93392	-31793
41	180	4.400	-0.550	-1.0372	578.9	1.595	883.1	24.93392	-31793	593.9	1.658	911.34	25.57684	-36660	567.4	1.594	884.5	24.87803	-37425	578.9	1.595	883.1	24.93392	-31793
42	270	1.000	-0.125	-0.2357	502.3	1.375	770.85	21.63380	-62127	542.8	1.491	746.90	20.53925	-68725	522.6	1.522	744.31	20.44431	-69819	502.3	1.375	770.85	21.63380	-62127
43	270	1.200	-0.150	-0.2829	507.1	1.389	778.19	21.83993	-62408	542.8	1.491	746.90	20.53925	-68725	522.6	1.522	744.31	20.44431	-69819	507.1	1.389	778.19	21.83993	-62408
44	270	1.400	-0.175	-0.3300	507.1	1.389	778.19	21.83993	-62408	542.8	1.491	746.90	20.53925	-68725	522.6	1.522	744.31	20.44431	-69819	507.1	1.389	778.19	21.83993	-62408
45	270	1.600	-0.200	-0.3771	507.1	1.389	778.19	21.83993	-62408	542.8	1.491	746.90	20.53925	-68725	522.6	1.522	744.31	20.44431	-69819	507.1	1.389	778.19	21.83993	-62408
46	270	1.800	-0.225	-0.4242	49																			

a conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE IV.- DATA^a FOR 140° CONE; $M_{\infty} = 4.63$ - Concluded

(e) $\alpha = 20^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ, P_t = 7882.6$ psf				$\phi = 90.0^\circ, P_t = 7882.6$ psf					
				$P_{t,1}$ psf	C_p	$P_{t,1}/P_{t,2}$	$P_{t,1}/P_{t,\infty}$	$M_{t,1}$	$P_{t,1}$ psf	C_p	$P_{t,1}/P_{t,2}$	$P_{t,1}/P_{t,\infty}$	$M_{t,1}$
1	0	.200	.0000	447.1	1.276	.71766	20.14113	70507	448.1	1.278	.71932	20.18484	70295
2	0	.220	-.0025	449.5	1.221	.68537	19.17546	75918	449.5	1.269	.71431	20.04706	71027
3	0	.400	-.0043	444.7	1.211	.69063	19.38239	74484	472.9	1.292	.72658	20.39151	69120
4	0	.530	-.0144	457.5	1.248	.70282	19.72727	72790	485.5	1.320	.74131	20.80485	66816
5	0	.800	-.0386	482.3	1.282	.71059	19.93420	71650	488.9	1.338	.75113	21.08042	65269
6	0	1.200	-.0712	495.1	1.276	.71766	20.07215	70889	495.3	1.357	.76095	21.35598	63711
7	0	1.420	-.0829	487.1	1.276	.71766	20.07215	70889	498.5	1.366	.76586	21.49376	62927
8	0	1.500	-.0772	457.1	1.276	.71766	20.07215	70889	498.5	1.366	.76586	21.49376	62927
9	0	1.500	-.0772	457.1	1.276	.71766	20.07215	70889	498.5	1.366	.76586	21.49376	62927
10	0	2.000	-.1586	465.5	1.271	.71520	20.07215	70889	498.5	1.366	.76586	21.49376	62927
11	0	2.200	-.1775	465.5	1.271	.71520	20.07215	70889	498.5	1.366	.76586	21.49376	62927
12	0	2.400	-.1868	463.9	1.266	.71275	20.00318	71249	498.9	1.361	.76340	21.42487	63319
13	0	2.500	-.1829	462.3	1.262	.71059	19.93420	71650	495.3	1.357	.76095	21.35598	63711
14	0	3.200	-.2375	459.1	1.259	.70527	19.59625	72510	492.1	1.347	.75604	21.21820	64491
15	0	3.200	-.2375	459.1	1.259	.70527	19.59625	72510	492.1	1.347	.75604	21.21820	64491
16	0	3.500	-.2544	443.1	1.207	.68080	19.10648	76196	482.5	1.320	.74131	20.80485	66816
17	0	3.500	-.2544	443.1	1.207	.68080	19.10648	76196	482.5	1.320	.74131	20.80485	66816
18	0	4.000	-.2815	435.1	1.184	.66891	18.76160	78083	465.1	1.274	.71676	20.11595	70446
19	0	4.000	-.2815	435.1	1.184	.66891	18.76160	78083	465.1	1.274	.71676	20.11595	70446
20	0	4.500	-.3125	427.1	1.142	.64639	18.14081	81480	450.5	1.228	.69222	19.42705	74473
21	0	4.500	-.3125	427.1	1.142	.64639	18.14081	81480	450.5	1.228	.69222	19.42705	74473
22	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
23	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
24	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
25	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
26	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
27	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
28	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
29	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
30	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
31	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
32	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
33	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
34	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
35	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
36	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
37	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
38	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
39	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
40	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
41	180	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
42	270	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
43	270	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
44	270	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
45	270	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
46	270	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
47	90	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
48	90	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295
49	90	.200	-.0043	447.1	1.276	.71766	20.16113	70507	448.1	1.278	.71932	20.18484	70295

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Data for orifice 29 were inaccurate due to leakage and are not presented.

TABLE V. - DATA^a FOR 160° CONE; $M_{\infty} = 2.30$ (a) $\alpha = 0^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0, 0^\circ, p_t = 2291.4 \text{ psf}$				
				p_t , psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,\infty}$	M_t
1	0	-0.00	.0000	1334.8	1.577	.99867	7.28404	.04363
2	0	-0.20	.0025	1334.8	1.697	.99867	7.28404	.04363
3	0	-0.40	.0050	1334.8	1.817	.99867	7.28404	.04363
4	0	-0.60	.0075	1334.8	1.937	.99867	7.28404	.04363
5	0	-0.80	.0100	1335.2	1.690	.99808	7.25787	.08397
6	0	-1.00	.0125	1320.4	1.683	.99149	7.23170	.11055
7	0	-1.20	.0150	1320.4	1.676	.98790	7.20553	.13197
8	0	-1.40	.0175	1315.6	1.669	.98432	7.17936	.15043
9	0	-1.60	.0200	1307.8	1.662	.98074	7.15319	.16685
10	0	-1.80	.0225	1294.8	1.650	.97675	7.10957	.19150
11	0	-2.00	.0250	1288.4	1.629	.96398	7.03106	.22951
12	0	-2.20	.0275	1278.8	1.615	.95681	6.97817	.25945
13	0	-2.40	.0300	1269.2	1.602	.95016	6.94165	.28595
14	0	-2.60	.0325	1259.7	1.589	.94400	6.91042	.30764
15	0	-2.80	.0350	1250.1	1.575	.93848	6.88422	.32392
16	0	-3.00	.0375	1237.3	1.553	.92571	6.75191	.33392
17	0	-3.20	.0400	1221.3	1.530	.91375	6.56468	.36128
18	0	-3.40	.0425	1195.7	1.492	.87492	6.37680	.40158
19	0	-3.60	.0450	1181.8	1.398	.84578	6.17616	.43294
20	0	-3.80	.0475	1059.8	1.292	.79295	5.78361	.58536
21	0	-4.00	.0500	985.2	1.155	.72159	5.27765	.69587
22	180	-0.20	.0025	1336.5	1.700	.99975	7.28404	.04363
23	180	-0.40	.0050	1336.5	1.820	.99975	7.28404	.04363
24	180	-0.60	.0075	1336.5	1.940	.99975	7.28404	.04363
25	180	-0.80	.0100	1320.1	1.690	.99517	7.25852	.08319
26	180	-1.00	.0125	1322.1	1.678	.99278	7.24110	.10179
27	180	-1.20	.0150	1318.9	1.674	.98920	7.21496	.12466
28	180	-1.40	.0175	1315.6	1.668	.98561	7.18883	.14650
29	180	-1.60	.0200	1304.6	1.652	.97606	7.15190	.16639
30	180	-1.80	.0225	1296.6	1.641	.97008	7.07554	.18639
31	180	-2.00	.0250	1290.2	1.631	.96530	7.04068	.20875
32	180	-2.20	.0275	1279.0	1.615	.95930	6.94068	.22517
33	180	-2.40	.0300	1269.2	1.602	.95277	6.87450	.24233
34	180	-2.60	.0325	1259.7	1.589	.94600	6.82140	.26016
35	180	-2.80	.0350	1250.1	1.575	.93902	6.76184	.27869
36	180	-3.00	.0375	1238.9	1.556	.92707	6.68599	.30699
37	180	-3.20	.0400	1221.5	1.530	.91393	6.66599	.33088
38	180	-3.40	.0425	1197.6	1.495	.87570	6.48115	.38151
39	180	-3.60	.0450	1187.3	1.391	.84345	6.38115	.43941
40	180	-3.80	.0475	1053.5	1.297	.79566	5.80333	.58090
41	180	-4.00	.0500	988.5	1.128	.70964	5.15188	.69924
42	270	-1.00	.0125	1246.3	1.674	.98672	7.17595	.11750
43	270	-1.20	.0150	1246.3	1.674	.98672	7.17595	.11750
44	270	-1.40	.0175	1219.9	1.528	.91274	7.01554	.15680
45	270	-1.60	.0200	1219.9	1.528	.91274	7.01554	.15680
46	90	-1.25	.0243	1323.6	1.681	.99030	7.22297	.11811
47	90	-1.50	.0286	1290.9	1.651	.97375	7.03458	.15526
48	90	-1.75	.0329	1251.4	1.614	.95175	6.84669	.19318
49	90	-2.00	.0372	955.8	1.110	.70086	5.11191	.73107

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE V.- DATA^a FOR 160° CONE; $M_{\infty} = 2.30$ - Continued

(b) $\alpha = 5^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ, p_t = 2294.6 \text{ psf}$					$\Phi = 22.5^\circ, p_t = 2291.2 \text{ psf}$					$\Phi = 45.0^\circ, p_t = 2291.9 \text{ psf}$				
				p_t , psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}	M_t
1	0	-0.000	-0.000	1335.0	1.687	0.9369	7.24774	0.9312	1328.3	1.688	0.9390	7.24927	0.9352	1326.7	1.685	0.9320	7.23834	1.0443
2	0	-0.005	-0.005	1321.6	1.678	0.9892	7.21290	1.3187	1320.3	1.676	0.9890	7.20565	1.3187	1320.7	1.678	0.9882	7.21217	1.0443
3	0	-0.010	-0.010	1310.2	1.669	0.9892	7.17803	1.1850	1318.7	1.673	0.9893	7.17063	1.1850	1317.1	1.671	0.9853	7.18601	1.0443
4	0	-0.015	-0.015	1301.6	1.664	0.97697	7.12519	1.0709	1316.4	1.673	0.9893	7.13587	1.0709	1317.1	1.671	0.9824	7.18601	1.0443
5	0	-0.020	-0.020	1297.6	1.654	0.97219	7.10084	0.9853	1307.5	1.659	0.9735	7.11567	0.9853	1307.7	1.656	0.9784	7.18601	1.0443
6	0	-0.025	-0.025	1291.2	1.645	0.96742	7.07650	0.9225	1299.5	1.653	0.9639	7.09225	0.9225	1299.7	1.649	0.9747	7.10752	1.0443
7	0	-0.030	-0.030	1284.6	1.635	0.96265	7.05211	0.8639	1291.5	1.643	0.9639	7.06863	0.8639	1294.7	1.638	0.9684	7.10392	1.0443
8	0	-0.035	-0.035	1277.2	1.626	0.95788	7.02772	0.8053	1283.6	1.622	0.9601	7.00001	0.8053	1288.3	1.628	0.9637	7.02904	1.0443
9	0	-0.040	-0.040	1270.2	1.617	0.95311	7.00333	0.7467	1275.6	1.622	0.9602	6.90002	0.7467	1280.4	1.616	0.9573	7.04953	1.0443
10	0	-0.045	-0.045	1263.7	1.608	0.94834	6.97894	0.6881	1267.6	1.609	0.9602	6.84799	0.6881	1273.3	1.608	0.9544	7.07000	1.0443
11	0	-0.050	-0.050	1257.1	1.599	0.94357	6.95455	0.6295	1260.6	1.599	0.9588	6.84799	0.6295	1270.1	1.598	0.9516	7.09051	1.0443
12	0	-0.055	-0.055	1250.6	1.590	0.93880	6.93016	0.5709	1253.8	1.593	0.9588	6.84799	0.5709	1265.2	1.598	0.9488	7.11102	1.0443
13	0	-0.060	-0.060	1244.0	1.581	0.93403	6.90577	0.5123	1246.8	1.583	0.9588	6.84799	0.5123	1261.0	1.598	0.9468	7.13153	1.0443
14	0	-0.065	-0.065	1237.5	1.572	0.92926	6.88138	0.4537	1239.6	1.585	0.9588	6.84799	0.4537	1256.2	1.590	0.9448	7.15204	1.0443
15	0	-0.070	-0.070	1230.9	1.563	0.92449	6.85699	0.3951	1232.1	1.585	0.9588	6.84799	0.3951	1251.4	1.588	0.9428	7.17255	1.0443
16	0	-0.075	-0.075	1224.4	1.554	0.91972	6.83260	0.3365	1224.6	1.583	0.9588	6.84799	0.3365	1246.6	1.580	0.9408	7.19306	1.0443
17	0	-0.080	-0.080	1217.8	1.545	0.91495	6.80821	0.2779	1216.9	1.583	0.9588	6.84799	0.2779	1241.8	1.572	0.9388	7.21357	1.0443
18	0	-0.085	-0.085	1211.3	1.536	0.91018	6.78382	0.2193	1210.1	1.583	0.9588	6.84799	0.2193	1236.6	1.569	0.9368	7.23408	1.0443
19	0	-0.090	-0.090	1204.7	1.527	0.90541	6.75943	0.1607	1203.4	1.583	0.9588	6.84799	0.1607	1231.4	1.569	0.9348	7.25459	1.0443
20	0	-0.095	-0.095	1198.2	1.518	0.90064	6.73504	0.1021	1196.6	1.583	0.9588	6.84799	0.1021	1226.2	1.569	0.9328	7.27510	1.0443
21	0	-0.100	-0.100	1191.6	1.509	0.89587	6.71065	0.0435	1190.0	1.583	0.9588	6.84799	0.0435	1221.0	1.569	0.9308	7.29561	1.0443
22	180	-0.095	-0.095	1185.1	1.499	0.89110	6.68626	0.0849	1183.4	1.583	0.9588	6.84799	0.0849	1215.8	1.569	0.9288	7.31612	1.0443
23	180	-0.090	-0.090	1178.5	1.489	0.88633	6.66187	0.1263	1175.8	1.583	0.9588	6.84799	0.1263	1210.6	1.569	0.9268	7.33663	1.0443
24	180	-0.085	-0.085	1172.0	1.479	0.88156	6.63748	0.1677	1168.9	1.583	0.9588	6.84799	0.1677	1205.4	1.569	0.9248	7.35714	1.0443
25	180	-0.080	-0.080	1165.4	1.469	0.87679	6.61309	0.2091	1161.8	1.583	0.9588	6.84799	0.2091	1200.2	1.569	0.9228	7.37765	1.0443
26	180	-0.075	-0.075	1158.9	1.459	0.87202	6.58870	0.2505	1154.3	1.583	0.9588	6.84799	0.2505	1195.0	1.569	0.9208	7.39816	1.0443
27	180	-0.070	-0.070	1152.3	1.449	0.86725	6.56431	0.2919	1147.8	1.583	0.9588	6.84799	0.2919	1189.8	1.569	0.9188	7.41867	1.0443
28	180	-0.065	-0.065	1145.8	1.439	0.86248	6.53992	0.3333	1141.2	1.583	0.9588	6.84799	0.3333	1184.6	1.569	0.9168	7.43918	1.0443
29	180	-0.060	-0.060	1139.2	1.429	0.85771	6.51553	0.3747	1134.6	1.583	0.9588	6.84799	0.3747	1179.4	1.569	0.9148	7.45969	1.0443
30	180	-0.055	-0.055	1132.6	1.419	0.85294	6.49114	0.4161	1128.0	1.583	0.9588	6.84799	0.4161	1174.2	1.569	0.9128	7.48020	1.0443
31	180	-0.050	-0.050	1126.0	1.409	0.84817	6.46675	0.4575	1121.4	1.583	0.9588	6.84799	0.4575	1169.0	1.569	0.9108	7.50071	1.0443
32	180	-0.045	-0.045	1119.4	1.400	0.84340	6.44236	0.4989	1114.8	1.583	0.9588	6.84799	0.4989	1163.8	1.569	0.9088	7.52122	1.0443
33	180	-0.040	-0.040	1112.8	1.390	0.83863	6.41797	0.5403	1108.2	1.583	0.9588	6.84799	0.5403	1158.6	1.569	0.9068	7.54173	1.0443
34	180	-0.035	-0.035	1106.2	1.381	0.83386	6.39358	0.5817	1101.6	1.583	0.9588	6.84799	0.5817	1153.4	1.569	0.9048	7.56224	1.0443
35	180	-0.030	-0.030	1100.0	1.371	0.82909	6.36919	0.6231	1095.0	1.583	0.9588	6.84799	0.6231	1148.2	1.569	0.9028	7.58275	1.0443
36	180	-0.025	-0.025	1093.4	1.362	0.82432	6.34480	0.6645	1088.4	1.583	0.9588	6.84799	0.6645	1143.0	1.569	0.9008	7.60326	1.0443
37	180	-0.020	-0.020	1086.8	1.352	0.81955	6.32041	0.7059	1081.8	1.583	0.9588	6.84799	0.7059	1137.8	1.569	0.8988	7.62377	1.0443
38	180	-0.015	-0.015	1080.2	1.343	0.81478	6.29602	0.7473	1075.2	1.583	0.9588	6.84799	0.7473	1132.6	1.569	0.8968	7.64428	1.0443
39	180	-0.010	-0.010	1073.6	1.333	0.80999	6.27163	0.7887	1068.6	1.583	0.9588	6.84799	0.7887	1127.4	1.569	0.8948	7.66479	1.0443
40	180	-0.005	-0.005	1067.0	1.324	0.80522	6.24724	0.8301	1062.0	1.583	0.9588	6.84799	0.8301	1122.2	1.569	0.8928	7.68530	1.0443
41	180	-0.000	-0.000	1060.4	1.314	0.80045	6.22285	0.8715	1055.4	1.583	0.9588	6.84799	0.8715	1117.0	1.569	0.8908	7.70581	1.0443
42	270	-0.000	-0.000	1053.8	1.305	0.79568	6.19846	0.9129	1048.8	1.583	0.9588	6.84799	0.9129	1111.8	1.569	0.8888	7.72632	1.0443
43	270	-0.005	-0.005	1047.2	1.295	0.79091	6.17407	0.9543	1042.2	1.583	0.9588	6.84799	0.9543	1106.6	1.569	0.8868	7.74683	1.0443
44	270	-0.010	-0.010	1040.6	1.286	0.78614	6.14968	0.9957	1035.6	1.583	0.9588	6.84799	0.9957	1101.4	1.569	0.8848	7.76734	1.0443
45	270	-0.015	-0.015	1034.0	1.276	0.78137	6.12529	1.0371	1029.0	1.583	0.9588	6.84799	1.0371	1096.2	1.569	0.8828	7.78785	1.0443
46	90	-0.020	-0.020	1027.4	1.267	0.77660	6.10090	1.0785	1022.4	1.583	0.9588	6.84799	1.0785	1091.0	1.569	0.8808	7.80836	1.0443
47	90	-0.025	-0.025	1020.8	1.257	0.77183	6.07651	1.1199	1015.8	1.583	0.9588	6.84799	1.1199	1085.8	1.569	0.8788	7.82887	1.0443
48	90	-0.030	-0.030	1014.2	1.248	0.76706	6.05212	1.1613	1009.2	1.583	0.9588	6.84799	1.1613	1080.6	1.569	0.8768	7.84938	1.0443
49	90	-0.035	-0.035	1007.6	1.238	0.76229	6.02773	1.2027	1002.6	1.583	0.9588	6.84799	1.2027	1075.4	1.569	0.8748	7.86989	1.0443
50	90	-0.040	-0.040	1001.0	1.229	0.75752	6.00334	1.2441	996.0	1.583	0.9588	6.84799	1.2441	1070.2	1.569	0.8728	7.89040	1.0443

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE V.- DATA^a FOR 160° CONE; $M_{\infty} = 2.30$ - Continued(b) $\alpha = 5^\circ$ - Concluded

Orifice 1	θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ$, $p_t = 2293.3$ psf				$\phi = 90.0^\circ$, $p_t = 2295.8$ psf			
					p_t , psf	C_p	$p_t/p_{t,2}$	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	M_t
1	0	0.200	0.000	-0.000	1328.2	1.686	0.9292	7.24213	1329.8	1.686	0.9304	7.24295
2	0	0.400	0.025	-0.043	1325.0	1.681	0.9053	7.22470	1328.2	1.686	0.93184	7.23424
3	0	0.600	0.050	-0.085	1318.6	1.679	0.8834	7.21598	1326.6	1.681	0.9055	7.22553
4	0	0.800	0.075	-0.148	1310.4	1.672	0.8575	7.19584	1320.2	1.672	0.8834	7.20553
5	0	1.000	0.100	-0.241	1302.6	1.660	0.8278	7.16627	1317.0	1.672	0.8575	7.19072
6	0	1.200	0.150	-0.356	1302.6	1.648	0.7938	7.12627	1312.6	1.658	0.8331	7.17331
7	0	1.400	0.175	-0.498	1297.8	1.641	0.7622	7.07655	1304.2	1.648	0.8094	7.13848
8	0	1.600	0.200	-0.664	1289.9	1.629	0.7255	7.01627	1294.2	1.638	0.7859	7.10366
9	0	1.800	0.225	-0.854	1279.5	1.617	0.6845	6.94627	1281.5	1.629	0.7531	7.06884
10	0	2.000	0.250	-1.064	1267.7	1.601	0.6393	6.87039	1265.0	1.618	0.7199	7.03402
11	0	2.200	0.275	-1.291	1254.3	1.587	0.5924	6.78947	1250.0	1.618	0.6862	6.99049
12	0	2.400	0.300	-1.534	1240.3	1.568	0.5438	6.70338	1240.7	1.599	0.6527	6.94887
13	0	2.600	0.325	-1.791	1225.5	1.549	0.4924	6.61204	1231.1	1.585	0.6191	6.90887
14	0	2.800	0.350	-2.059	1210.9	1.529	0.4382	6.51630	1220.7	1.565	0.5859	6.86987
15	0	3.000	0.375	-2.336	1197.4	1.500	0.3815	6.41630	1210.7	1.540	0.5527	6.83138
16	0	3.200	0.400	-2.621	1184.8	1.460	0.3222	6.31244	1201.7	1.517	0.5194	6.79351
17	0	3.400	0.425	-2.914	1174.6	1.420	0.2615	6.20549	1192.0	1.479	0.4862	6.75616
18	0	3.600	0.450	-3.214	1165.2	1.372	0.1994	6.09570	1182.6	1.439	0.4531	6.71947
19	0	3.800	0.475	-3.519	1156.4	1.316	0.1364	5.98344	1173.6	1.385	0.4200	6.68326
20	0	4.000	0.500	-3.828	1148.2	1.252	0.0728	5.86847	1165.0	1.284	0.3869	6.64767
21	0	4.200	0.525	-4.141	1140.6	1.180	0.0094	5.75144	1156.5	1.284	0.3538	6.61265
22	180	4.000	0.500	-3.828	1148.2	1.252	0.0728	5.86847	1165.0	1.284	0.3869	6.64767
23	180	4.200	0.525	-4.141	1140.6	1.180	0.0094	5.75144	1156.5	1.284	0.3538	6.61265
24	180	4.400	0.550	-4.454	1133.5	1.109	0.0454	5.63444	1148.2	1.284	0.3207	6.57767
25	180	4.600	0.575	-4.767	1126.4	1.038	0.0819	5.51744	1139.7	1.284	0.2876	6.54267
26	180	4.800	0.600	-5.080	1119.3	0.967	0.1184	5.40044	1131.2	1.284	0.2545	6.50767
27	180	5.000	0.625	-5.393	1112.2	0.896	0.1549	5.28344	1122.7	1.284	0.2214	6.47267
28	180	5.200	0.650	-5.706	1105.1	0.825	0.1914	5.16644	1114.2	1.284	0.1883	6.43767
29	180	5.400	0.675	-6.019	1098.0	0.754	0.2279	5.04944	1105.7	1.284	0.1552	6.40267
30	180	5.600	0.700	-6.332	1090.9	0.683	0.2644	4.93244	1097.2	1.284	0.1221	6.36767
31	180	5.800	0.725	-6.645	1083.8	0.612	0.3009	4.81544	1088.7	1.284	0.0890	6.33267
32	180	6.000	0.750	-6.958	1076.7	0.541	0.3374	4.69844	1080.2	1.284	0.0559	6.29767
33	180	6.200	0.775	-7.271	1069.6	0.470	0.3739	4.58144	1071.7	1.284	0.0228	6.26267
34	180	6.400	0.800	-7.584	1062.5	0.400	0.4104	4.46444	1063.2	1.284	0.0000	6.22767
35	180	6.600	0.825	-7.897	1055.4	0.329	0.4469	4.34744	1054.7	1.284	0.0000	6.19267
36	180	6.800	0.850	-8.210	1048.3	0.258	0.4834	4.23044	1046.2	1.284	0.0000	6.15767
37	180	7.000	0.875	-8.523	1041.2	0.187	0.5199	4.11344	1037.7	1.284	0.0000	6.12267
38	180	7.200	0.900	-8.836	1034.1	0.116	0.5564	4.00044	1029.2	1.284	0.0000	6.08767
39	180	7.400	0.925	-9.149	1027.0	0.045	0.5929	3.88744	1020.7	1.284	0.0000	6.05267
40	180	7.600	0.950	-9.462	1019.9	0.000	0.6294	3.77444	1012.2	1.284	0.0000	6.01767
41	180	7.800	0.975	-9.775	1012.8	0.000	0.6659	3.66144	1003.7	1.284	0.0000	5.98267
42	270	7.200	0.900	-8.836	1027.0	0.045	0.5929	3.88744	1020.7	1.284	0.0000	6.05267
43	270	7.400	0.925	-9.149	1019.9	0.000	0.6294	3.77444	1012.2	1.284	0.0000	6.01767
44	270	7.600	0.950	-9.462	1012.8	0.000	0.6659	3.66144	1003.7	1.284	0.0000	5.98267
45	270	7.800	0.975	-9.775	1005.7	0.000	0.7024	3.54844	995.2	1.284	0.0000	5.94767
46	270	8.000	1.000	-10.088	998.6	0.000	0.7389	3.43544	986.7	1.284	0.0000	5.91267
47	90	2.000	0.250	-2.463	1301.0	1.582	0.9261	7.09398	1301.0	1.582	0.9261	7.09398
48	90	2.000	0.250	-2.463	1297.8	1.582	0.9261	7.09398	1297.8	1.582	0.9261	7.09398
49	90	4.000	0.500	-3.828	1148.2	1.252	0.0728	5.86847	1148.2	1.252	0.0728	5.86847
50	90	4.000	0.500	-3.828	901.5	1.057	0.5950	4.91324	901.5	1.057	0.5950	4.91324

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE V.- DATA^a FOR 160° CONE; $M_{\infty} = 2.30$ - Continued

(c) $\alpha = 10^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, p_t = 2290.8 \text{ psf}$				$\phi = 22.5^\circ, p_t = 2291.4 \text{ psf}$				$\phi = 45.0^\circ, p_t = 2293.8 \text{ psf}$						
				p_t/psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,0}$	M_t	p_t/psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,0}$	M_t	p_t/psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,0}$	M_t
1	0	.030	.0000	1306.4	1.653	.97620	7.12016	-1.8582	1306.2	1.652	.97576	7.11698	-1.8754	1304.3	1.650	.97486	7.11035	-1.9108
2	0	.230	.0025	1293.2	1.636	.96783	7.05908	-2.1665	1294.6	1.638	.96858	7.06459	-2.2104	1293.4	1.641	.97008	7.07549	-2.0878
3	0	.430	.0050	1281.6	1.629	.96456	7.03290	-2.5390	1291.4	1.638	.96819	7.04712	-2.2222	1293.1	1.641	.97072	7.08599	-2.0778
4	0	.630	.0075	1270.0	1.621	.96129	6.99800	-2.9119	1281.6	1.631	.96819	7.03446	-2.2822	1293.1	1.643	.97099	7.10321	-2.0300
5	0	.830	.0100	1258.4	1.608	.95347	6.93692	-3.2847	1270.0	1.621	.96200	7.00157	-2.3422	1293.0	1.640	.96932	7.10231	-2.0049
6	0	1.030	.0125	1246.8	1.596	.94749	6.85374	-3.6574	1258.4	1.612	.94943	6.92487	-2.4022	1292.6	1.638	.96779	7.09479	-2.0007
7	0	1.230	.0150	1235.2	1.584	.94151	6.75974	-4.0301	1246.8	1.600	.94493	6.87129	-2.4622	1292.0	1.636	.96746	7.09044	-2.0000
8	0	1.430	.0175	1223.6	1.572	.93553	6.65571	-4.4028	1235.2	1.588	.93895	6.81781	-2.5222	1291.6	1.634	.96738	7.08994	-2.0000
9	0	1.630	.0200	1212.0	1.560	.92955	6.54171	-4.7755	1223.6	1.576	.93297	6.76433	-2.5822	1291.0	1.632	.96738	7.08994	-2.0000
10	0	1.830	.0225	1200.4	1.548	.92357	6.41771	-5.1482	1212.0	1.564	.92699	6.71085	-2.6422	1290.6	1.630	.96738	7.08994	-2.0000
11	0	2.030	.0250	1188.8	1.521	.90921	6.03152	-5.5209	1200.4	1.552	.92069	6.65737	-2.7022	1290.0	1.628	.96738	7.08994	-2.0000
12	0	2.230	.0275	1177.2	1.504	.90083	5.87044	-5.8936	1188.8	1.540	.91227	6.60391	-2.7622	1289.6	1.626	.96738	7.08994	-2.0000
13	0	2.430	.0300	1165.6	1.487	.89245	5.70936	-6.2663	1177.2	1.528	.90389	6.55045	-2.8222	1289.0	1.624	.96738	7.08994	-2.0000
14	0	2.630	.0325	1154.0	1.470	.88407	5.54828	-6.6390	1165.6	1.516	.89551	6.49699	-2.8822	1288.4	1.622	.96738	7.08994	-2.0000
15	0	2.830	.0350	1142.4	1.453	.87569	5.38720	-7.0117	1154.0	1.504	.88713	6.44353	-2.9422	1287.8	1.620	.96738	7.08994	-2.0000
16	0	3.030	.0375	1130.8	1.436	.86731	5.22612	-7.3844	1142.4	1.492	.87867	6.39007	-3.0000	1287.2	1.618	.96738	7.08994	-2.0000
17	0	3.230	.0400	1119.2	1.419	.85893	5.06504	-7.7571	1130.8	1.480	.87021	6.33661	-3.0599	1286.6	1.616	.96738	7.08994	-2.0000
18	0	3.430	.0425	1107.6	1.402	.85055	4.90396	-8.1298	1119.2	1.468	.86175	6.28315	-3.1199	1286.0	1.614	.96738	7.08994	-2.0000
19	0	3.630	.0450	1096.0	1.385	.84217	4.74288	-8.5025	1107.6	1.456	.85329	6.22969	-3.1799	1285.4	1.612	.96738	7.08994	-2.0000
20	0	3.830	.0475	1084.4	1.368	.83379	4.58180	-8.8752	1096.0	1.444	.84483	6.17623	-3.2399	1284.8	1.610	.96738	7.08994	-2.0000
21	180	2.30	.025	1318.8	1.684	.99663	7.26914	-6.8064	1318.8	1.682	.99749	7.27545	-6.7788	1309.2	1.674	.99048	7.26701	-6.9092
22	180	2.50	.0275	1307.2	1.667	.98825	7.10806	-7.1791	1307.2	1.665	.98910	7.11437	-7.1484	1309.0	1.672	.99048	7.26701	-6.9092
23	180	2.70	.030	1295.6	1.650	.97987	6.94698	-7.5494	1295.6	1.648	.98071	7.02068	-7.5180	1308.8	1.670	.99048	7.26701	-6.9092
24	180	2.90	.0325	1284.0	1.633	.97149	6.78590	-7.9197	1284.0	1.631	.97232	6.92699	-7.8877	1308.6	1.668	.99048	7.26701	-6.9092
25	180	3.10	.0350	1272.4	1.616	.96311	6.62482	-8.2899	1272.4	1.614	.96405	6.83331	-8.2573	1308.4	1.666	.99048	7.26701	-6.9092
26	180	3.30	.0375	1260.8	1.599	.95473	6.46374	-8.6602	1260.8	1.597	.95567	6.73962	-8.6269	1308.2	1.664	.99048	7.26701	-6.9092
27	180	3.50	.0400	1249.2	1.582	.94635	6.30266	-9.0305	1249.2	1.580	.94729	6.64593	-9.0062	1308.0	1.662	.99048	7.26701	-6.9092
28	180	3.70	.0425	1237.6	1.565	.93797	6.14158	-9.4008	1237.6	1.563	.93891	6.55224	-9.3759	1307.8	1.660	.99048	7.26701	-6.9092
29	180	3.90	.0450	1226.0	1.548	.92959	5.98050	-9.7711	1226.0	1.546	.93053	6.45855	-9.7456	1307.6	1.658	.99048	7.26701	-6.9092
30	180	4.10	.0475	1214.4	1.531	.92121	5.81942	-10.1414	1214.4	1.529	.92216	6.36487	-10.1152	1307.4	1.656	.99048	7.26701	-6.9092
31	180	4.30	.0500	1202.8	1.514	.91283	5.65834	-10.5117	1202.8	1.512	.91378	6.27119	-10.4849	1307.2	1.654	.99048	7.26701	-6.9092
32	180	4.50	.0525	1191.2	1.497	.90445	5.49726	-10.8820	1191.2	1.495	.90537	6.17751	-10.8546	1307.0	1.652	.99048	7.26701	-6.9092
33	180	4.70	.0550	1179.6	1.480	.89607	5.33618	-11.2523	1179.6	1.478	.89700	6.08383	-11.2242	1306.8	1.650	.99048	7.26701	-6.9092
34	180	4.90	.0575	1168.0	1.463	.88769	5.17510	-11.6226	1168.0	1.461	.88862	5.99007	-11.5943	1306.6	1.648	.99048	7.26701	-6.9092
35	180	5.10	.0600	1156.4	1.446	.87931	5.01402	-11.9929	1156.4	1.444	.88024	5.89631	-11.9640	1306.4	1.646	.99048	7.26701	-6.9092
36	180	5.30	.0625	1144.8	1.429	.87093	4.85294	-12.3632	1144.8	1.427	.87186	5.78801	-12.3337	1306.2	1.644	.99048	7.26701	-6.9092
37	180	5.50	.0650	1133.2	1.412	.86255	4.69186	-12.7335	1133.2	1.410	.86348	5.67370	-12.7034	1306.0	1.642	.99048	7.26701	-6.9092
38	180	5.70	.0675	1121.6	1.395	.85417	4.53078	-13.1038	1121.6	1.393	.85510	5.55939	-13.0731	1305.8	1.640	.99048	7.26701	-6.9092
39	180	5.90	.0700	1110.0	1.378	.84579	4.36970	-13.4741	1110.0	1.376	.84672	5.44599	-13.4428	1305.6	1.638	.99048	7.26701	-6.9092
40	180	6.10	.0725	1098.4	1.361	.83741	4.20862	-13.8444	1098.4	1.359	.83834	5.33375	-13.8125	1305.4	1.636	.99048	7.26701	-6.9092
41	270	3.000	.375	928.8	1.090	.89028	6.50372	-7.4738	928.4	1.088	.89120	6.40946	-7.5338	915.1	1.086	.99048	7.26701	-6.9092
42	270	3.200	.400	917.2	1.073	.88190	6.34264	-7.8441	916.8	1.071	.88282	6.28517	-7.8941	914.9	1.084	.99048	7.26701	-6.9092
43	270	3.400	.425	905.6	1.056	.87352	6.18156	-8.2144	905.2	1.054	.87384	6.16087	-8.2544	914.0	1.082	.99048	7.26701	-6.9092
44	270	3.600	.450	894.0	1.039	.86514	6.02048	-8.5847	893.6	1.037	.86416	6.03658	-8.6147	913.1	1.080	.99048	7.26701	-6.9092
45	270	3.800	.475	882.4	1.022	.85676	5.85940	-8.9550	882.0	1.020	.85518	5.91229	-8.9750	912.2	1.078	.99048	7.26701	-6.9092
46	270	4.000	.500	870.8	1.005	.84838	5.69832	-9.3253	870.4	1.003	.84660	5.78801	-9.3353	911.3	1.076	.99048	7.26701	-6.9092
47	270	4.200	.525	859.2	0.988	.83999	5.53724	-9.6956	858.8	0.986	.83782	5.67370	-9.6956	910.4	1.074	.99048	7.26701	-6.9092
48	270	4.400	.550	847.6	0.971	.83161	5.37616	-10.0659	847.2	0.969	.82944	5.55939	-10.0559	909.5	1.072	.99048	7.26701	-6.9092
49	270	4.600	.575	836.0	0.954	.82323	5.21508	-10.4362	835.6	0.952	.82126	5.44599	-10.4262	908.6	1.070	.99048	7.26701	-6.9092
50	270	4.800	.600	824.4	0.937	.81485	5.05400	-10.8065	824.0	0.935	.81328	5.33375	-10.8065	907.7	1.068	.99048	7.26701	-6.9092

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE V.- DATA^a FOR 160° CONE; $M_{\infty} = 2.30$ - Continued(c) $\alpha = 10^\circ$ - Concluded

Office	θ , deg	s , in.	s/D	s/s^*	$\Phi = 67.5^\circ$, $P_t = 2294.8$ psf				$\Phi = 90.0^\circ$, $P_t = 2295.1$ psf					
					P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t	
1	0	230	.000	.0000	1304.3	1.649	.97443	7.10725	1.9272	1305.8	1.651	.97543	7.11454	1.8885
2	0	230	.025	.0493	1331.1	1.645	.97204	7.08993	1.9268	1304.2	1.649	.97424	7.10583	1.9346
3	0	230	.050	.0985	1297.9	1.640	.96965	7.07229	1.9187	1304.2	1.649	.97424	7.10583	1.9346
4	0	230	.075	.1478	1284.7	1.635	.96727	7.05499	1.9105	1304.2	1.649	.97424	7.10583	1.9346
5	0	230	.100	.1970	1271.5	1.630	.96488	7.03757	1.9023	1304.2	1.644	.97185	7.08841	2.0239
6	0	1300	.125	.2463	1258.3	1.619	.95989	6.99047	2.8557	1237.8	1.639	.96946	7.07100	2.0196
7	0	1300	.150	.2956	1245.1	1.607	.95490	6.95024	2.8333	1231.1	1.632	.96588	7.04647	2.2326
8	0	1300	.175	.3448	1231.9	1.600	.94991	6.90959	2.8109	1224.8	1.628	.96349	7.02746	2.3112
9	0	1300	.200	.3941	1218.7	1.598	.94492	6.86895	2.7885	1218.5	1.628	.96349	7.02746	2.3112
10	0	1300	.225	.4434	1205.5	1.596	.93993	6.82832	2.7661	1212.3	1.627	.96109	6.99874	2.3998
11	0	2200	.250	.4926	1192.3	1.582	.93494	6.78749	3.3206	1256.9	1.592	.94558	6.89683	2.8368
12	0	2200	.275	.5419	1179.1	1.548	.92108	6.73273	3.3008	1256.3	1.578	.93862	6.84548	3.0270
13	0	2400	.300	.5912	1165.9	1.529	.90715	6.67595	3.2811	1245.1	1.562	.93006	6.78363	3.2151
14	0	2400	.325	.6404	1152.7	1.526	.90199	6.62920	3.2614	1238.9	1.562	.92766	6.73273	3.4032
15	0	2800	.350	.6897	1139.5	1.482	.88965	6.48885	4.2125	1217.6	1.522	.90976	6.63559	3.7006
16	0	3200	.375	.7389	1126.3	1.456	.87651	6.39304	4.3805	1200.3	1.476	.89643	6.50918	3.9760
17	0	3200	.400	.7882	1113.1	1.419	.85740	6.25368	4.7401	1176.4	1.461	.88732	6.43376	4.3376
18	0	3200	.425	.8375	1100.0	1.379	.83710	6.10562	5.1047	1147.2	1.421	.86863	6.35114	4.7213
19	0	3400	.450	.8867	1086.8	1.326	.81598	5.95968	5.4694	1105.3	1.268	.83732	6.25111	5.0517
20	0	3800	.475	.9360	1073.6	1.226	.79568	5.81944	6.8344	1045.3	1.201	.80929	6.15651	6.0519
21	0	4200	.500	.9852	1060.4	1.094	.69261	5.05122	9.9342	934.2	1.134	.71277	5.19875	7.1266
22	180	220	.025	.0493	1312.5	1.661	.98051	7.15156	1.6794	1306.0	1.651	.97554	7.11534	1.8842
23	180	2400	.050	.0985	1316.1	1.664	.98170	7.15026	1.6794	1304.4	1.649	.97435	7.10664	1.9304
24	180	2600	.075	.1478	1319.7	1.664	.98170	7.14896	1.6794	1302.2	1.644	.97182	7.08744	2.0195
25	180	2800	.100	.1970	1323.3	1.664	.98170	7.14766	1.6794	1300.2	1.644	.97182	7.08744	2.0195
26	180	1300	.125	.2463	1326.9	1.659	.97931	7.14286	1.7307	1299.6	1.642	.97077	7.08054	2.2280
27	180	1300	.150	.2956	1330.5	1.657	.97812	7.13416	1.7806	1293.2	1.633	.96600	7.04575	2.2785
28	180	1400	.175	.3448	1334.1	1.652	.97573	7.11676	1.8765	1290.0	1.628	.96361	7.02835	2.3072
29	180	1500	.200	.3941	1337.7	1.649	.97334	7.09936	2.1605	1285.7	1.624	.96122	6.99855	2.4777
30	180	1600	.225	.4434	1341.3	1.646	.97095	7.08436	2.1605	1279.5	1.621	.95883	6.97355	2.6477
31	180	2200	.250	.4926	1344.9	1.631	.96856	6.95000	2.6118	1257.7	1.595	.94652	6.90058	2.8023
32	180	2200	.275	.5419	1348.5	1.619	.95904	6.90496	2.6518	1259.1	1.581	.93976	6.85438	2.9925
33	180	2400	.300	.5912	1352.1	1.605	.95188	6.84276	2.6637	1246.9	1.565	.93141	6.79350	3.2022
34	180	2600	.325	.6404	1355.7	1.593	.94729	6.80156	2.6637	1246.9	1.565	.93141	6.79350	3.2022
35	180	2800	.350	.6897	1359.3	1.589	.94678	6.79276	2.6637	1246.9	1.565	.93141	6.79350	3.2022
36	180	3000	.375	.7389	1362.9	1.546	.92026	6.72525	3.3246	1208.2	1.499	.89802	6.54994	3.9503
37	180	3200	.400	.7882	1366.5	1.513	.90536	6.60345	3.3246	1178.3	1.464	.88013	6.41946	4.3101
38	180	3400	.425	.8375	1370.1	1.476	.88627	6.46455	4.1981	1151.1	1.424	.85986	6.27159	4.6949
39	180	3600	.450	.8867	1373.7	1.463	.88265	6.45056	4.1981	1151.1	1.424	.85986	6.27159	4.6949
40	180	3800	.475	.9360	1377.3	1.451	.87924	6.43657	4.1981	1151.1	1.424	.85986	6.27159	4.6949
41	270	1030	.125	.2463	1333.2	1.692	.99601	7.26467	1.9570	1306.0	1.703	.99787	7.26860	1.9700
42	270	1030	.250	.4926	1326.8	1.682	.99124	7.22987	1.9121	1334.7	1.694	.99701	7.27191	1.9654
43	270	1030	.375	.7389	1320.4	1.672	.98647	7.19504	1.8694	1328.3	1.682	.99361	7.22835	2.3072
44	270	1030	.500	.9852	1314.0	1.662	.98170	7.16027	1.8694	1321.9	1.682	.99361	7.22835	2.3072
45	90	1300	.125	.2463	1267.6	1.595	.94669	6.90692	2.9010	1257.5	1.595	.94678	6.85459	2.8621
46	90	1300	.250	.4926	1261.2	1.592	.94430	6.86962	2.9010	1257.5	1.592	.94678	6.85459	2.8621
47	90	2300	.375	.7389	1254.8	1.589	.94191	6.82999	3.6946	1217.6	1.589	.94678	6.85459	2.8621
48	90	3300	.500	.9852	1248.4	1.586	.93952	6.78749	4.6473	1136.4	1.402	.84887	6.49490	4.8952
49	90	4300	.500	.9852	866.8	1.005	.64723	4.72073	8.1350	863.1	1.000	.64473	4.70239	8.1737

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE V.- DATA^a FOR 160° CONE; $M_{\infty} = 2.30$ - Continued

(d) $\alpha = 15^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\phi = 0, 0.0^\circ, P_t = 2295.7 \text{ psf}$				
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,0}$	M_t
1	0	.200	.0000	1266.1	1.592	.94547	6.89599	.28418
2	0	.400	.0025	1284.9	1.576	.93711	6.83504	.30604
3	0	.600	.0050	1291.7	1.571	.93472	6.81763	.31205
4	0	.800	.0075	1294.8	1.559	.92875	6.77409	.32667
5	0	1.000	.0100	1294.8	1.548	.92458	6.71505	.34078
6	0	1.200	.0125	1291.7	1.536	.90846	6.68702	.35443
7	0	1.400	.0150	1286.5	1.519	.90466	6.62607	.37289
8	0	1.600	.0175	1265.9	1.499	.89430	6.57383	.38818
9	0	1.800	.0200	1195.7	1.489	.89294	6.51288	.40548
10	0	2.000	.0225	1184.7	1.472	.88458	6.45193	.42226
11	0	2.200	.0250	1171.7	1.453	.87503	6.38227	.44069
12	0	2.400	.0275	1159.0	1.435	.86548	6.31262	.45902
13	0	2.600	.0300	1143.0	1.411	.85355	6.22555	.48106
14	0	2.800	.0325	1128.6	1.390	.84280	6.14718	.50039
15	0	3.000	.0350	1105.5	1.369	.83255	6.07383	.51887
16	0	3.200	.0375	1093.4	1.338	.81456	5.95563	.53598
17	0	3.400	.0400	1063.0	1.294	.79386	5.77019	.58387
18	0	3.600	.0425	1039.1	1.258	.77595	5.65959	.61305
19	0	3.800	.0450	1005.5	1.209	.75088	5.47674	.65308
20	0	4.000	.0475	983.2	1.165	.72842	5.31845	.69586
21	0	4.200	.0500	983.2	1.000	.64464	4.70181	.81749
22	180	.200	.0025	1293.4	1.632	.96588	7.04489	.22325
23	180	.400	.0050	1309.4	1.656	.97780	7.13186	.17935
24	180	.600	.0075	1318.9	1.670	.98496	7.18405	.15730
25	180	.800	.0100	1321.7	1.679	.98973	7.21884	.12153
26	180	1.000	.0125	1331.7	1.689	.99450	7.25762	.08881
27	180	1.200	.0150	1338.1	1.693	.99688	7.27102	.06679
28	180	1.400	.0175	1344.8	1.698	.99927	7.28842	.03233
29	180	1.600	.0200	1341.3	1.703	1.00165	7.30581	.00000
30	180	1.800	.0225	1341.3	1.703	1.00165	7.30581	.00000
31	180	2.000	.0250	1341.3	1.703	1.00165	7.30581	.00000
32	180	2.200	.0275	1341.3	1.703	1.00165	7.30581	.00000
33	180	2.400	.0300	1341.3	1.703	1.00165	7.30581	.00000
34	180	2.600	.0325	1341.3	1.703	1.00165	7.30581	.00000
35	180	2.800	.0350	1341.3	1.703	1.00165	7.30581	.00000
36	180	3.000	.0375	1341.3	1.703	1.00165	7.30581	.00000
37	180	3.200	.0400	1341.3	1.703	1.00165	7.30581	.00000
38	180	3.400	.0425	1341.3	1.703	1.00165	7.30581	.00000
39	180	3.600	.0450	1341.3	1.703	1.00165	7.30581	.00000
40	180	3.800	.0475	1341.3	1.703	1.00165	7.30581	.00000
41	180	4.000	.0500	1341.3	1.703	1.00165	7.30581	.00000
42	270	1.000	.0125	1267.8	1.595	.94680	6.90573	.28055
43	270	2.000	.0250	1242.3	1.557	.92772	6.76657	.32914
44	270	3.000	.0375	1181.6	1.478	.89441	6.58171	.40548
45	270	4.000	.0500	1097.8	1.378	.84666	6.49230	.47562
46	90	1.000	.0125	1257.7	1.595	.94666	6.90470	.28094
47	90	2.000	.0250	1262.1	1.557	.92756	6.76538	.32953
48	90	3.000	.0375	1181.3	1.468	.88220	6.43452	.42697
49	90	4.000	.0500	995.6	1.068	.67926	4.94532	.76433

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE V. - DATA^a FOR 160° CONE; $M_{\infty} = 2.30$ - Continued(e) $\alpha = 20^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ, p_t = 2291.4$ psf					$\Phi = 22.5^\circ, p_t = 2291.5$ psf					$\Phi = 45.0^\circ, p_t = 2292.9$ psf				
				$p_{t,c}$ psf	C_p	$p_{t,c}/p_{t,2}$	$p_{t,c}/p_\infty$	$M_{t,c}$	$p_{t,c}$ psf	C_p	$p_{t,c}/p_{t,2}$	$p_{t,c}/p_\infty$	$M_{t,c}$	$p_{t,c}$ psf	C_p	$p_{t,c}/p_{t,2}$	$p_{t,c}/p_\infty$	$M_{t,c}$
1	0	-0.20	-0.000	1205.2	1.506	0.90173	6.57698	-3.8727	1206.8	1.508	0.90289	6.58542	-3.8483	1207.1	1.508	0.90253	6.58280	-3.8559
2	0	-0.25	-0.003	1192.4	1.487	0.89216	6.50720	-4.0706	1195.6	1.492	0.89451	6.52436	-4.0226	1197.5	1.494	0.89536	6.52800	-4.0052
3	0	-0.50	-0.085	1194.0	1.490	0.89336	6.51592	-4.0662	1195.6	1.492	0.89451	6.52436	-4.0226	1197.5	1.494	0.89536	6.52800	-4.0052
4	0	-0.75	-0.147	1197.7	1.498	0.89579	6.48103	-4.1413	1190.8	1.485	0.89095	6.50550	-4.0755	1187.9	1.479	0.88820	6.51314	-4.0450
5	0	-1.00	-0.191	1197.7	1.498	0.89579	6.48103	-4.1413	1190.8	1.485	0.89095	6.50550	-4.0755	1187.9	1.479	0.88820	6.51314	-4.0450
6	0	-1.25	-0.243	1173.1	1.454	0.87542	6.38508	-4.4015	1176.9	1.461	0.87897	6.41097	-4.3328	1181.5	1.470	0.88343	6.44348	-4.2555
7	0	-1.50	-0.296	1162.1	1.442	0.85944	6.34147	-4.5157	1166.9	1.449	0.87259	6.36736	-4.4682	1173.6	1.458	0.87746	6.39995	-4.3822
8	0	-1.75	-0.344	1154.1	1.431	0.85346	6.29785	-4.6280	1157.3	1.435	0.85581	6.31502	-4.5940	1165.6	1.447	0.87149	6.37561	-4.4768
9	0	-2.00	-0.394	1150.1	1.420	0.84748	6.25426	-4.7403	1151.5	1.424	0.84977	6.28181	-4.7525	1159.9	1.427	0.86592	6.31287	-4.5896
10	0	-2.25	-0.434	1144.1	1.410	0.84150	6.21067	-4.8526	1145.9	1.413	0.84379	6.23836	-4.8648	1153.7	1.416	0.86592	6.31287	-4.5896
11	0	-2.50	-0.476	1138.1	1.400	0.83552	6.16707	-4.9649	1139.9	1.402	0.83787	6.19591	-4.9771	1147.5	1.404	0.86592	6.31287	-4.5896
12	0	-2.75	-0.519	1132.1	1.390	0.82954	6.12348	-5.0772	1133.7	1.386	0.83113	6.13185	-5.0894	1141.1	1.404	0.86592	6.31287	-4.5896
13	0	-3.00	-0.562	1126.1	1.380	0.82356	6.07989	-5.1895	1127.3	1.387	0.83113	6.13185	-5.0894	1141.1	1.404	0.86592	6.31287	-4.5896
14	0	-3.25	-0.604	1120.1	1.370	0.81758	6.03630	-5.3018	1121.5	1.376	0.82472	6.08722	-5.1017	1134.7	1.388	0.84164	6.13812	-5.0425
15	0	-3.50	-0.647	1114.1	1.360	0.81160	5.99271	-5.4141	1115.7	1.366	0.82472	6.08722	-5.1017	1134.7	1.388	0.84164	6.13812	-5.0425
16	0	-3.75	-0.689	1108.1	1.350	0.80562	5.94862	-5.5264	1109.3	1.356	0.82954	6.07989	-5.1895	1128.9	1.379	0.82104	6.10822	-5.0915
17	0	-4.00	-0.732	1102.1	1.340	0.79964	5.90503	-5.6387	1103.5	1.346	0.82954	6.07989	-5.1895	1128.9	1.379	0.82104	6.10822	-5.0915
18	0	-4.25	-0.775	1096.1	1.330	0.79366	5.86144	-5.7510	1097.9	1.346	0.82954	6.07989	-5.1895	1128.9	1.379	0.82104	6.10822	-5.0915
19	0	-4.50	-0.818	1090.1	1.320	0.78768	5.81785	-5.8633	1091.7	1.327	0.78938	5.82965	-5.2140	1116.9	1.324	0.80941	5.90362	-5.5802
20	0	-4.75	-0.861	1084.1	1.310	0.78170	5.77426	-5.9756	1085.5	1.317	0.78938	5.82965	-5.2140	1116.9	1.324	0.80941	5.90362	-5.5802
21	0	-5.00	-0.904	1078.1	1.300	0.77572	5.73067	-6.0879	1079.9	1.307	0.78938	5.82965	-5.2140	1116.9	1.324	0.80941	5.90362	-5.5802
22	180	-0.20	-0.005	1263.8	1.563	0.90559	6.18259	-3.8505	1264.2	1.560	0.92936	6.17850	-3.8251	1265.0	1.562	0.92936	6.17850	-3.8251
23	180	-0.50	-0.085	1270.7	1.603	0.90040	6.05633	-4.0537	1266.5	1.596	0.92936	6.17850	-3.8251	1265.0	1.562	0.92936	6.17850	-3.8251
24	180	-0.80	-0.169	1277.6	1.643	0.89521	5.92903	-4.2569	1273.0	1.626	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
25	180	-1.00	-0.246	1284.9	1.683	0.89002	5.80000	-4.4601	1278.5	1.668	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
26	180	-1.25	-0.263	1304.5	1.652	0.87599	5.71186	-4.6666	1295.5	1.640	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
27	180	-1.50	-0.295	1312.5	1.664	0.86196	5.62381	-4.8731	1304.5	1.652	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
28	180	-1.75	-0.344	1320.5	1.676	0.84794	5.53576	-5.0796	1313.5	1.664	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
29	180	-2.00	-0.394	1328.5	1.688	0.83392	5.44771	-5.2861	1322.5	1.676	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
30	180	-2.25	-0.434	1336.5	1.690	0.81990	5.35966	-5.4926	1331.5	1.688	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
31	180	-2.50	-0.476	1344.5	1.692	0.80588	5.27161	-5.6991	1340.5	1.690	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
32	180	-2.75	-0.519	1352.5	1.694	0.79186	5.18356	-5.9056	1349.5	1.692	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
33	180	-3.00	-0.562	1360.5	1.696	0.77784	5.09551	-6.1121	1358.5	1.694	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
34	180	-3.25	-0.604	1368.5	1.698	0.76382	5.00746	-6.3186	1367.5	1.696	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
35	180	-3.50	-0.647	1376.5	1.700	0.74980	4.91941	-6.5251	1376.5	1.698	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
36	180	-3.75	-0.689	1384.5	1.702	0.73578	4.83136	-6.7316	1385.5	1.698	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
37	180	-4.00	-0.732	1392.5	1.704	0.72176	4.74331	-6.9381	1394.5	1.700	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
38	180	-4.25	-0.775	1400.5	1.706	0.70774	4.65526	-7.1446	1403.5	1.702	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
39	180	-4.50	-0.818	1408.5	1.708	0.69372	4.56721	-7.3511	1412.5	1.704	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
40	180	-4.75	-0.861	1416.5	1.710	0.67970	4.47916	-7.5576	1421.5	1.706	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
41	180	-5.00	-0.904	1424.5	1.712	0.66568	4.39111	-7.7641	1430.5	1.708	0.92811	6.02446	-4.2333	1270.9	1.606	0.92811	6.02446	-4.2333
42	270	-0.20	-0.005	1270.7	1.603	0.90040	6.05633	-4.0537	1266.5	1.615	0.90653	6.07890	-4.0537	1263.0	1.590	0.90431	6.07890	-4.0537
43	270	-0.50	-0.085	1277.6	1.643	0.89521	5.92903	-4.2569	1273.0	1.626	0.90281	5.95328	-4.2569	1269.4	1.602	0.90028	5.95328	-4.2569
44	270	-0.80	-0.169	1284.9	1.683	0.89002	5.80000	-4.4601	1278.5	1.668	0.90281	5.95328	-4.2569	1269.4	1.602	0.90028	5.95328	-4.2569
45	270	-1.00	-0.246	1292.1	1.700	0.88583	5.71186	-4.6666	1287.1	1.676	0.90281	5.95328	-4.2569	1269.4	1.602	0.90028	5.95328	-4.2569
46	270	-1.25	-0.263	1300.5	1.702	0.87180	5.62381	-4.8731	1292.1	1.690	0.90281	5.95328	-4.2569	1269.4	1.602	0.90028	5.95328	-4.2569
47	270	-1.50	-0.295	1308.5	1.704	0.85778	5.53576	-5.0796	1297.1	1.702	0.90281	5.95328	-4.2569	1269.4	1.602	0.90028	5.95328	-4.2569
48	270	-1.75	-0.344	1316.5	1.706	0.84376	5.44771	-5.2861	1302.1	1.704	0.90281	5.95328	-4.2569	1269.4	1.602	0.90028	5.95328	-4.2569
49	270	-2.00	-0.394	1324.5	1.708	0.82974	5.35966	-5.4926	1307.1	1.706	0.90281	5.95328	-4.2569	1269.4	1.602	0.90028	5.95328	-4.2569
50	270	-2.25	-0.434	1332.5	1.710	0.81572	5.27161	-5.6991	1312.1	1.708	0.90281	5.95328	-4.2569	1269.4	1.602	0.90028	5.95328	-4.2569

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE V.- DATA^a FOR 160° CONE; $M_{\infty} = 2.30$ - Concluded(e) $\alpha = 20^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\theta = 67.5^\circ$, $p_t = 2293.5$ psf				$\theta = 90.0^\circ$, $p_t = 2293.3$ psf					
				P_t , psf	C_p	$p_t/p_{t,2}$	P_t/ρ_{∞}	M_t	P_t , psf	C_p	$p_t/p_{t,2}$	P_t/ρ_{∞}	M_t
1	0	.200	.0000	1208.4	1.509	.90329	6.59839	.38397	1208.3	1.509	.90331	6.59851	.38393
2	0	.220	.0005	1206.8	1.502	.89971	6.56225	.39151	1211.5	1.514	.90570	6.60594	.37884
3	0	.240	.0015	1205.2	1.500	.89852	6.52798	.39801	1215.9	1.520	.90948	6.64080	.36850
4	0	.260	.0025	1203.6	1.497	.89733	6.50176	.40612	1221.1	1.528	.91287	6.66949	.36059
5	0	.280	.0035	1198.4	1.495	.89614	6.46742	.41354	1221.1	1.528	.91287	6.66949	.36059
6	0	.300	.0045	1194.8	1.493	.89495	6.43312	.42096	1219.5	1.526	.91167	6.64951	.36588
7	0	.320	.0055	1191.2	1.491	.89376	6.40114	.42838	1217.9	1.524	.91048	6.63208	.37110
8	0	.340	.0065	1187.6	1.489	.89257	6.36742	.43580	1216.3	1.522	.90929	6.61465	.37632
9	0	.360	.0075	1184.0	1.487	.89138	6.33312	.44322	1214.7	1.520	.90810	6.59719	.38154
10	0	.380	.0085	1180.4	1.485	.89019	6.29887	.45064	1213.1	1.518	.90691	6.57979	.38676
11	0	.400	.0095	1176.8	1.483	.88900	6.26462	.45806	1211.5	1.516	.90572	6.56239	.39198
12	0	.420	.0105	1173.2	1.481	.88781	6.23037	.46548	1209.9	1.514	.90453	6.54500	.39720
13	0	.440	.0115	1169.6	1.479	.88662	6.19612	.47290	1208.3	1.512	.90334	6.52761	.40242
14	0	.460	.0125	1166.0	1.477	.88543	6.16187	.48032	1206.7	1.510	.90215	6.51022	.40764
15	0	.480	.0135	1162.4	1.475	.88424	6.12762	.48774	1205.1	1.508	.90096	6.49283	.41286
16	0	.500	.0145	1158.8	1.473	.88305	6.09337	.49516	1203.5	1.506	.90000	6.47544	.41808
17	0	.520	.0155	1155.2	1.471	.88186	6.05912	.50258	1201.9	1.504	.89901	6.45805	.42330
18	0	.540	.0165	1151.6	1.469	.88067	6.02487	.51000	1200.3	1.502	.89802	6.44066	.42852
19	0	.560	.0175	1148.0	1.467	.87948	6.00062	.51742	1198.7	1.500	.89703	6.42327	.43374
20	0	.580	.0185	1144.4	1.465	.87829	5.96637	.52484	1197.1	1.498	.89604	6.40588	.43896
21	0	.600	.0195	1140.8	1.463	.87710	5.93212	.53226	1195.5	1.496	.89505	6.38849	.44418
22	0	.620	.0205	1137.2	1.461	.87591	5.89787	.53968	1193.9	1.494	.89406	6.37110	.44940
23	0	.640	.0215	1133.6	1.459	.87472	5.86362	.54710	1192.3	1.492	.89307	6.35371	.45462
24	0	.660	.0225	1130.0	1.457	.87353	5.82937	.55452	1190.7	1.490	.89208	6.33632	.45984
25	0	.680	.0235	1126.4	1.455	.87234	5.79512	.56194	1189.1	1.488	.89109	6.31893	.46506
26	0	.700	.0245	1122.8	1.453	.87115	5.76087	.56936	1187.5	1.486	.89010	6.30154	.47028
27	0	.720	.0255	1119.2	1.451	.87000	5.72662	.57678	1185.9	1.484	.88911	6.28415	.47550
28	0	.740	.0265	1115.6	1.449	.86881	5.69237	.58420	1184.3	1.482	.88812	6.26676	.48072
29	0	.760	.0275	1112.0	1.447	.86762	5.65812	.59162	1182.7	1.480	.88713	6.24937	.48594
30	0	.780	.0285	1108.4	1.445	.86643	5.62387	.59904	1181.1	1.478	.88614	6.23198	.49116
31	0	.800	.0295	1104.8	1.443	.86524	5.58962	.60646	1179.5	1.476	.88515	6.21459	.49638
32	0	.820	.0305	1101.2	1.441	.86405	5.55537	.61388	1177.9	1.474	.88416	6.19720	.50160
33	0	.840	.0315	1097.6	1.439	.86286	5.52112	.62130	1176.3	1.472	.88317	6.17981	.50682
34	0	.860	.0325	1094.0	1.437	.86167	5.48687	.62872	1174.7	1.470	.88218	6.16242	.51204
35	0	.880	.0335	1090.4	1.435	.86048	5.45262	.63614	1173.1	1.468	.88119	6.14503	.51726
36	0	.900	.0345	1086.8	1.433	.85929	5.41837	.64356	1171.5	1.466	.88020	6.12764	.52248
37	0	.920	.0355	1083.2	1.431	.85810	5.38412	.65098	1169.9	1.464	.87921	6.11025	.52770
38	0	.940	.0365	1079.6	1.429	.85691	5.34987	.65840	1168.3	1.462	.87822	6.09286	.53292
39	0	.960	.0375	1076.0	1.427	.85572	5.31562	.66582	1166.7	1.460	.87723	6.07547	.53814
40	0	.980	.0385	1072.4	1.425	.85453	5.28137	.67324	1165.1	1.458	.87624	6.05808	.54336
41	0	1.000	.0395	1068.8	1.423	.85334	5.24712	.68066	1163.5	1.456	.87525	6.04069	.54858
42	0	1.020	.0405	1065.2	1.421	.85215	5.21287	.68808	1161.9	1.454	.87426	6.02330	.55380
43	0	1.040	.0415	1061.6	1.419	.85096	5.17862	.69550	1160.3	1.452	.87327	6.00591	.55902
44	0	1.060	.0425	1058.0	1.417	.84977	5.14437	.70292	1158.7	1.450	.87228	5.98852	.56424
45	0	1.080	.0435	1054.4	1.415	.84858	5.11012	.71034	1157.1	1.448	.87129	5.97113	.56946
46	0	1.100	.0445	1050.8	1.413	.84739	5.07587	.71776	1155.5	1.446	.87030	5.95374	.57468
47	0	1.120	.0455	1047.2	1.411	.84620	5.04162	.72518	1153.9	1.444	.86931	5.93635	.57990
48	0	1.140	.0465	1043.6	1.409	.84501	5.00737	.73260	1152.3	1.442	.86832	5.91896	.58512
49	0	1.160	.0475	1040.0	1.407	.84382	4.97312	.74002	1150.7	1.440	.86733	5.90157	.59034
50	0	1.180	.0485	1036.4	1.405	.84263	4.93887	.74744	1149.1	1.438	.86634	5.88418	.59556

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VI. - DATA^a FOR 160° CONE; $M_\infty = 2.96$ (a) $\alpha = 0^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\phi = 0.0^\circ, p_t = 3241.9 \text{ psf}$				
				p_t , psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,\infty}$	M_t
1	0	0.000	0.000	1088.4	1.730	0.9800	11.6122	13144
2	0	-0.025	-0.043	1088.4	1.720	0.9800	11.6122	13144
3	0	-0.050	-0.085	1088.4	1.710	0.9800	11.6122	13144
4	0	-0.075	-0.127	1088.4	1.700	0.9800	11.6122	13144
5	0	-0.100	-0.168	1088.4	1.690	0.9800	11.6122	13144
6	0	-0.125	-0.209	1088.4	1.680	0.9800	11.6122	13144
7	0	-0.150	-0.250	1088.4	1.670	0.9800	11.6122	13144
8	0	-0.175	-0.291	1088.4	1.660	0.9800	11.6122	13144
9	0	-0.200	-0.332	1088.4	1.650	0.9800	11.6122	13144
10	0	-0.225	-0.373	1088.4	1.640	0.9800	11.6122	13144
11	0	-0.250	-0.414	1088.4	1.630	0.9800	11.6122	13144
12	0	-0.275	-0.455	1088.4	1.620	0.9800	11.6122	13144
13	0	-0.300	-0.496	1088.4	1.610	0.9800	11.6122	13144
14	0	-0.325	-0.537	1088.4	1.600	0.9800	11.6122	13144
15	0	-0.350	-0.578	1088.4	1.590	0.9800	11.6122	13144
16	0	-0.375	-0.619	1088.4	1.580	0.9800	11.6122	13144
17	0	-0.400	-0.660	1088.4	1.570	0.9800	11.6122	13144
18	0	-0.425	-0.701	1088.4	1.560	0.9800	11.6122	13144
19	0	-0.450	-0.742	1088.4	1.550	0.9800	11.6122	13144
20	0	-0.475	-0.783	1088.4	1.540	0.9800	11.6122	13144
21	0	-0.500	-0.824	1088.4	1.530	0.9800	11.6122	13144
22	0	-0.525	-0.865	1088.4	1.520	0.9800	11.6122	13144
23	0	-0.550	-0.906	1088.4	1.510	0.9800	11.6122	13144
24	0	-0.575	-0.947	1088.4	1.500	0.9800	11.6122	13144
25	0	-0.600	-0.988	1088.4	1.490	0.9800	11.6122	13144
26	0	-0.625	-1.029	1088.4	1.480	0.9800	11.6122	13144
27	0	-0.650	-1.070	1088.4	1.470	0.9800	11.6122	13144
28	0	-0.675	-1.111	1088.4	1.460	0.9800	11.6122	13144
29	0	-0.700	-1.152	1088.4	1.450	0.9800	11.6122	13144
30	0	-0.725	-1.193	1088.4	1.440	0.9800	11.6122	13144
31	0	-0.750	-1.234	1088.4	1.430	0.9800	11.6122	13144
32	0	-0.775	-1.275	1088.4	1.420	0.9800	11.6122	13144
33	0	-0.800	-1.316	1088.4	1.410	0.9800	11.6122	13144
34	0	-0.825	-1.357	1088.4	1.400	0.9800	11.6122	13144
35	0	-0.850	-1.398	1088.4	1.390	0.9800	11.6122	13144
36	0	-0.875	-1.439	1088.4	1.380	0.9800	11.6122	13144
37	0	-0.900	-1.480	1088.4	1.370	0.9800	11.6122	13144
38	0	-0.925	-1.521	1088.4	1.360	0.9800	11.6122	13144
39	0	-0.950	-1.562	1088.4	1.350	0.9800	11.6122	13144
40	0	-0.975	-1.603	1088.4	1.340	0.9800	11.6122	13144
41	0	-1.000	-1.644	1088.4	1.330	0.9800	11.6122	13144
42	0	-1.025	-1.685	1088.4	1.320	0.9800	11.6122	13144
43	0	-1.050	-1.726	1088.4	1.310	0.9800	11.6122	13144
44	0	-1.075	-1.767	1088.4	1.300	0.9800	11.6122	13144
45	0	-1.100	-1.808	1088.4	1.290	0.9800	11.6122	13144
46	0	-1.125	-1.849	1088.4	1.280	0.9800	11.6122	13144
47	0	-1.150	-1.890	1088.4	1.270	0.9800	11.6122	13144
48	0	-1.175	-1.931	1088.4	1.260	0.9800	11.6122	13144
49	0	-1.200	-1.972	1088.4	1.250	0.9800	11.6122	13144
50	0	-1.225	-2.013	1088.4	1.240	0.9800	11.6122	13144
51	0	-1.250	-2.054	1088.4	1.230	0.9800	11.6122	13144
52	0	-1.275	-2.095	1088.4	1.220	0.9800	11.6122	13144
53	0	-1.300	-2.136	1088.4	1.210	0.9800	11.6122	13144
54	0	-1.325	-2.177	1088.4	1.200	0.9800	11.6122	13144
55	0	-1.350	-2.218	1088.4	1.190	0.9800	11.6122	13144
56	0	-1.375	-2.259	1088.4	1.180	0.9800	11.6122	13144
57	0	-1.400	-2.300	1088.4	1.170	0.9800	11.6122	13144
58	0	-1.425	-2.341	1088.4	1.160	0.9800	11.6122	13144
59	0	-1.450	-2.382	1088.4	1.150	0.9800	11.6122	13144
60	0	-1.475	-2.423	1088.4	1.140	0.9800	11.6122	13144
61	0	-1.500	-2.464	1088.4	1.130	0.9800	11.6122	13144
62	0	-1.525	-2.505	1088.4	1.120	0.9800	11.6122	13144
63	0	-1.550	-2.546	1088.4	1.110	0.9800	11.6122	13144
64	0	-1.575	-2.587	1088.4	1.100	0.9800	11.6122	13144
65	0	-1.600	-2.628	1088.4	1.090	0.9800	11.6122	13144
66	0	-1.625	-2.669	1088.4	1.080	0.9800	11.6122	13144
67	0	-1.650	-2.710	1088.4	1.070	0.9800	11.6122	13144
68	0	-1.675	-2.751	1088.4	1.060	0.9800	11.6122	13144
69	0	-1.700	-2.792	1088.4	1.050	0.9800	11.6122	13144
70	0	-1.725	-2.833	1088.4	1.040	0.9800	11.6122	13144
71	0	-1.750	-2.874	1088.4	1.030	0.9800	11.6122	13144
72	0	-1.775	-2.915	1088.4	1.020	0.9800	11.6122	13144
73	0	-1.800	-2.956	1088.4	1.010	0.9800	11.6122	13144
74	0	-1.825	-2.997	1088.4	1.000	0.9800	11.6122	13144
75	0	-1.850	-3.038	1088.4	0.990	0.9800	11.6122	13144
76	0	-1.875	-3.079	1088.4	0.980	0.9800	11.6122	13144
77	0	-1.900	-3.120	1088.4	0.970	0.9800	11.6122	13144
78	0	-1.925	-3.161	1088.4	0.960	0.9800	11.6122	13144
79	0	-1.950	-3.202	1088.4	0.950	0.9800	11.6122	13144
80	0	-1.975	-3.243	1088.4	0.940	0.9800	11.6122	13144
81	0	-2.000	-3.284	1088.4	0.930	0.9800	11.6122	13144
82	0	-2.025	-3.325	1088.4	0.920	0.9800	11.6122	13144
83	0	-2.050	-3.366	1088.4	0.910	0.9800	11.6122	13144
84	0	-2.075	-3.407	1088.4	0.900	0.9800	11.6122	13144
85	0	-2.100	-3.448	1088.4	0.890	0.9800	11.6122	13144
86	0	-2.125	-3.489	1088.4	0.880	0.9800	11.6122	13144
87	0	-2.150	-3.530	1088.4	0.870	0.9800	11.6122	13144
88	0	-2.175	-3.571	1088.4	0.860	0.9800	11.6122	13144
89	0	-2.200	-3.612	1088.4	0.850	0.9800	11.6122	13144
90	0	-2.225	-3.653	1088.4	0.840	0.9800	11.6122	13144
91	0	-2.250	-3.694	1088.4	0.830	0.9800	11.6122	13144
92	0	-2.275	-3.735	1088.4	0.820	0.9800	11.6122	13144
93	0	-2.300	-3.776	1088.4	0.810	0.9800	11.6122	13144
94	0	-2.325	-3.817	1088.4	0.800	0.9800	11.6122	13144
95	0	-2.350	-3.858	1088.4	0.790	0.9800	11.6122	13144
96	0	-2.375	-3.899	1088.4	0.780	0.9800	11.6122	13144
97	0	-2.400	-3.940	1088.4	0.770	0.9800	11.6122	13144
98	0	-2.425	-3.981	1088.4	0.760	0.9800	11.6122	13144
99	0	-2.450	-4.022	1088.4	0.750	0.9800	11.6122	13144
100	0	-2.475	-4.063	1088.4	0.740	0.9800	11.6122	13144
101	0	-2.500	-4.104	1088.4	0.730	0.9800	11.6122	13144
102	0	-2.525	-4.145	1088.4	0.720	0.9800	11.6122	13144
103	0	-2.550	-4.186	1088.4	0.710	0.9800	11.6122	13144
104	0	-2.575	-4.227	1088.4	0.700	0.9800	11.6122	13144
105	0	-2.600	-4.268	1088.4	0.690	0.9800	11.6122	13144
106	0	-2.625	-4.309	1088.4	0.680	0.9800	11.6122	13144
107	0	-2.650	-4.350	1088.4	0.670	0.9800	11.6122	13144
108	0	-2.675	-4.391	1088.4	0.660	0.9800	11.6122	13144
109	0	-2.700	-4.432	1088.4	0.650	0.9800	11.6122	13144
110	0	-2.725	-4.473	1088.4	0.640	0.9800	11.6122	13144
111	0	-2.750	-4.514	1088.4	0.630	0.9800	11.6122	13144
112	0	-2.775	-4.555	1088.4	0.620	0.9800	11.6122	13144
113	0	-2.800	-4.596	1088.4	0.610	0.9800	11.6122	13144
114	0	-2.825	-4.637	1088.4	0.600	0.9800	11.6122	13144
115	0	-2.850	-4.678	1088.4	0.590	0.9800	11.6122	13144
116	0	-2.875	-4.719	1088.4	0.580	0.9800	11.6122	13144
117	0	-2.900	-4.760	1088.4	0.570	0.9800	11.6122	13144
118	0	-2.925	-4.801	1088.4	0.560	0.9800	11.6122	13144
119	0	-2.950	-4.842	1088.4	0.550	0.9800	11.6122	13144
120	0	-2.975	-4.883	1088.4	0.540	0.9800	11.6122	13144
121	0	-3.000	-4.924	1088.4	0.530	0.9800	11.6122	13144
122	0	-3.025	-4.965	1088.4	0.520	0.9800	11.6122	13144
123	0	-3.050	-5.006	1088.4	0.510	0.9800	11.6122	13144
124	0	-3.075	-5.047	1088.4	0.500	0.9800	11.6122	13144
125	0	-3.100	-5.088	1088.4	0.490	0.9800	11.6122	13144
126	0	-3.125	-5.129	1088.4	0.480	0.9800	11.6122	13144
127	0	-3.150	-5.170	1088.4	0.470	0.9800	11.6122	13144
128	0	-3.175	-5.211	1088.4	0.460	0.9800	11.6122	13144
129	0	-3.200	-5.252	1088.4	0.450	0.9800	11.6122	13144
130	0	-3.225	-5.293	1088.4	0.440			

TABLE VI.- DATA^a FOR 160° CONE; $M_{\infty} = 2.96$ - Continued(b) $\alpha = 5^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, P_t = 3239.0 \text{ psf}$	$\phi = 22.5^\circ, P_t = 3241.0 \text{ psf}$	$\phi = 45.0^\circ, P_t = 3240.7 \text{ psf}$									
				P_t/psf	C_p	$P_t/P_{t,2}$	M_t	P_t/psf	C_p	$P_t/P_{t,2}$	M_t	P_t/psf	C_p	$P_t/P_{t,2}$	M_t
1	0	-0.00	-0.000	1079.4	1.716	-98073	11.52704	1079.1	1.715	-97985	11.51672	1081.3	1.719	-98196	11.54150
2	0	-0.00	-0.000	1079.6	1.708	-97537	11.47581	1079.5	1.709	-97695	11.46826	1081.3	1.713	-97906	11.50740
3	0	-0.00	-0.000	1081.2	1.697	-97146	11.44165	1081.2	1.704	-97404	11.43498	1081.9	1.703	-97355	11.49221
4	0	-0.00	-0.000	1083.4	1.689	-96620	11.41367	1083.4	1.695	-96869	11.40610	1085.5	1.708	-97161	11.47431
5	0	-0.00	-0.000	1085.4	1.677	-96039	11.37976	1085.4	1.687	-96333	11.37299	1088.5	1.708	-97161	11.47431
6	0	-0.00	-0.000	1087.2	1.669	-95603	11.35673	1087.2	1.679	-95917	11.35667	1092.2	1.708	-97161	11.47431
7	0	-0.00	-0.000	1089.4	1.667	-95422	11.34842	1089.4	1.681	-95917	11.34842	1095.1	1.708	-97161	11.47431
8	0	-0.00	-0.000	1091.4	1.663	-95314	11.34126	1091.4	1.681	-95917	11.34126	1098.6	1.708	-97161	11.47431
9	0	-0.00	-0.000	1093.4	1.659	-95242	11.33596	1093.4	1.681	-95917	11.33596	1101.6	1.708	-97161	11.47431
10	0	-0.00	-0.000	1095.4	1.657	-95170	11.33126	1095.4	1.681	-95917	11.33126	1104.6	1.708	-97161	11.47431
11	0	-0.00	-0.000	1097.4	1.655	-95100	11.32704	1097.4	1.681	-95917	11.32704	1107.6	1.708	-97161	11.47431
12	0	-0.00	-0.000	1099.4	1.653	-95030	11.32326	1099.4	1.681	-95917	11.32326	1110.6	1.708	-97161	11.47431
13	0	-0.00	-0.000	1101.4	1.651	-94960	11.31946	1101.4	1.681	-95917	11.31946	1113.6	1.708	-97161	11.47431
14	0	-0.00	-0.000	1103.4	1.649	-94890	11.31566	1103.4	1.681	-95917	11.31566	1116.6	1.708	-97161	11.47431
15	0	-0.00	-0.000	1105.4	1.647	-94820	11.31186	1105.4	1.681	-95917	11.31186	1119.6	1.708	-97161	11.47431
16	0	-0.00	-0.000	1107.4	1.645	-94750	11.30806	1107.4	1.681	-95917	11.30806	1122.6	1.708	-97161	11.47431
17	0	-0.00	-0.000	1109.4	1.643	-94680	11.30426	1109.4	1.681	-95917	11.30426	1125.6	1.708	-97161	11.47431
18	0	-0.00	-0.000	1111.4	1.641	-94610	11.30046	1111.4	1.681	-95917	11.30046	1128.6	1.708	-97161	11.47431
19	0	-0.00	-0.000	1113.4	1.639	-94540	11.29666	1113.4	1.681	-95917	11.29666	1131.6	1.708	-97161	11.47431
20	0	-0.00	-0.000	1115.4	1.637	-94470	11.29286	1115.4	1.681	-95917	11.29286	1134.6	1.708	-97161	11.47431
21	0	-0.00	-0.000	1117.4	1.635	-94400	11.28906	1117.4	1.681	-95917	11.28906	1137.6	1.708	-97161	11.47431
22	0	-0.00	-0.000	1119.4	1.633	-94330	11.28526	1119.4	1.681	-95917	11.28526	1140.6	1.708	-97161	11.47431
23	0	-0.00	-0.000	1121.4	1.631	-94260	11.28146	1121.4	1.681	-95917	11.28146	1143.6	1.708	-97161	11.47431
24	0	-0.00	-0.000	1123.4	1.629	-94190	11.27766	1123.4	1.681	-95917	11.27766	1146.6	1.708	-97161	11.47431
25	0	-0.00	-0.000	1125.4	1.627	-94120	11.27386	1125.4	1.681	-95917	11.27386	1149.6	1.708	-97161	11.47431
26	0	-0.00	-0.000	1127.4	1.625	-94050	11.27006	1127.4	1.681	-95917	11.27006	1152.6	1.708	-97161	11.47431
27	0	-0.00	-0.000	1129.4	1.623	-93980	11.26626	1129.4	1.681	-95917	11.26626	1155.6	1.708	-97161	11.47431
28	0	-0.00	-0.000	1131.4	1.621	-93910	11.26246	1131.4	1.681	-95917	11.26246	1158.6	1.708	-97161	11.47431
29	0	-0.00	-0.000	1133.4	1.619	-93840	11.25866	1133.4	1.681	-95917	11.25866	1161.6	1.708	-97161	11.47431
30	0	-0.00	-0.000	1135.4	1.617	-93770	11.25486	1135.4	1.681	-95917	11.25486	1164.6	1.708	-97161	11.47431
31	0	-0.00	-0.000	1137.4	1.615	-93700	11.25106	1137.4	1.681	-95917	11.25106	1167.6	1.708	-97161	11.47431
32	0	-0.00	-0.000	1139.4	1.613	-93630	11.24726	1139.4	1.681	-95917	11.24726	1170.6	1.708	-97161	11.47431
33	0	-0.00	-0.000	1141.4	1.611	-93560	11.24346	1141.4	1.681	-95917	11.24346	1173.6	1.708	-97161	11.47431
34	0	-0.00	-0.000	1143.4	1.609	-93490	11.23966	1143.4	1.681	-95917	11.23966	1176.6	1.708	-97161	11.47431
35	0	-0.00	-0.000	1145.4	1.607	-93420	11.23586	1145.4	1.681	-95917	11.23586	1179.6	1.708	-97161	11.47431
36	0	-0.00	-0.000	1147.4	1.605	-93350	11.23206	1147.4	1.681	-95917	11.23206	1182.6	1.708	-97161	11.47431
37	0	-0.00	-0.000	1149.4	1.603	-93280	11.22826	1149.4	1.681	-95917	11.22826	1185.6	1.708	-97161	11.47431
38	0	-0.00	-0.000	1151.4	1.601	-93210	11.22446	1151.4	1.681	-95917	11.22446	1188.6	1.708	-97161	11.47431
39	0	-0.00	-0.000	1153.4	1.599	-93140	11.22066	1153.4	1.681	-95917	11.22066	1191.6	1.708	-97161	11.47431
40	0	-0.00	-0.000	1155.4	1.597	-93070	11.21686	1155.4	1.681	-95917	11.21686	1194.6	1.708	-97161	11.47431
41	0	-0.00	-0.000	1157.4	1.595	-92930	11.21306	1157.4	1.681	-95917	11.21306	1197.6	1.708	-97161	11.47431
42	0	-0.00	-0.000	1159.4	1.593	-92860	11.20926	1159.4	1.681	-95917	11.20926	1200.6	1.708	-97161	11.47431
43	0	-0.00	-0.000	1161.4	1.591	-92790	11.20546	1161.4	1.681	-95917	11.20546	1203.6	1.708	-97161	11.47431
44	0	-0.00	-0.000	1163.4	1.589	-92720	11.20166	1163.4	1.681	-95917	11.20166	1206.6	1.708	-97161	11.47431
45	0	-0.00	-0.000	1165.4	1.587	-92650	11.19786	1165.4	1.681	-95917	11.19786	1209.6	1.708	-97161	11.47431
46	0	-0.00	-0.000	1167.4	1.585	-92580	11.19406	1167.4	1.681	-95917	11.19406	1212.6	1.708	-97161	11.47431
47	0	-0.00	-0.000	1169.4	1.583	-92510	11.19026	1169.4	1.681	-95917	11.19026	1215.6	1.708	-97161	11.47431
48	0	-0.00	-0.000	1171.4	1.581	-92440	11.18646	1171.4	1.681	-95917	11.18646	1218.6	1.708	-97161	11.47431
49	0	-0.00	-0.000	1173.4	1.579	-92370	11.18266	1173.4	1.681	-95917	11.18266	1221.6	1.708	-97161	11.47431
50	0	-0.00	-0.000	1175.4	1.577	-92300	11.17886	1175.4	1.681	-95917	11.17886	1224.6	1.708	-97161	11.47431

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VI.- DATA^a FOR 160° CONE; $M_\infty = 2.96$ - Continued(b) $\alpha = 5^\circ$ - Concluded

Orifice a, deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ, p_t = 3241.6 \text{ psf}$				$\Phi = 90.0^\circ, p_t = 3239.6 \text{ psf}$			
				p_t , psf	C_p	$p_t/p_{t,2}$	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	M_t
1	0	.300	.0000	1081.2	1.718	.98155	.16333	1080.0	1.717	.98107	.16348
2	0	.400	.0000	1079.6	1.710	.98010	.16971	1080.0	1.717	.98107	.16548
3	0	.500	.0000	1078.4	1.704	.97820	.18182	1078.4	1.714	.97962	.17178
4	0	.600	.0075	1076.4	1.690	.97430	.20402	1075.2	1.703	.97382	.18376
5	0	.800	.1000	1073.2	1.650	.96705	.21930	1072.0	1.683	.96512	.21092
6	0	1.000	.1550	1069.4	1.600	.95835	.23367	1067.2	1.657	.96188	.22576
7	0	1.200	.2000	1065.6	1.540	.94835	.24604	1063.6	1.626	.95498	.23977
8	0	1.400	.2500	1061.2	1.460	.93730	.25644	1059.6	1.592	.94918	.25337
9	0	1.600	.3000	1056.8	1.360	.92505	.26464	1055.2	1.558	.94324	.26717
10	0	1.800	.3500	1052.4	1.250	.91180	.27064	1050.8	1.522	.93730	.28117
11	0	2.000	.4000	1048.0	1.130	.89780	.27464	1046.4	1.486	.93136	.29537
12	0	2.200	.4500	1043.6	1.000	.88330	.27764	1042.0	1.450	.92542	.30977
13	0	2.400	.5000	1039.2	.860	.86830	.27964	1037.6	1.414	.91948	.32437
14	0	2.600	.5500	1034.8	.720	.85330	.28064	1033.2	1.378	.91354	.33917
15	0	2.800	.6000	1030.4	.580	.83830	.28164	1028.8	1.342	.90760	.35417
16	0	3.000	.6500	1026.0	.440	.82330	.28264	1024.4	1.306	.90166	.36937
17	0	3.200	.7000	1021.6	.300	.80830	.28364	1020.0	1.270	.89572	.38477
18	0	3.400	.7500	1017.2	.160	.79330	.28464	1015.6	1.234	.88978	.39997
19	0	3.600	.8000	1012.8	.020	.77830	.28564	1011.2	1.198	.88384	.41537
20	0	3.800	.8500	1008.4	-.120	.76330	.28664	1006.8	1.162	.87790	.43097
21	0	4.000	.9000	1004.0	-.260	.74830	.28764	1002.4	1.126	.87196	.44657
22	180	.000	.0000	1000.0	1.710	.97430	.16971	1000.0	1.710	.97430	.16971
23	180	.000	.0000	996.0	1.704	.97280	.18182	996.0	1.704	.97280	.18182
24	180	.000	.0000	992.0	1.690	.96990	.20402	992.0	1.690	.96990	.20402
25	180	.000	.0000	988.0	1.676	.96700	.21930	988.0	1.676	.96700	.21930
26	180	.000	.0000	984.0	1.660	.96410	.23367	984.0	1.660	.96410	.23367
27	180	.000	.0000	980.0	1.644	.96120	.24604	980.0	1.644	.96120	.24604
28	180	.000	.0000	976.0	1.628	.95830	.25644	976.0	1.628	.95830	.25644
29	180	.000	.0000	972.0	1.612	.95540	.26464	972.0	1.612	.95540	.26464
30	180	.000	.0000	968.0	1.596	.95250	.27064	968.0	1.596	.95250	.27064
31	180	.000	.0000	964.0	1.580	.94960	.27464	964.0	1.580	.94960	.27464
32	180	.000	.0000	960.0	1.564	.94670	.27764	960.0	1.564	.94670	.27764
33	180	.000	.0000	956.0	1.548	.94380	.27964	956.0	1.548	.94380	.27964
34	180	.000	.0000	952.0	1.532	.94090	.28064	952.0	1.532	.94090	.28064
35	180	.000	.0000	948.0	1.516	.93800	.28164	948.0	1.516	.93800	.28164
36	180	.000	.0000	944.0	1.500	.93510	.28264	944.0	1.500	.93510	.28264
37	180	.000	.0000	940.0	1.484	.93220	.28364	940.0	1.484	.93220	.28364
38	180	.000	.0000	936.0	1.468	.92930	.28464	936.0	1.468	.92930	.28464
39	180	.000	.0000	932.0	1.452	.92640	.28564	932.0	1.452	.92640	.28564
40	180	.000	.0000	928.0	1.436	.92350	.28664	928.0	1.436	.92350	.28664
41	180	.000	.0000	924.0	1.420	.92060	.28764	924.0	1.420	.92060	.28764
42	180	.000	.0000	920.0	1.404	.91770	.28864	920.0	1.404	.91770	.28864
43	180	.000	.0000	916.0	1.388	.91480	.28964	916.0	1.388	.91480	.28964
44	180	.000	.0000	912.0	1.372	.91190	.29064	912.0	1.372	.91190	.29064
45	180	.000	.0000	908.0	1.356	.90900	.29164	908.0	1.356	.90900	.29164
46	180	.000	.0000	904.0	1.340	.90610	.29264	904.0	1.340	.90610	.29264
47	180	.000	.0000	900.0	1.324	.90320	.29364	900.0	1.324	.90320	.29364
48	180	.000	.0000	896.0	1.308	.90030	.29464	896.0	1.308	.90030	.29464
49	180	.000	.0000	892.0	1.292	.89740	.29564	892.0	1.292	.89740	.29564

Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VI.- DATA^a FOR 160° CONE; $M_{\infty} = 2.96$ - Continued(c) $\alpha = 10^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ$, $P_t = 3238.7$ psf					$\Phi = 22.5^\circ$, $P_t = 3241.5$ psf					$\Phi = 45.0^\circ$, $P_t = 3242.9$ psf				
				P_{t1} psf	C_p	$P_t/P_{t1,2}$	P_t/P_{t1}	M_{t1}	P_{t1} psf	C_p	$P_t/P_{t1,2}$	P_t/P_{t1}	M_{t1}	P_{t1} psf	C_p	$P_t/P_{t1,2}$	P_t/P_{t1}	M_{t1}
1	0	.000	.0000	1050.4	1.683	.9331	11.32473	.23104	1059.9	1.681	.9328	11.31024	.23501	1060.1	1.681	.93207	11.30771	.23569
2	0	.025	.0093	1050.8	1.667	.93480	11.22225	.25792	1051.9	1.667	.93502	11.22494	.25724	1053.7	1.667	.95626	11.23949	.25157
3	0	.050	.0095	1047.6	1.661	.93480	11.18409	.26534	1047.1	1.659	.93502	11.17376	.26980	1048.9	1.661	.95191	11.18832	.24658
4	0	.075	.0096	1044.4	1.655	.93480	11.14596	.27276	1043.9	1.655	.93502	11.12258	.27617	1045.7	1.655	.94701	11.15421	.24147
5	0	.100	.0097	1041.2	1.649	.93480	11.10783	.28018	1040.9	1.650	.93502	11.08611	.28359	1042.5	1.649	.94212	11.11594	.23636
6	0	.125	.0098	1038.0	1.643	.93480	11.06970	.28760	1038.5	1.628	.93470	10.98611	.29101	1039.6	1.643	.93723	11.07567	.23125
7	0	.150	.0099	1034.8	1.637	.93480	11.03157	.29502	1035.1	1.617	.92890	10.91787	.29842	1036.2	1.637	.93234	11.03540	.22614
8	0	.175	.0100	1031.6	1.631	.93480	11.01344	.30244	1031.2	1.603	.92164	10.83258	.30184	1031.8	1.631	.92724	11.01310	.22103
9	0	.200	.0101	1028.4	1.625	.93480	11.01344	.30986	1027.8	1.597	.91438	10.74778	.31126	1028.4	1.625	.92234	10.99283	.21592
10	0	.225	.0102	1025.2	1.619	.93480	11.01344	.31728	1024.6	1.591	.90712	10.66298	.31368	1025.2	1.619	.91704	10.91310	.21081
11	0	.250	.0103	1022.0	1.613	.93480	11.01344	.32470	1021.0	1.585	.89986	10.57818	.31610	1022.0	1.613	.91214	10.83332	.20570
12	0	.275	.0104	1018.8	1.607	.93480	11.01344	.33212	1017.4	1.579	.89260	10.49338	.31852	1018.8	1.607	.90724	10.75354	.20059
13	0	.300	.0105	1015.6	1.601	.93480	11.01344	.33954	1014.2	1.573	.88534	10.40854	.32094	1015.6	1.601	.90234	10.67376	.19548
14	0	.325	.0106	1012.4	1.595	.93480	11.01344	.34696	1011.0	1.567	.87808	10.32370	.32336	1012.4	1.595	.89744	10.59398	.19037
15	0	.350	.0107	1009.2	1.589	.93480	11.01344	.35438	1007.6	1.561	.87082	10.23886	.32578	1009.2	1.589	.89254	10.51420	.18526
16	0	.375	.0108	1006.0	1.583	.93480	11.01344	.36180	1004.4	1.555	.86356	10.15402	.32820	1006.0	1.583	.88764	10.43442	.18015
17	0	.400	.0109	1002.8	1.577	.93480	11.01344	.36922	1001.2	1.549	.85630	10.06918	.33062	1002.8	1.577	.88274	10.35464	.17504
18	0	.425	.0110	1000.0	1.571	.93480	11.01344	.37664	998.0	1.543	.84904	9.98434	.33304	1000.0	1.571	.87784	10.27486	.16993
19	0	.450	.0111	996.8	1.565	.93480	11.01344	.38406	994.8	1.537	.84178	9.90454	.33546	996.8	1.565	.87294	10.19508	.16482
20	0	.475	.0112	993.6	1.559	.93480	11.01344	.39148	991.6	1.531	.83452	9.82474	.33788	993.6	1.559	.86804	10.11530	.15971
21	0	.500	.0113	990.4	1.553	.93480	11.01344	.39890	988.4	1.525	.82726	9.74494	.34030	990.4	1.553	.86314	10.03552	.15460
22	0	.525	.0114	987.2	1.547	.93480	11.01344	.40632	985.2	1.519	.82000	9.66514	.34272	987.2	1.547	.85824	9.95574	.14949
23	0	.550	.0115	984.0	1.541	.93480	11.01344	.41374	982.0	1.513	.81274	9.58534	.34514	984.0	1.541	.85334	9.87596	.14438
24	0	.575	.0116	980.8	1.535	.93480	11.01344	.42116	978.8	1.507	.80548	9.50554	.34756	980.8	1.535	.84844	9.79618	.13927
25	0	.600	.0117	977.6	1.529	.93480	11.01344	.42858	975.6	1.501	.79822	9.42574	.35000	977.6	1.529	.84354	9.71640	.13416
26	0	.625	.0118	974.4	1.523	.93480	11.01344	.43600	972.4	1.495	.79096	9.34594	.35242	974.4	1.523	.83864	9.63662	.12905
27	0	.650	.0119	971.2	1.517	.93480	11.01344	.44342	969.2	1.489	.78370	9.26614	.35484	971.2	1.517	.83374	9.55684	.12394
28	0	.675	.0120	968.0	1.511	.93480	11.01344	.45084	966.0	1.483	.77644	9.18634	.35726	968.0	1.511	.82884	9.47706	.11883
29	0	.700	.0121	964.8	1.505	.93480	11.01344	.45826	962.8	1.477	.76918	9.10654	.35968	964.8	1.505	.82394	9.39728	.11372
30	0	.725	.0122	961.6	1.500	.93480	11.01344	.46568	959.6	1.471	.76192	9.02674	.36210	961.6	1.500	.81904	9.31750	.10861
31	0	.750	.0123	958.4	1.494	.93480	11.01344	.47310	956.4	1.465	.75466	8.94694	.36452	958.4	1.494	.81414	9.23772	.10350
32	0	.775	.0124	955.2	1.488	.93480	11.01344	.48052	953.2	1.459	.74740	8.86714	.36694	955.2	1.488	.80924	9.15794	.9839
33	0	.800	.0125	952.0	1.482	.93480	11.01344	.48794	950.0	1.453	.74014	8.78734	.36936	952.0	1.482	.80434	9.07816	.9328
34	0	.825	.0126	948.8	1.476	.93480	11.01344	.49536	946.8	1.447	.73288	8.70754	.37178	948.8	1.476	.79944	8.99838	.8817
35	0	.850	.0127	945.6	1.470	.93480	11.01344	.50278	943.6	1.441	.72562	8.62774	.37420	945.6	1.470	.79454	8.91860	.8306
36	0	.875	.0128	942.4	1.464	.93480	11.01344	.51020	940.4	1.435	.71836	8.54794	.37662	942.4	1.464	.78964	8.83882	.7795
37	0	.900	.0129	939.2	1.458	.93480	11.01344	.51762	937.2	1.429	.71110	8.46814	.37904	939.2	1.458	.78474	8.75904	.7284
38	0	.925	.0130	936.0	1.452	.93480	11.01344	.52504	934.0	1.423	.70384	8.38834	.38146	936.0	1.452	.77984	8.67926	.6773
39	0	.950	.0131	932.8	1.446	.93480	11.01344	.53246	930.8	1.417	.69658	8.30854	.38388	932.8	1.446	.77494	8.59948	.6262
40	0	.975	.0132	929.6	1.440	.93480	11.01344	.53988	927.6	1.411	.68932	8.22874	.38630	929.6	1.440	.77004	8.51970	.5751
41	0	.1000	.0133	926.4	1.434	.93480	11.01344	.54730	924.4	1.405	.68206	8.14894	.38872	926.4	1.434	.76514	8.43992	.5240
42	0	.1025	.0134	923.2	1.428	.93480	11.01344	.55472	921.2	1.400	.67480	8.06914	.39114	923.2	1.428	.76024	8.36014	.4729
43	0	.1050	.0135	920.0	1.422	.93480	11.01344	.56214	918.0	1.394	.66754	7.98934	.39356	920.0	1.422	.75534	8.28036	.4218
44	0	.1075	.0136	916.8	1.416	.93480	11.01344	.56956	914.8	1.388	.66028	7.90954	.39598	916.8	1.416	.75044	8.20058	.3707
45	0	.1100	.0137	913.6	1.410	.93480	11.01344	.57698	911.6	1.382	.65302	7.82974	.39840	913.6	1.410	.74554	8.12080	.3196
46	0	.1125	.0138	910.4	1.404	.93480	11.01344	.58440	908.4	1.376	.64576	7.74994	.40082	910.4	1.404	.74064	8.04102	.2685
47	0	.1150	.0139	907.2	1.398	.93480	11.01344	.59182	905.2	1.370	.63850	7.67014	.40324	907.2	1.398	.73574	7.96124	.2174
48	0	.1175	.0140	904.0	1.392	.93480	11.01344	.59924	902.0	1.364	.63124	7.59034	.40566	904.0	1.392	.73084	7.88146	.1663
49	0	.1200	.0141	900.8	1.386	.93480	11.01344	.60666	898.8	1.358	.62400	7.51054	.40808	900.8	1.386	.72594	7.80168	.1152

Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VI.- DATA^a FOR 160° CONE; $M_{\infty} = 2.96$ - Continued(c) $\alpha = 10^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ$, $P_t = 3242.6$ psf				$\Phi = 90.0^\circ$, $P_t = 3241.7$ psf			
				P_t , psf	C_p	$P_t/P_t, 2$	M_t	P_t , psf	C_p	$P_t/P_t, 2$	M_t
1	0	.200	.0000	1050.4	1.681	.96240	11.31167	1060.4	1.682	.96267	11.31481
2	0	.200	.0025	1055.6	1.673	.95806	11.26056	1063.4	1.682	.96267	11.31481
3	0	.200	.0050	1055.6	1.670	.95601	11.24953	1058.8	1.679	.96122	11.29777
4	0	.200	.0075	1050.8	1.665	.95371	11.17539	1055.6	1.673	.95832	11.26369
5	0	.200	.0100	1042.8	1.661	.94946	11.12428	1052.4	1.668	.95542	11.25961
6	0	.200	.0125	1034.8	1.657	.94666	11.05614	1049.2	1.662	.95252	11.19523
7	0	.200	.0150	1026.8	1.653	.94406	11.08799	1046.0	1.654	.94962	11.19523
8	0	.200	.0175	1018.8	1.650	.94146	11.08799	1042.8	1.650	.94672	11.19523
9	0	.200	.0200	1010.8	1.646	.93886	11.08799	1039.6	1.646	.94382	11.19523
10	0	.200	.0225	1002.8	1.643	.93626	11.08799	1036.4	1.643	.94092	11.19523
11	0	.200	.0250	994.8	1.640	.93366	11.08799	1033.2	1.640	.93802	11.19523
12	0	.200	.0275	986.8	1.637	.93106	11.08799	1030.0	1.637	.93512	11.19523
13	0	.200	.0300	978.8	1.634	.92846	11.08799	1026.8	1.634	.93222	11.19523
14	0	.200	.0325	970.8	1.631	.92586	11.08799	1023.6	1.631	.92932	11.19523
15	0	.200	.0350	962.8	1.628	.92326	11.08799	1020.4	1.628	.92642	11.19523
16	0	.200	.0375	954.8	1.625	.92066	11.08799	1017.2	1.625	.92352	11.19523
17	0	.200	.0400	946.8	1.622	.91806	11.08799	1014.0	1.622	.92062	11.19523
18	0	.200	.0425	938.8	1.619	.91546	11.08799	1010.8	1.619	.91772	11.19523
19	0	.200	.0450	930.8	1.616	.91286	11.08799	1007.6	1.616	.91482	11.19523
20	0	.200	.0475	922.8	1.613	.91026	11.08799	1004.4	1.613	.91192	11.19523
21	0	.200	.0500	914.8	1.610	.90766	11.08799	1001.2	1.610	.90902	11.19523
22	0	.200	.0525	906.8	1.607	.90506	11.08799	998.0	1.607	.90642	11.19523
23	0	.200	.0550	898.8	1.604	.90246	11.08799	994.8	1.604	.90372	11.19523
24	0	.200	.0575	890.8	1.601	.90006	11.08799	991.6	1.601	.90132	11.19523
25	0	.200	.0600	882.8	1.598	.89746	11.08799	988.4	1.598	.89862	11.19523
26	0	.200	.0625	874.8	1.595	.89486	11.08799	985.2	1.595	.89592	11.19523
27	0	.200	.0650	866.8	1.592	.89226	11.08799	982.0	1.592	.89332	11.19523
28	0	.200	.0675	858.8	1.589	.88966	11.08799	978.8	1.589	.89032	11.19523
29	0	.200	.0700	850.8	1.586	.88706	11.08799	975.6	1.586	.88762	11.19523
30	0	.200	.0725	842.8	1.583	.88446	11.08799	972.4	1.583	.88492	11.19523
31	0	.200	.0750	834.8	1.580	.88186	11.08799	969.2	1.580	.88222	11.19523
32	0	.200	.0775	826.8	1.577	.87926	11.08799	966.0	1.577	.87952	11.19523
33	0	.200	.0800	818.8	1.574	.87666	11.08799	962.8	1.574	.87672	11.19523
34	0	.200	.0825	810.8	1.571	.87406	11.08799	959.6	1.571	.87402	11.19523
35	0	.200	.0850	802.8	1.568	.87146	11.08799	956.4	1.568	.87132	11.19523
36	0	.200	.0875	794.8	1.565	.86886	11.08799	953.2	1.565	.86862	11.19523
37	0	.200	.0900	786.8	1.562	.86626	11.08799	950.0	1.562	.86592	11.19523
38	0	.200	.0925	778.8	1.559	.86366	11.08799	946.8	1.559	.86332	11.19523
39	0	.200	.0950	770.8	1.556	.86106	11.08799	943.6	1.556	.86072	11.19523
40	0	.200	.0975	762.8	1.553	.85846	11.08799	940.4	1.553	.85812	11.19523
41	0	.200	.1000	754.8	1.550	.85586	11.08799	937.2	1.550	.85552	11.19523
42	0	.200	.1025	746.8	1.547	.85326	11.08799	934.0	1.547	.85292	11.19523
43	0	.200	.1050	738.8	1.544	.85066	11.08799	930.8	1.544	.85032	11.19523
44	0	.200	.1075	730.8	1.541	.84806	11.08799	927.6	1.541	.84772	11.19523
45	0	.200	.1100	722.8	1.538	.84546	11.08799	924.4	1.538	.84512	11.19523
46	0	.200	.1125	714.8	1.535	.84286	11.08799	921.2	1.535	.84252	11.19523
47	0	.200	.1150	706.8	1.532	.84026	11.08799	918.0	1.532	.84002	11.19523
48	0	.200	.1175	698.8	1.529	.83766	11.08799	914.8	1.529	.83732	11.19523
49	0	.200	.1200	690.8	1.526	.83506	11.08799	911.6	1.526	.83472	11.19523

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VI.- DATA^a FOR 160° CONE; $M_{\infty} = 2.96$ - Continued

(d) $\alpha = 15^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0, 0^\circ, p_t = 3240.5$ psf			
				p_t , psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,\infty}$
1	0	-0.200	-0.000	1024.9	1.621	0.3197	10.43983
2	0	-0.200	-0.025	1015.3	1.624	0.3205	10.43983
3	0	-0.200	-0.050	1005.7	1.598	0.3195	10.43983
4	0	-0.200	-0.075	996.1	1.572	0.3185	10.43983
5	0	-0.200	-0.100	986.5	1.546	0.3175	10.43983
6	0	-0.200	-0.125	976.9	1.520	0.3165	10.43983
7	0	-0.200	-0.150	967.3	1.494	0.3155	10.43983
8	0	-0.200	-0.175	957.7	1.468	0.3145	10.43983
9	0	-0.200	-0.200	948.1	1.442	0.3135	10.43983
10	0	-0.200	-0.225	938.5	1.416	0.3125	10.43983
11	0	-0.200	-0.250	928.9	1.390	0.3115	10.43983
12	0	-0.200	-0.275	919.3	1.364	0.3105	10.43983
13	0	-0.200	-0.300	909.7	1.338	0.3095	10.43983
14	0	-0.200	-0.325	899.9	1.312	0.3085	10.43983
15	0	-0.200	-0.350	890.1	1.286	0.3075	10.43983
16	0	-0.200	-0.375	880.3	1.260	0.3065	10.43983
17	0	-0.200	-0.400	870.5	1.234	0.3055	10.43983
18	0	-0.200	-0.425	860.7	1.208	0.3045	10.43983
19	0	-0.200	-0.450	850.9	1.182	0.3035	10.43983
20	0	-0.200	-0.475	841.1	1.156	0.3025	10.43983
21	0	-0.200	-0.500	831.3	1.130	0.3015	10.43983
22	180	-0.200	-0.025	1051.8	1.667	0.3517	11.22668
23	180	-0.200	-0.050	1041.5	1.690	0.3575	11.22668
24	180	-0.200	-0.075	1031.2	1.714	0.3633	11.22668
25	180	-0.200	-0.100	1020.9	1.738	0.3691	11.22668
26	180	-0.200	-0.125	1010.6	1.762	0.3749	11.22668
27	180	-0.200	-0.150	1000.3	1.786	0.3807	11.22668
28	180	-0.200	-0.175	990.0	1.810	0.3865	11.22668
29	180	-0.200	-0.200	979.7	1.834	0.3923	11.22668
30	180	-0.200	-0.225	969.4	1.858	0.3981	11.22668
31	180	-0.200	-0.250	959.1	1.882	0.4039	11.22668
32	180	-0.200	-0.275	948.8	1.906	0.4097	11.22668
33	180	-0.200	-0.300	938.5	1.930	0.4155	11.22668
34	180	-0.200	-0.325	928.2	1.954	0.4213	11.22668
35	180	-0.200	-0.350	917.9	1.978	0.4271	11.22668
36	180	-0.200	-0.375	907.6	2.002	0.4329	11.22668
37	180	-0.200	-0.400	897.3	2.026	0.4387	11.22668
38	180	-0.200	-0.425	887.0	2.050	0.4445	11.22668
39	180	-0.200	-0.450	876.7	2.074	0.4503	11.22668
40	180	-0.200	-0.475	866.4	2.098	0.4561	11.22668
41	180	-0.200	-0.500	856.1	2.122	0.4619	11.22668
42	270	-0.200	-0.025	1027.9	1.626	0.3346	10.97152
43	270	-0.200	-0.050	1018.1	1.629	0.3354	10.97152
44	270	-0.200	-0.075	1008.3	1.632	0.3362	10.97152
45	270	-0.200	-0.100	998.5	1.635	0.3370	10.97152
46	270	-0.200	-0.125	988.7	1.638	0.3378	10.97152
47	270	-0.200	-0.150	978.9	1.641	0.3386	10.97152
48	270	-0.200	-0.175	969.1	1.644	0.3394	10.97152
49	270	-0.200	-0.200	959.3	1.647	0.3402	10.97152
50	270	-0.200	-0.225	949.5	1.650	0.3410	10.97152

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VI.- DATA^a FOR 160° CONE; $M_{\infty} = 2.96$ - Continued(e) $\alpha = 20^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ$, $p_t = 3242.1$ psf					$\phi = 22.5^\circ$, $p_t = 3241.9$ psf					$\phi = 45.0^\circ$, $p_t = 3242.8$ psf				
				$p_{t, \text{psf}}$	C_p	$p_{t, \text{psf}}$	M_t	$p_{t, \text{psf}}$	C_p	$p_{t, \text{psf}}$	M_t	$p_{t, \text{psf}}$	C_p	$p_{t, \text{psf}}$	$p_{t, \text{psf}}$	$p_{t, \text{psf}}$	$p_{t, \text{psf}}$	M_t
1	0	.000	.0000	972.1	1.528	.88241	10.37150	972.5	1.529	.88282	10.37623	972.7	1.530	.88325	10.37651	.88375	10.37651	42587
2	0	.200	.0025	969.3	1.511	.87371	10.26921	964.5	1.515	.87557	10.29104	961.9	1.515	.87551	10.32440	.87551	10.29033	43398
3	0	.400	.0050	962.5	1.511	.87371	10.26921	964.5	1.515	.87557	10.29104	961.9	1.515	.87551	10.32440	.87551	10.29033	43398
4	0	.600	.0075	956.5	1.511	.86645	10.18386	956.5	1.501	.86832	10.20596	956.5	1.501	.86832	10.20596	.86832	10.20596	44554
5	0	.800	.0100	948.1	1.486	.85054	10.11583	950.2	1.490	.85252	10.13700	948.1	1.487	.85054	10.11583	.85054	10.11583	45737
6	0	1.000	.0125	925.6	1.475	.82558	9.98210	935.8	1.465	.82756	9.98210	935.8	1.465	.82756	9.98210	.82756	9.98210	46920
7	0	1.200	.0150	898.1	1.445	.80117	9.85975	907.8	1.445	.80315	9.85975	907.8	1.445	.80315	9.85975	.80315	9.85975	48103
8	0	1.400	.0175	872.2	1.428	.78307	9.75740	882.9	1.437	.78505	9.75740	882.9	1.437	.78505	9.75740	.78505	9.75740	49286
9	0	1.600	.0200	848.4	1.414	.76776	9.67211	860.6	1.437	.76974	9.67211	860.6	1.437	.76974	9.67211	.76974	9.67211	50469
10	0	1.800	.0225	826.6	1.402	.75382	9.60233	840.6	1.428	.75580	9.60233	840.6	1.428	.75580	9.60233	.75580	9.60233	51652
11	0	2.000	.0250	806.6	1.392	.74111	9.54330	822.9	1.420	.74309	9.54330	822.9	1.420	.74309	9.54330	.74309	9.54330	52835
12	0	2.200	.0275	788.4	1.382	.72943	9.49330	806.6	1.414	.73141	9.49330	806.6	1.414	.73141	9.49330	.73141	9.49330	54018
13	0	2.400	.0300	771.9	1.372	.71876	9.45233	792.5	1.408	.72074	9.45233	792.5	1.408	.72074	9.45233	.72074	9.45233	55201
14	0	2.600	.0325	757.0	1.362	.70905	9.41933	780.3	1.402	.71103	9.41933	780.3	1.402	.71103	9.41933	.71103	9.41933	56384
15	0	2.800	.0350	743.6	1.356	.70029	9.39330	769.2	1.396	.70227	9.39330	769.2	1.396	.70227	9.39330	.70227	9.39330	57567
16	0	3.000	.0375	731.5	1.350	.69249	9.37330	759.2	1.390	.69447	9.37330	759.2	1.390	.69447	9.37330	.69447	9.37330	58750
17	0	3.200	.0400	720.6	1.344	.68564	9.35830	750.2	1.384	.68762	9.35830	750.2	1.384	.68762	9.35830	.68762	9.35830	59933
18	0	3.400	.0425	710.8	1.338	.67974	9.34830	742.2	1.378	.68172	9.34830	742.2	1.378	.68172	9.34830	.68172	9.34830	61116
19	0	3.600	.0450	702.0	1.332	.67479	9.34330	735.2	1.372	.67677	9.34330	735.2	1.372	.67677	9.34330	.67677	9.34330	62300
20	0	3.800	.0475	694.2	1.326	.67079	9.34330	729.2	1.366	.67275	9.34330	729.2	1.366	.67275	9.34330	.67275	9.34330	63483
21	0	4.000	.0500	687.4	1.320	.66774	9.34330	724.2	1.360	.66970	9.34330	724.2	1.360	.66970	9.34330	.66970	9.34330	64666
22	180	.000	.0000	972.1	1.528	.88241	10.37150	972.5	1.529	.88282	10.37623	972.7	1.530	.88325	10.37651	.88375	10.37651	42587
23	180	.200	.0025	969.3	1.511	.87371	10.26921	964.5	1.515	.87557	10.29104	961.9	1.515	.87551	10.32440	.87551	10.29033	43398
24	180	.400	.0050	962.5	1.511	.87371	10.26921	964.5	1.515	.87557	10.29104	961.9	1.515	.87551	10.32440	.87551	10.29033	43398
25	180	.600	.0075	956.5	1.511	.86645	10.18386	956.5	1.501	.86832	10.20596	956.5	1.501	.86832	10.20596	.86832	10.20596	44554
26	180	.800	.0100	948.1	1.486	.85054	10.11583	950.2	1.490	.85252	10.13700	948.1	1.487	.85054	10.11583	.85054	10.11583	45737
27	180	1.000	.0125	925.6	1.475	.82558	9.98210	935.8	1.465	.82756	9.98210	935.8	1.465	.82756	9.98210	.82756	9.98210	46920
28	180	1.200	.0150	898.1	1.445	.80117	9.85975	907.8	1.445	.80315	9.85975	907.8	1.445	.80315	9.85975	.80315	9.85975	48103
29	180	1.400	.0175	872.2	1.428	.78307	9.75740	882.9	1.437	.78505	9.75740	882.9	1.437	.78505	9.75740	.78505	9.75740	49286
30	180	1.600	.0200	848.4	1.414	.76776	9.67211	860.6	1.437	.76974	9.67211	860.6	1.437	.76974	9.67211	.76974	9.67211	50469
31	180	1.800	.0225	826.6	1.402	.75382	9.60233	840.6	1.428	.75580	9.60233	840.6	1.428	.75580	9.60233	.75580	9.60233	51652
32	180	2.000	.0250	806.6	1.392	.74111	9.54330	822.9	1.420	.74309	9.54330	822.9	1.420	.74309	9.54330	.74309	9.54330	52835
33	180	2.200	.0275	788.4	1.382	.72943	9.49330	806.6	1.414	.73141	9.49330	806.6	1.414	.73141	9.49330	.73141	9.49330	54018
34	180	2.400	.0300	771.9	1.372	.71876	9.45233	792.5	1.408	.72074	9.45233	792.5	1.408	.72074	9.45233	.72074	9.45233	55201
35	180	2.600	.0325	757.0	1.362	.70905	9.41933	780.3	1.402	.71103	9.41933	780.3	1.402	.71103	9.41933	.71103	9.41933	56384
36	180	2.800	.0350	743.6	1.356	.70029	9.39330	769.2	1.396	.70227	9.39330	769.2	1.396	.70227	9.39330	.70227	9.39330	57567
37	180	3.000	.0375	731.5	1.350	.69249	9.37330	759.2	1.390	.69447	9.37330	759.2	1.390	.69447	9.37330	.69447	9.37330	58750
38	180	3.200	.0400	720.6	1.344	.68564	9.35830	750.2	1.384	.68762	9.35830	750.2	1.384	.68762	9.35830	.68762	9.35830	59933
39	180	3.400	.0425	710.8	1.338	.67974	9.34830	742.2	1.378	.68172	9.34830	742.2	1.378	.68172	9.34830	.68172	9.34830	61116
40	180	3.600	.0450	702.0	1.332	.67479	9.34330	735.2	1.372	.67677	9.34330	735.2	1.372	.67677	9.34330	.67677	9.34330	62300
41	180	3.800	.0475	694.2	1.326	.67079	9.34330	729.2	1.366	.67275	9.34330	729.2	1.366	.67275	9.34330	.67275	9.34330	63483
42	180	4.000	.0500	687.4	1.320	.66774	9.34330	724.2	1.360	.66970	9.34330	724.2	1.360	.66970	9.34330	.66970	9.34330	64666
43	180	4.200	.0525	681.5	1.314	.66479	9.34330	719.2	1.354	.66677	9.34330	719.2	1.354	.66677	9.34330	.66677	9.34330	65849
44	180	4.400	.0550	676.5	1.308	.66184	9.34330	714.2	1.348	.66382	9.34330	714.2	1.348	.66382	9.34330	.66382	9.34330	67032
45	180	4.600	.0575	672.5	1.302	.65989	9.34330	709.2	1.342	.66187	9.34330	709.2	1.342	.66187	9.34330	.66187	9.34330	68215
46	180	4.800	.0600	669.3	1.296	.65794	9.34330	704.2	1.336	.65992	9.34330	704.2	1.336	.65992	9.34330	.65992	9.34330	69398
47	180	5.000	.0625	666.2	1.290	.65600	9.34330	700.2	1.330	.65799	9.34330	700.2	1.330	.65799	9.34330	.65799	9.34330	70581
48	180	5.200	.0650	663.1	1.284	.65405	9.34330	696.2	1.324	.65604	9.34330	696.2	1.324	.65604	9.34330	.65604	9.34330	71764
49	180	5.400	.0675	660.0	1.278	.65210	9.34330	692.2	1.318	.65409	9.34330	692.2	1.318	.65409	9.34330	.65409	9.34330	72947
50	180	5.600	.0700	656.9	1.272	.65015	9.34330	688.2	1.312	.65214	9.34330	688.2	1.312	.65214	9.34330	.65214	9.34330	74130

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VI.- DATA^a FOR 160° CONE; $M_{\infty} = 2.96$ - Concluded

(e) $\alpha = 20^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\theta = 67.5^\circ, p_t = 3242.8 \text{ psf}$					$\theta = 90.0^\circ, p_t = 3240.7 \text{ psf}$				
				p_t/psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}	M_t	p_t/psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}	M_t
1	0	.000	.0000	974.8	1.532	.88461	10.39732	-4.2221	973.7	1.531	.88419	10.39233	-4.2305
2	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
3	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
4	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
5	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
6	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
7	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
8	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
9	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
10	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
11	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
12	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
13	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
14	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
15	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
16	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
17	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
18	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
19	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
20	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
21	0	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
22	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
23	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
24	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
25	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
26	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
27	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
28	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
29	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
30	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
31	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
32	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
33	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
34	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
35	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
36	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
37	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
38	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
39	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
40	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
41	180	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
42	270	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
43	270	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
44	270	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
45	270	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
46	270	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
47	90	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
48	90	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728
49	90	.000	.0000	973.2	1.529	.88316	10.38031	-4.2507	972.9	1.527	.88270	10.42646	-4.1728

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VII.- DATA^a FOR 160° CONE; $M_{\infty} = 3.95$ (a) $\alpha = 0^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ, P_t = 5753.1 \text{ psf}$				M_t
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t\infty}$	
1	0	.000	.0000	815.0	1.753	.97953	20.14241	.17214
2	0	.020	.0493	816.4	1.749	.97761	20.10291	.17015
3	0	.040	.0956	817.8	1.745	.97569	20.06342	.16816
4	0	.060	.1388	819.2	1.741	.97377	20.02392	.16617
5	0	.080	.1791	820.6	1.737	.97185	19.98443	.16418
6	0	.100	.2163	822.0	1.733	.96993	19.94494	.16219
7	0	.120	.2506	823.4	1.729	.96801	19.90545	.16020
8	0	.140	.2819	824.8	1.725	.96609	19.86596	.15821
9	0	.160	.3102	826.2	1.721	.96417	19.82647	.15622
10	0	.180	.3354	827.6	1.717	.96225	19.78698	.15423
11	0	.200	.3586	829.0	1.713	.96033	19.74749	.15224
12	0	.220	.3798	830.4	1.709	.95841	19.70800	.15025
13	0	.240	.3990	831.8	1.705	.95649	19.66851	.14826
14	0	.260	.4162	833.2	1.701	.95457	19.62902	.14627
15	0	.280	.4314	834.6	1.697	.95265	19.58953	.14428
16	0	.300	.4446	836.0	1.693	.95073	19.55004	.14229
17	0	.320	.4558	837.4	1.689	.94881	19.51055	.14030
18	0	.340	.4650	838.8	1.685	.94689	19.47106	.13831
19	0	.360	.4722	840.2	1.681	.94497	19.43157	.13632
20	0	.380	.4774	841.6	1.677	.94305	19.39208	.13433
21	0	.400	.4806	843.0	1.673	.94113	19.35259	.13234
22	0	.420	.4818	844.4	1.669	.93921	19.31310	.13035
23	0	.440	.4810	845.8	1.665	.93729	19.27361	.12836
24	0	.460	.4782	847.2	1.661	.93537	19.23412	.12637
25	0	.480	.4734	848.6	1.657	.93345	19.19463	.12438
26	0	.500	.4666	850.0	1.653	.93153	19.15514	.12239
27	180	1.000	.125	815.1	1.751	.97844	20.12003	.17672
28	180	1.200	.190	811.9	1.743	.97461	20.04113	.17205
29	180	1.400	.246	808.7	1.736	.97078	19.96223	.16738
30	180	1.600	.294	805.5	1.728	.96695	19.88332	.16271
31	180	1.800	.334	802.3	1.721	.96312	19.80441	.15804
32	180	2.000	.366	799.1	1.714	.95929	19.72550	.15337
33	180	2.200	.391	795.9	1.707	.95546	19.64659	.14870
34	180	2.400	.408	792.7	1.700	.95163	19.56768	.14403
35	180	2.600	.419	789.5	1.693	.94780	19.48877	.13936
36	180	2.800	.425	786.3	1.686	.94397	19.40986	.13469
37	180	3.000	.427	783.1	1.679	.94014	19.33095	.13002
38	180	3.200	.424	779.9	1.672	.93631	19.25204	.12535
39	180	3.400	.418	776.7	1.665	.93248	19.17313	.12068
40	180	3.600	.410	773.5	1.658	.92865	19.09422	.11601
41	180	3.800	.400	770.3	1.651	.92482	19.01531	.11134
42	180	4.000	.388	767.1	1.644	.92099	18.93640	.10667
43	180	4.200	.374	763.9	1.637	.91716	18.85749	.10200
44	180	4.400	.358	760.7	1.630	.91333	18.77858	.09733
45	180	4.600	.341	757.5	1.623	.90950	18.69967	.09266
46	180	4.800	.323	754.3	1.616	.90567	18.62076	.08800
47	180	5.000	.305	751.1	1.609	.90184	18.54185	.08333
48	180	5.200	.286	747.9	1.602	.89801	18.46294	.07866
49	180	5.400	.267	744.7	1.595	.89418	18.38403	.07400
50	180	5.600	.247	741.5	1.588	.89035	18.30512	.06933

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VII.- DATA^a FOR 160° CONE; $M_{\infty} = 3.95$ - Continued

(b) $\alpha = 5^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, p_t = 5762.6$ psf						$\phi = 22.5^\circ, p_t = 5762.6$ psf						$\phi = 45.0^\circ, p_t = 5762.6$ psf							
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,0}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,0}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,0}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,0}$	M_t
1	0	.330	.0000	817.3	1.753	.97939	20.14466	1.753	817.4	1.753	.97963	20.14466	1.7171	815.6	1.749	.97744	20.09945	1.7171	815.6	1.749	.97744	20.09945	1.8084
2	0	.430	.0025	.0985	1.742	.97374	19.98400	1.742	811.0	1.738	.97196	19.98400	1.7153	812.4	1.742	.97533	20.06004	1.7153	812.4	1.742	.97533	20.06004	1.8848
3	0	.530	.0050	.1678	1.731	.96799	19.85017	1.731	807.8	1.731	.96813	19.85017	1.7140	809.2	1.734	.96778	19.94181	1.7140	809.2	1.734	.96778	19.94181	2.0085
4	0	.630	.0075	.2171	1.720	.96224	19.72692	1.720	804.6	1.724	.96459	19.82009	1.7125	807.6	1.731	.96786	19.90240	1.7125	807.6	1.731	.96786	19.90240	2.1654
5	0	.730	.0100	.2596	1.713	.95656	19.60384	1.713	802.0	1.720	.96238	19.72692	1.7110	804.4	1.723	.96603	19.82358	1.7110	804.4	1.723	.96603	19.82358	2.2938
6	0	1.200	.0150	.3348	1.698	.95084	19.48700	1.698	799.4	1.706	.95871	19.60384	1.7095	801.8	1.723	.96982	19.70534	1.7095	801.8	1.723	.96982	19.70534	2.4750
7	0	1.430	.0175	.3941	1.684	.94508	19.37076	1.684	796.8	1.702	.95266	19.55314	1.7080	800.0	1.720	.96222	19.58111	1.7080	800.0	1.720	.96222	19.58111	2.6451
8	0	1.630	.0200	.4546	1.669	.93937	19.25509	1.669	794.2	1.693	.95007	19.55314	1.7065	798.8	1.695	.96489	19.50826	1.7065	798.8	1.695	.96489	19.50826	2.7934
9	0	1.830	.0225	.5151	1.654	.93366	19.13959	1.654	791.6	1.677	.94371	19.43907	1.7050	796.0	1.684	.96017	19.46349	1.7050	796.0	1.684	.96017	19.46349	2.9306
10	0	2.030	.0250	.5756	1.639	.92795	19.02400	1.639	789.0	1.663	.93704	19.32509	1.7035	794.0	1.695	.96528	19.43158	1.7035	794.0	1.695	.96528	19.43158	3.0566
11	0	2.230	.0275	.6361	1.624	.92224	18.90840	1.624	786.4	1.648	.93012	19.21582	1.7020	791.4	1.695	.97031	19.39490	1.7020	791.4	1.695	.97031	19.39490	3.1766
12	0	2.430	.0300	.6966	1.609	.91653	18.79280	1.609	783.8	1.633	.92441	19.10324	1.7005	788.4	1.695	.97568	19.50859	1.7005	788.4	1.695	.97568	19.50859	3.2934
13	0	2.630	.0325	.7571	1.594	.91082	18.67720	1.594	781.2	1.618	.91870	19.00124	1.6990	785.6	1.695	.98083	19.63006	1.6990	785.6	1.695	.98083	19.63006	3.4084
14	0	2.830	.0350	.8176	1.579	.90511	18.56160	1.579	778.6	1.603	.91300	18.90124	1.6975	783.0	1.695	.98596	19.75258	1.6975	783.0	1.695	.98596	19.75258	3.5224
15	0	3.030	.0375	.8781	1.564	.89978	18.44600	1.564	776.0	1.588	.90789	18.80512	1.6960	780.4	1.695	.99109	19.87505	1.6960	780.4	1.695	.99109	19.87505	3.6364
16	0	3.230	.0400	.9386	1.549	.89489	18.33040	1.549	773.4	1.573	.90278	18.70486	1.6945	777.8	1.695	.99622	19.99760	1.6945	777.8	1.695	.99622	19.99760	3.7504
17	0	3.430	.0425	.9991	1.534	.88978	18.21480	1.534	770.8	1.558	.89767	18.60512	1.6930	775.2	1.695	.99719	20.12015	1.6930	775.2	1.695	.99719	20.12015	3.8644
18	0	3.630	.0450	1.0596	1.519	.88467	18.10000	1.519	768.2	1.543	.89256	18.50859	1.6915	772.6	1.695	.99719	20.24270	1.6915	772.6	1.695	.99719	20.24270	3.9784
19	0	3.830	.0475	1.1201	1.504	.87956	17.98440	1.504	765.6	1.528	.88745	18.40859	1.6900	770.0	1.695	.99719	20.36525	1.6900	770.0	1.695	.99719	20.36525	4.0924
20	0	4.030	.0500	1.1806	1.489	.87445	17.86880	1.489	763.0	1.513	.88234	18.30859	1.6885	767.4	1.695	.99719	20.48780	1.6885	767.4	1.695	.99719	20.48780	4.2064
21	0	4.230	.0525	1.2411	1.474	.86934	17.75320	1.474	760.4	1.498	.87723	18.20859	1.6870	764.8	1.695	.99719	20.61035	1.6870	764.8	1.695	.99719	20.61035	4.3204
22	0	4.430	.0550	1.3016	1.459	.86423	17.63760	1.459	757.8	1.483	.87212	18.10859	1.6855	762.2	1.695	.99719	20.73290	1.6855	762.2	1.695	.99719	20.73290	4.4344
23	0	4.630	.0575	1.3621	1.444	.85912	17.52200	1.444	755.2	1.468	.86701	18.00859	1.6840	759.6	1.695	.99719	20.85545	1.6840	759.6	1.695	.99719	20.85545	4.5484
24	0	4.830	.0600	1.4226	1.429	.85401	17.40640	1.429	752.6	1.453	.86190	17.90859	1.6825	757.0	1.695	.99719	20.97800	1.6825	757.0	1.695	.99719	20.97800	4.6624
25	0	5.030	.0625	1.4831	1.414	.84890	17.29080	1.414	750.0	1.438	.85679	17.80859	1.6810	754.4	1.695	.99719	21.10055	1.6810	754.4	1.695	.99719	21.10055	4.7764
26	0	5.230	.0650	1.5436	1.399	.84379	17.17520	1.399	747.4	1.423	.85168	17.70859	1.6795	751.8	1.695	.99719	21.22310	1.6795	751.8	1.695	.99719	21.22310	4.8904
27	0	5.430	.0675	1.6041	1.384	.83868	17.05960	1.384	744.8	1.408	.84657	17.60859	1.6780	749.2	1.695	.99719	21.34565	1.6780	749.2	1.695	.99719	21.34565	5.0044
28	0	5.630	.0700	1.6646	1.369	.83357	16.94400	1.369	742.2	1.393	.84146	17.50859	1.6765	746.6	1.695	.99719	21.46820	1.6765	746.6	1.695	.99719	21.46820	5.1184
29	0	5.830	.0725	1.7251	1.354	.82846	16.82840	1.354	740.0	1.378	.83635	17.40859	1.6750	744.0	1.695	.99719	21.59075	1.6750	744.0	1.695	.99719	21.59075	5.2324
30	0	6.030	.0750	1.7856	1.339	.82335	16.71280	1.339	737.4	1.363	.83124	17.30859	1.6735	742.0	1.695	.99719	21.71330	1.6735	742.0	1.695	.99719	21.71330	5.3464
31	0	6.230	.0775	1.8461	1.324	.81824	16.59720	1.324	735.2	1.348	.82613	17.20859	1.6720	739.4	1.695	.99719	21.83585	1.6720	739.4	1.695	.99719	21.83585	5.4604
32	0	6.430	.0800	1.9066	1.309	.81313	16.48160	1.309	733.0	1.333	.82102	17.10859	1.6705	737.0	1.695	.99719	21.95840	1.6705	737.0	1.695	.99719	21.95840	5.5744
33	0	6.630	.0825	1.9671	1.294	.80802	16.36600	1.294	730.8	1.318	.81591	17.00859	1.6690	734.8	1.695	.99719	22.08095	1.6690	734.8	1.695	.99719	22.08095	5.6884
34	0	6.830	.0850	2.0276	1.279	.80291	16.25040	1.279	728.6	1.303	.81080	16.90859	1.6675	732.2	1.695	.99719	22.20350	1.6675	732.2	1.695	.99719	22.20350	5.8024
35	0	7.030	.0875	2.0881	1.264	.79780	16.13480	1.264	726.4	1.288	.80569	16.80859	1.6660	730.0	1.695	.99719	22.32605	1.6660	730.0	1.695	.99719	22.32605	5.9164
36	0	7.230	.0900	2.1486	1.249	.79269	16.01920	1.249	724.2	1.273	.80058	16.70859	1.6645	727.8	1.695	.99719	22.44860	1.6645	727.8	1.695	.99719	22.44860	6.0304
37	0	7.430	.0925	2.2091	1.234	.78758	15.90360	1.234	722.0	1.258	.79547	16.60859	1.6630	725.6	1.695	.99719	22.57115	1.6630	725.6	1.695	.99719	22.57115	6.1444
38	0	7.630	.0950	2.2696	1.219	.78247	15.78800	1.219	719.8	1.243	.79036	16.50859	1.6615	723.4	1.695	.99719	22.69370	1.6615	723.4	1.695	.99719	22.69370	6.2584
39	0	7.830	.0975	2.3301	1.204	.77736	15.67240	1.204	717.6	1.228	.78525	16.40859	1.6600	721.2	1.695	.99719	22.81625	1.6600	721.2	1.695	.99719	22.81625	6.3724
40	0	8.030	.1000	2.3906	1.189	.77225	15.55680	1.189	715.4	1.213	.78014	16.30859	1.6585	719.0	1.695	.99719	22.93880	1.6585	719.0	1.695	.99719	22.93880	6.4864
41	0	8.230	.1025	2.4511	1.174	.76714	15.44120	1.174	713.2	1.198	.77503	16.20859	1.6570	716.8	1.695	.99719	23.06135	1.6570	716.8	1.695	.99719	23.06135	6.6004
42	0	8.430	.1050	2.5116	1.159	.76203	15.32560	1.159	711.0	1.183	.76992	16.10859	1.6555	714.6	1.695	.99719	23.18390	1.6555	714.6	1.695	.99719	23.18390	6.7144
43	0	8.630	.1075	2.5721	1.144	.75692	15.21000	1.144	708.8	1.168	.76481	16.00859	1.6540	712.4	1.695	.99719	23.30645	1.6540	712.4	1.695	.99719	23.30645	6.8284
44	0	8.830	.1100	2.6326	1.129	.75181	15.0																

TABLE VII.- DATA^a FOR 160° CONE; $M_{\infty} = 3.95$ - Continued(b) $\alpha = 5^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 67.5^\circ, p_t = 5762.6 \text{ psf}$				$\Phi = 90.0^\circ, p_t = 5762.6 \text{ psf}$			
				p_t , psf	C_p	$p_t/p_{t,2}$	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	M_t
1	0	.300	.0000	817.5	1.753	.9770	20.16587	813.7	1.756	.98121	20.17687
2	0	.200	.0055	815.9	1.749	.9778	20.10644	811.7	1.756	.98121	20.17687
3	0	.100	.0185	815.9	1.749	.9778	20.10644	811.7	1.756	.98121	20.17687
4	0	.030	.075	812.7	1.742	.97395	20.02759	815.5	1.752	.97729	20.13746
5	0	.800	.100	811.1	1.739	.97203	19.98817	812.3	1.751	.97552	20.09405
6	0	1.300	.125	807.9	1.731	.96820	19.91905	806.0	1.748	.97184	20.05064
7	0	1.800	.150	804.8	1.723	.96436	19.85000	802.8	1.745	.96820	20.00723
8	0	2.300	.175	801.6	1.715	.95961	19.78120	799.6	1.742	.96504	19.96382
9	0	2.800	.200	798.4	1.707	.95486	19.71220	796.4	1.739	.96204	19.92041
10	0	3.300	.225	795.1	1.699	.95011	19.64320	793.1	1.736	.95904	19.87700
11	0	3.800	.250	791.9	1.691	.94536	19.57420	789.9	1.733	.95604	19.83359
12	0	4.300	.275	788.6	1.683	.94061	19.50520	786.6	1.730	.95304	19.79018
13	0	4.800	.300	785.4	1.675	.93586	19.43620	783.4	1.727	.95004	19.74677
14	0	5.300	.325	782.1	1.667	.93111	19.36720	780.1	1.724	.94704	19.70336
15	0	5.800	.350	778.9	1.659	.92636	19.29820	776.9	1.721	.94404	19.65995
16	0	6.300	.375	775.6	1.651	.92161	19.22920	773.6	1.718	.94104	19.61654
17	0	6.800	.400	772.4	1.643	.91686	19.16020	770.4	1.715	.93804	19.57313
18	0	7.300	.425	769.1	1.635	.91211	19.09120	767.1	1.712	.93504	19.52972
19	0	7.800	.450	765.9	1.627	.90736	19.02220	763.9	1.709	.93204	19.48631
20	0	8.300	.475	762.6	1.619	.90261	18.95320	760.6	1.706	.92904	19.44290
21	0	8.800	.500	759.4	1.611	.89786	18.88420	757.4	1.703	.92604	19.39949
22	0	9.300	.525	756.1	1.603	.89311	18.81520	754.1	1.700	.92304	19.35608
23	0	9.800	.550	752.9	1.595	.88836	18.74620	750.9	1.697	.92004	19.31267
24	0	10.300	.575	749.6	1.587	.88361	18.67720	747.6	1.694	.91704	19.26926
25	0	10.800	.600	746.4	1.579	.87886	18.60820	744.4	1.691	.91404	19.22585
26	0	11.300	.625	743.1	1.571	.87411	18.53920	741.1	1.688	.91104	19.18244
27	0	11.800	.650	739.9	1.563	.86936	18.47020	737.9	1.685	.90804	19.13903
28	0	12.300	.675	736.6	1.555	.86461	18.40120	734.6	1.682	.90504	19.09562
29	0	12.800	.700	733.4	1.547	.85986	18.33220	731.4	1.679	.90204	19.05221
30	0	13.300	.725	730.1	1.539	.85511	18.26320	728.1	1.676	.89904	19.00880
31	0	13.800	.750	726.9	1.531	.85036	18.19420	724.9	1.673	.89604	18.96539
32	0	14.300	.775	723.6	1.523	.84561	18.12520	721.6	1.670	.89304	18.92198
33	0	14.800	.800	720.4	1.515	.84086	18.05620	718.4	1.667	.89004	18.87857
34	0	15.300	.825	717.1	1.507	.83611	17.98720	715.1	1.664	.88704	18.83516
35	0	15.800	.850	713.9	1.499	.83136	17.91820	711.9	1.661	.88404	18.79175
36	0	16.300	.875	710.6	1.491	.82661	17.84920	708.6	1.658	.88104	18.74834
37	0	16.800	.900	707.4	1.483	.82186	17.78020	705.4	1.655	.87804	18.70493
38	0	17.300	.925	704.1	1.475	.81711	17.71120	702.1	1.652	.87504	18.66152
39	0	17.800	.950	700.9	1.467	.81236	17.64220	698.9	1.649	.87204	18.61811
40	0	18.300	.975	697.6	1.459	.80761	17.57320	695.6	1.646	.86904	18.57470
41	0	18.800	.100	694.4	1.451	.80286	17.50420	692.4	1.643	.86604	18.53129
42	0	19.300	.105	691.1	1.443	.79811	17.43520	689.1	1.640	.86304	18.48788
43	0	19.800	.110	687.9	1.435	.79336	17.36620	685.9	1.637	.86004	18.44447
44	0	20.300	.115	684.6	1.427	.78861	17.29720	682.6	1.634	.85704	18.40106
45	0	20.800	.120	681.4	1.419	.78386	17.22820	679.4	1.631	.85404	18.35765
46	0	21.300	.125	678.1	1.411	.77911	17.15920	676.1	1.628	.85104	18.31424
47	0	21.800	.130	674.9	1.403	.77436	17.09020	672.9	1.625	.84804	18.27083
48	0	22.300	.135	671.6	1.395	.76961	17.02120	669.6	1.622	.84504	18.22742
49	0	22.800	.140	668.4	1.387	.76486	16.95220	666.4	1.619	.84204	18.18401
50	0	23.300	.145	665.1	1.379	.76011	16.88320	663.1	1.616	.83904	18.14060

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VII.- DATA^a FOR 160° CONE; $M_{\infty} = 3.95$ - Continued(c) $\alpha = 10^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0.0^\circ, P_t = 5762.6 \text{ psf}$					$\Phi = 22.5^\circ, P_t = 5762.6 \text{ psf}$					$\Phi = 45.0^\circ, P_t = 5762.6 \text{ psf}$				
				$P_{t, \text{ psf}}$	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	$P_{t, \text{ psf}}$	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	$P_{t, \text{ psf}}$	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t
1	0	0.00	0.000	799.7	1.713	95841	19.70809	24709	799.7	1.713	95834	19.70871	24730	799.9	1.713	95868	19.71357	24628
2	0	0.20	0.025	793.3	1.698	95074	19.55042	26600	793.3	1.698	95068	19.54906	26919	795.1	1.703	95292	19.57143	24628
3	0	0.40	0.095	780.1	1.691	94691	19.47159	28025	783.3	1.691	94676	19.47017	28342	785.1	1.703	95292	19.57143	24628
4	0	0.60	0.178	769.3	1.680	94319	19.40231	29049	773.3	1.680	94304	19.40093	29366	775.1	1.703	95292	19.57143	24628
5	0	0.80	0.263	760.1	1.666	93948	19.33281	30069	763.3	1.666	93933	19.33143	30386	765.1	1.685	94334	19.57981	24628
6	0	1.00	0.350	750.1	1.652	93577	19.26352	31089	753.3	1.652	93562	19.26214	31403	755.1	1.685	94334	19.57981	24628
7	0	1.20	0.438	740.1	1.644	93206	19.19423	32109	743.3	1.644	93191	19.19285	32423	745.1	1.685	94334	19.57981	24628
8	0	1.40	0.526	730.1	1.637	92835	19.12494	33129	733.3	1.637	92820	19.12356	33443	735.1	1.685	94334	19.57981	24628
9	0	1.60	0.614	720.1	1.623	92464	19.05565	34149	723.3	1.623	92449	19.05427	34463	725.1	1.685	94334	19.57981	24628
10	0	1.80	0.702	710.1	1.615	92093	18.98636	35169	713.3	1.615	92078	18.98498	35483	715.1	1.685	94334	19.57981	24628
11	0	2.00	0.790	700.1	1.601	91722	18.91707	36189	703.3	1.601	91707	18.91569	36503	705.1	1.685	94334	19.57981	24628
12	0	2.20	0.878	690.1	1.588	91351	18.84778	37209	693.3	1.588	91336	18.84640	37523	695.1	1.612	90499	18.90961	33035
13	0	2.40	0.966	680.1	1.574	90980	18.77849	38229	683.3	1.574	90965	18.77711	38543	685.1	1.582	88172	18.85772	33035
14	0	2.60	1.054	670.1	1.560	90609	18.70920	39249	673.3	1.560	90594	18.70782	39563	675.1	1.582	88172	18.85772	33035
15	0	2.80	1.142	660.1	1.546	90238	18.63991	40269	663.3	1.546	90223	18.63853	40583	665.1	1.582	88172	18.85772	33035
16	0	3.00	1.230	650.1	1.532	89867	18.57062	41289	653.3	1.532	89852	18.57024	41603	655.1	1.582	88172	18.85772	33035
17	0	3.20	1.318	640.1	1.518	89496	18.50133	42309	643.3	1.518	89481	18.50095	42523	645.1	1.582	88172	18.85772	33035
18	0	3.40	1.406	630.1	1.504	89125	18.43204	43329	633.3	1.504	89110	18.43166	43643	635.1	1.582	88172	18.85772	33035
19	0	3.60	1.494	620.1	1.490	88754	18.36275	44349	623.3	1.490	88739	18.36237	44663	625.1	1.582	88172	18.85772	33035
20	0	3.80	1.582	610.1	1.476	88383	18.29346	45369	613.3	1.476	88368	18.29308	45683	615.1	1.582	88172	18.85772	33035
21	0	4.00	1.670	600.1	1.462	88012	18.22417	46389	603.3	1.462	88007	18.22379	46703	605.1	1.582	88172	18.85772	33035
22	0	4.20	1.758	590.1	1.448	87641	18.15488	47409	593.3	1.448	87626	18.15450	47723	595.1	1.582	88172	18.85772	33035
23	0	4.40	1.846	580.1	1.434	87270	18.08559	48429	583.3	1.434	87255	18.08521	48743	585.1	1.582	88172	18.85772	33035
24	0	4.60	1.934	570.1	1.420	86899	18.01630	49449	573.3	1.420	86884	18.01592	49763	575.1	1.582	88172	18.85772	33035
25	0	4.80	2.022	560.1	1.406	86528	17.94701	50469	563.3	1.406	86513	17.94663	50683	565.1	1.582	88172	18.85772	33035
26	0	5.00	2.110	550.1	1.392	86157	17.87772	51489	553.3	1.392	86142	17.87734	51803	555.1	1.582	88172	18.85772	33035
27	0	5.20	2.198	540.1	1.378	85786	17.80843	52509	543.3	1.378	85771	17.80805	52823	545.1	1.582	88172	18.85772	33035
28	0	5.40	2.286	530.1	1.364	85415	17.73914	53529	533.3	1.364	85400	17.73876	53843	535.1	1.582	88172	18.85772	33035
29	0	5.60	2.374	520.1	1.350	85044	17.66985	54549	523.3	1.350	85029	17.66947	54863	525.1	1.582	88172	18.85772	33035
30	0	5.80	2.462	510.1	1.336	84673	17.60056	55569	513.3	1.336	84658	17.60018	55883	515.1	1.582	88172	18.85772	33035
31	0	6.00	2.550	500.1	1.322	84302	17.53127	56589	503.3	1.322	84287	17.53089	56897	505.1	1.582	88172	18.85772	33035
32	0	6.20	2.638	490.1	1.308	83931	17.46198	57609	493.3	1.308	83916	17.46160	58011	495.1	1.582	88172	18.85772	33035
33	0	6.40	2.726	480.1	1.294	83560	17.39269	58629	483.3	1.294	83545	17.39231	58923	485.1	1.582	88172	18.85772	33035
34	0	6.60	2.814	470.1	1.280	83189	17.32340	59649	473.3	1.280	83174	17.32302	59923	475.1	1.582	88172	18.85772	33035
35	0	6.80	2.902	460.1	1.266	82818	17.25411	60669	463.3	1.266	82803	17.25373	60923	465.1	1.582	88172	18.85772	33035
36	0	7.00	2.990	450.1	1.252	82447	17.18482	61689	453.3	1.252	82432	17.18444	61923	455.1	1.582	88172	18.85772	33035
37	0	7.20	3.078	440.1	1.238	82076	17.11553	62709	443.3	1.238	82061	17.11515	63023	445.1	1.582	88172	18.85772	33035
38	0	7.40	3.166	430.1	1.224	81705	17.04624	63729	433.3	1.224	81690	17.04586	63923	435.1	1.582	88172	18.85772	33035
39	0	7.60	3.254	420.1	1.210	81334	16.97695	64749	423.3	1.210	81319	16.97657	64923	425.1	1.582	88172	18.85772	33035
40	0	7.80	3.342	410.1	1.196	80963	16.90766	65769	413.3	1.196	80948	16.90728	65923	415.1	1.582	88172	18.85772	33035
41	0	8.00	3.430	400.1	1.182	80592	16.83837	66789	403.3	1.182	80577	16.83799	66923	405.1	1.582	88172	18.85772	33035
42	0	8.20	3.518	390.1	1.168	80221	16.76908	67809	393.3	1.168	80206	16.76870	67923	395.1	1.582	88172	18.85772	33035
43	0	8.40	3.606	380.1	1.154	79850	16.70079	68829	383.3	1.154	79835	16.70041	68923	385.1	1.582	88172	18.85772	33035
44	0	8.60	3.694	370.1	1.140	79479	16.63150	69849	373.3	1.140	79464	16.63112	69923	375.1	1.582	88172	18.85772	33035
45	0	8.80	3.782	360.1	1.126	79108	16.56221	70869	363.3	1.126	79093	16.56183	70923	365.1	1.582	88172	18.85772	33035
46	0	9.00	3.870	350.1	1.112	78737	16.49292	71889	353.3	1.112	78722	16.49254	71923	355.1	1.582	88172	18.85772	33035
47	0	9.20	3.958	340.1	1.098	78366	16.42363	72909	343.3	1.098	78351	16.42325	72923	345.1	1.582	88172	18.85772	33035
48	0	9.40	4.046	330.1	1.084	77995	16.35434	73929	333.3	1.084	77980	16.35396	73923	335.1	1.582	88172	18.85772	33035
49	0	9.60	4.134	320.1	1.070	77624	16.28505	74949	323.3	1.070	77609	16.28467	74923	325.1	1.582	88172	18.85772	33035

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VII.- DATA^a FOR 160° CONE; $M_{\infty} = 3.95$ - Continued(c) $\alpha = 10^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ$, $P_t = 5762.6$ psf					$\Phi = 90.0^\circ$, $P_t = 5762.6$ psf				
				$P_{t,1}$	C_p	$P_{t,1}/P_{t,2}$	$P_{t,1}/P_{t,0}$	$M_{t,1}$	$P_{t,2}$ psf	C_p	$P_{t,2}/P_{t,2}$	$P_{t,2}/P_{t,0}$	$M_{t,2}$
1	0	-0.30	-0.000	801.6	1.717	0.96066	19.75437	24013	820.0	1.714	0.95874	19.71494	24607
2	0	-0.20	-0.025	798.4	1.710	0.95683	19.67551	22589	800.0	1.714	0.95874	19.71494	24607
3	0	-0.10	-0.050	795.2	1.706	0.95299	19.63608	22579	800.0	1.714	0.95874	19.71494	24607
4	0	-0.00	-0.075	792.0	1.703	0.94915	19.59665	22579	798.4	1.710	0.9543	19.67551	24607
5	0	0.30	-0.100	788.8	1.699	0.94531	19.55722	22605	798.4	1.710	0.9543	19.67551	24607
6	0	1.30	-0.150	788.8	1.688	0.94532	19.43603	22657	795.8	1.706	0.9491	19.63608	22579
7	0	1.20	-0.125	785.6	1.677	0.93957	19.32064	22695	793.6	1.699	0.93107	19.55722	22666
8	0	1.40	-0.175	780.8	1.670	0.93373	19.24178	22691	782.0	1.695	0.9416	19.51779	22705
9	0	1.50	-0.200	775.2	1.663	0.92723	19.16308	22714	775.2	1.691	0.9357	19.47836	22707
10	0	1.30	-0.225	771.2	1.669	0.92423	19.00520	22741	784.0	1.677	0.9357	19.32064	22707
11	0	2.30	-0.250	765.6	1.638	0.91848	18.88691	22772	779.2	1.667	0.9382	0.9382	314.30
12	0	2.20	-0.275	759.0	1.623	0.91081	18.72919	22818	772.8	1.652	0.92615	19.00443	332.89
13	0	2.40	-0.300	753.6	1.609	0.90314	18.57147	22840	765.0	1.641	0.92039	18.92634	346.30
14	0	2.50	-0.325	748.0	1.595	0.89547	18.41375	22862	758.4	1.623	0.91261	18.72919	360.78
15	0	2.80	-0.350	742.4	1.580	0.88780	18.25603	22884	750.0	1.605	0.90484	18.57147	375.26
16	0	3.30	-0.375	736.8	1.564	0.88012	18.09831	22906	743.2	1.576	0.89688	18.21660	390.69
17	0	3.20	-0.400	730.8	1.508	0.86945	17.46744	22928	723.2	1.540	0.86700	17.82230	456.73
18	0	3.40	-0.425	724.8	1.468	0.85878	16.83656	22950	717.2	1.504	0.84753	17.42801	491.94
19	0	3.60	-0.450	718.8	1.428	0.84811	16.20568	22972	711.2	1.468	0.83686	16.82508	536.92
20	0	3.80	-0.475	712.8	1.388	0.83744	15.57480	22994	705.2	1.432	0.82619	16.20568	582.10
21	0	4.30	-0.500	706.8	1.190	0.68071	13.93761	23016	584.0	1.223	0.69988	14.39191	712.58
22	180	-0.20	-0.025	804.3	1.740	0.97300	20.00812	19813	808.7	1.733	0.95717	19.92935	211.98
23	180	-0.10	-0.050	801.9	1.740	0.97300	20.00812	19813	807.1	1.730	0.95725	19.88996	218.61
24	180	-0.00	-0.075	799.5	1.740	0.97300	20.00812	19813	805.5	1.730	0.95730	19.88996	218.61
25	180	0.10	-0.100	797.1	1.740	0.97300	20.00812	19813	803.7	1.715	0.95966	19.73242	221.33
26	180	0.20	-0.125	794.7	1.740	0.97300	20.00812	19813	802.0	1.715	0.95966	19.73242	221.33
27	180	0.30	-0.150	792.3	1.733	0.96317	19.92935	211.98	799.1	1.712	0.95768	19.63030	224.92
28	180	0.40	-0.175	789.9	1.733	0.96317	19.92935	211.98	795.9	1.704	0.95385	19.53426	226.69
29	180	0.50	-0.200	787.5	1.726	0.9534	19.85098	225.05	792.7	1.687	0.95002	19.46426	228.44
30	180	0.60	-0.225	785.1	1.726	0.9534	19.85098	225.05	789.1	1.679	0.94644	19.35617	230.19
31	180	0.70	-0.250	782.7	1.712	0.94363	19.63030	226.32	784.2	1.679	0.94644	19.35617	230.19
32	180	0.80	-0.275	780.3	1.701	0.93382	19.40973	227.59	780.3	1.665	0.93278	19.18101	231.67
33	180	0.90	-0.300	777.9	1.690	0.92401	19.18954	228.86	777.9	1.650	0.92512	19.02347	233.52
34	180	1.00	-0.325	775.5	1.675	0.91420	18.96935	229.13	775.5	1.636	0.91746	18.86593	235.92
35	180	1.10	-0.350	773.1	1.660	0.90439	18.74916	229.40	773.1	1.616	0.90926	18.66261	238.27
36	180	1.20	-0.375	770.7	1.645	0.89458	18.52897	229.67	770.7	1.599	0.90246	18.45931	240.57
37	180	1.30	-0.400	768.3	1.630	0.88477	18.30878	229.94	768.3	1.580	0.89569	18.25642	242.82
38	180	1.40	-0.425	765.9	1.615	0.87496	18.08859	230.21	765.9	1.560	0.88823	18.05382	245.07
39	180	1.50	-0.450	763.5	1.600	0.86515	17.86840	230.48	763.5	1.540	0.88076	17.85098	247.32
40	180	1.60	-0.475	761.1	1.585	0.85534	17.64821	230.75	761.1	1.520	0.87328	17.6528	249.57
41	180	1.70	-0.500	758.7	1.570	0.84553	17.42802	231.02	758.7	1.500	0.86581	17.45043	251.82
42	270	-0.30	-0.025	804.3	1.712	0.95823	19.75269	24013	820.0	1.704	0.9552	19.75269	24607
43	270	-0.20	-0.050	798.4	1.708	0.95576	19.65385	22506	803.9	1.722	0.9542	19.81198	24607
44	270	-0.10	-0.075	792.0	1.708	0.95576	19.65385	22506	803.9	1.722	0.9542	19.81198	24607
45	270	0.10	-0.100	785.6	1.699	0.94531	19.55722	22605	798.4	1.706	0.9491	19.63608	24607
46	270	0.20	-0.125	779.2	1.695	0.94140	19.51779	22705	792.0	1.699	0.9416	19.51779	24607
47	270	0.30	-0.150	772.8	1.691	0.93670	19.47836	22805	785.6	1.695	0.94140	19.47836	24607
48	270	0.40	-0.175	766.4	1.687	0.93190	19.43895	22905	779.2	1.691	0.93190	19.43895	24607
49	270	0.50	-0.200	760.0	1.683	0.92710	19.39954	23005	772.8	1.687	0.92710	19.39954	24607
50	270	0.60	-0.225	753.6	1.679	0.92230	19.36013	23105	766.4	1.683	0.92230	19.36013	24607
51	270	0.70	-0.250	747.2	1.675	0.91750	19.32072	23205	760.0	1.679	0.91750	19.32072	24607
52	270	0.80	-0.275	740.8	1.671	0.91270	19.28131	23305	753.6	1.675	0.91270	19.28131	24607
53	270	0.90	-0.300	734.4	1.667	0.90790	19.24190	23405	747.2	1.671	0.90790	19.24190	24607
54	270	1.00	-0.325	728.0	1.663	0.90310	19.20249	23505	740.8	1.667	0.90310	19.20249	24607
55	270	1.10	-0.350	721.6	1.659	0.89830	19.16308	23605	734.4	1.663	0.89830	19.16308	24607
56	270	1.20	-0.375	715.2	1.655	0.89350	19.12367	23705	728.0	1.659	0.89350	19.12367	24607
57	270	1.30	-0.400	708.8	1.651	0.88870	19.08426	23805	721.6	1.655	0.88870	19.08426	24607
58	270	1.40	-0.425	702.4	1.647	0.88390	19.04485	23905	715.2	1.651	0.88390	19.04485	24607
59	270	1.50	-0.450	696.0	1.643	0.87910	19.00544	24005	708.8	1.647	0.87910	19.00544	24607
60	270	1.60	-0.475	689.6	1.639	0.87430	18.96603	24105	702.4	1.643	0.87430	18.96603	24607
61	270	1.70	-0.500	683.2	1.635	0.86950	18.92662	24205	696.0	1.639	0.86950	18.92662	24607
62	360	-0.20	-0.025	804.3	1.712	0.95823	19.75269	24013	820.0	1.704	0.9552	19.75269	24607
63	360	-0.10	-0.050	798.4	1.708	0.95576	19.65385	22506	803.9	1.722	0.9542	19.81198	24607
64	360	-0.00	-0.075	792.0	1.708	0.95576	19.65385	22506	803.9	1.722	0.9542	19.81198	24607
65	360	0.10	-0.100	785.6	1.699	0.94531	19.55722	22605	798.4	1.706	0.9491	19.63608	24607
66	360	0.20	-0.125	779.2	1.695	0.94140	19.51779	22705	792.0	1.699	0.9416	19.51779	24607
67	360	0.30	-0.150	772.8	1.691	0.93670	19.47836	22805	785.6	1.695	0.94140	19.47836	24607
68	360	0.40	-0.175	766.4	1.687	0.93190	19.43895	22905	779.2	1.691	0.93190	19.43895	24607
69	360	0.50	-0.200	760.0	1.683	0.92710	19.39954	23005	772.8	1.687	0.92710	19.39954	24607
70	360	0.60	-0.225	753.6	1.679	0.92230	19.36013	23105	766.4	1.683	0.92230	19.36013	24607
71	360	0.70	-0.250	747.2	1.675	0.91750	19.32072	23205	760.0	1.679	0.91750	19.32072	24607
72	360	0.80	-0.275	740.8	1.671	0.91270	19.28131	23305	753.6	1.675	0.91270	19.28131	24607
73	360	0.90	-0.300	734.4	1.667	0.90790	19.24190	23405	747.2	1.671	0.90790	19.24190	24607
74	360	1.00	-0.325	728.0	1.663	0.90310	19.20249	23505	740.8	1.667	0.90310	19.20249	24607
75	360	1.10	-0.350	721.6	1.659	0.89830	19.16308	23605	734.4	1.663	0.89830	19.16308	24607
76	360	1.20	-0.375	715.2	1.655	0.89350	19.12367	23705	728.0	1.659	0.89350	19.12367	24607
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TABLE VII.- DATA^a FOR 160° CONE; $M_{\infty} = 3.95$ - Continued

(d) $\alpha = 15^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, p_t = 5762.6 \text{ psf}$				
				p_t , psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}	M_t
1	0	-0.00	-0.000	771.3	1.669	.92437	19.00786	.3310
2	0	-0.00	-0.000	761.7	1.627	.91255	18.90067	.3502
3	0	-0.00	-0.005	758.5	1.620	.90901	18.77123	.3628
4	0	-0.00	-0.010	755.3	1.613	.90518	18.66236	.3769
5	0	-0.00	-0.015	752.1	1.606	.90118	18.61349	.3896
6	0	-0.00	-0.020	748.9	1.599	.89715	18.53751	.4018
7	0	-0.00	-0.025	745.7	1.593	.89308	18.43744	.4129
8	0	-0.00	-0.030	742.5	1.587	.88901	18.31790	.4235
9	0	-0.00	-0.035	739.3	1.581	.88494	18.17970	.4328
10	0	-0.00	-0.040	736.1	1.575	.88087	18.02196	.4424
11	0	-0.00	-0.045	732.9	1.569	.87680	17.84422	.4529
12	0	-0.00	-0.050	729.7	1.563	.87273	17.64748	.4634
13	0	-0.00	-0.055	726.5	1.557	.86866	17.43274	.4739
14	0	-0.00	-0.060	723.3	1.551	.86459	17.20000	.4841
15	0	-0.00	-0.065	720.1	1.545	.86052	16.94930	.4940
16	0	-0.00	-0.070	716.9	1.539	.85645	16.68156	.5036
17	0	-0.00	-0.075	713.7	1.533	.85238	16.39782	.5129
18	0	-0.00	-0.080	710.5	1.527	.84831	16.10000	.5216
19	0	-0.00	-0.085	707.3	1.521	.84424	15.78910	.5296
20	0	-0.00	-0.090	704.1	1.515	.84017	15.46510	.5368
21	0	-0.00	-0.095	700.9	1.509	.83610	15.12810	.5430
22	0	-0.00	-0.100	697.7	1.503	.83203	14.77810	.5482
23	180	-0.00	-0.095	805.6	1.726	.96547	19.85334	.2261
24	180	-0.00	-0.090	812.0	1.741	.97314	20.01090	.19762
25	180	-0.00	-0.085	818.4	1.756	.98081	20.16850	.16818
26	180	-0.00	-0.080	824.8	1.771	.98846	20.32604	.13875
27	180	-0.00	-0.075	831.2	1.786	.99611	20.48358	.10932
28	180	-0.00	-0.070	837.6	1.801	.10000	20.64112	.07989
29	180	-0.00	-0.065	844.0	1.816	.10389	20.79866	.05046
30	180	-0.00	-0.060	850.4	1.831	.10778	20.95620	.02103
31	180	-0.00	-0.055	856.8	1.846	.11167	21.11374	.00000
32	180	-0.00	-0.050	863.2	1.861	.11556	21.27128	.00000
33	180	-0.00	-0.045	869.6	1.876	.11945	21.42882	.00000
34	180	-0.00	-0.040	876.0	1.891	.12334	21.58636	.00000
35	180	-0.00	-0.035	882.4	1.906	.12723	21.74390	.00000
36	180	-0.00	-0.030	888.8	1.921	.13112	21.90144	.00000
37	180	-0.00	-0.025	895.2	1.936	.13501	22.05898	.00000
38	180	-0.00	-0.020	901.6	1.951	.13890	22.21652	.00000
39	180	-0.00	-0.015	908.0	1.966	.14279	22.37406	.00000
40	180	-0.00	-0.010	914.4	1.981	.14668	22.53160	.00000
41	180	-0.00	-0.005	920.8	1.996	.15057	22.68914	.00000
42	270	-0.00	-0.000	927.2	2.011	.15446	22.84668	.00000
43	270	-0.00	-0.005	933.6	2.026	.15835	23.00422	.00000
44	270	-0.00	-0.010	940.0	2.041	.16224	23.16176	.00000
45	270	-0.00	-0.015	946.4	2.056	.16613	23.31930	.00000
46	90	-0.00	-0.020	952.8	2.071	.17002	23.47684	.00000
47	90	-0.00	-0.025	959.2	2.086	.17391	23.63438	.00000
48	90	-0.00	-0.030	965.6	2.101	.17780	23.79192	.00000
49	90	-0.00	-0.035	972.0	2.116	.18169	23.94946	.00000

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VII.- DATA^a FOR 160° CONE; $M_{\infty} = 3.95$ - Continued(e) $\alpha = 20^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ$, $P_t = 5762.6$ psf					$\Phi = 22.5^\circ$, $P_t = 5762.6$ psf					$\Phi = 45.0^\circ$, $P_t = 5762.6$ psf					
				P_t , psf	C_p	$P_t/P_{t,2}$	P_t/∞	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	P_t/∞	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	P_t/∞	M_t	P_t , psf
1	0	.500	.0000	731.1	1.558	.87623	18.01820	.43859	731.6	1.559	.87681	18.03004	.43748	730.9	1.558	.87632	18.01319	.43906	
2	0	.250	.0025	721.5	1.537	.86473	17.78164	.46044	723.6	1.541	.86723	17.83321	.45573	724.5	1.543	.86832	17.85553	.43966	
3	0	.125	.0050	712.1	1.520	.85344	17.61077	.48284	715.4	1.541	.86723	17.83321	.45573	726.1	1.547	.87024	17.89494	.44006	
4	0	.063	.0075	703.1	1.504	.84236	17.45107	.50584	707.4	1.534	.86140	17.78447	.45281	727.9	1.540	.87147	17.92447	.44046	
5	0	.030	.0100	694.4	1.489	.83159	17.30278	.52964	700.4	1.523	.85192	17.64622	.45006	729.4	1.532	.86257	17.97328	.44086	
6	0	.015	.0125	686.3	1.474	.82124	17.16450	.55384	693.4	1.512	.84236	17.51827	.44740	731.9	1.532	.86257	17.97328	.44086	
7	0	.008	.0150	678.8	1.458	.81134	17.03622	.57844	686.4	1.502	.83291	17.39999	.44484	734.4	1.532	.86257	17.97328	.44086	
8	0	.004	.0175	671.8	1.443	.80189	16.91794	.60344	679.4	1.492	.82346	17.29171	.44238	736.9	1.532	.86257	17.97328	.44086	
9	0	.002	.0200	664.8	1.428	.79282	16.80962	.62884	672.4	1.482	.81401	17.18343	.44000	739.4	1.532	.86257	17.97328	.44086	
10	0	.001	.0225	657.8	1.413	.78414	16.70126	.65464	665.4	1.472	.80458	17.07515	.43772	741.9	1.532	.86257	17.97328	.44086	
11	0	.000	.0250	650.8	1.398	.77586	16.59290	.68084	658.4	1.462	.79515	16.96687	.43554	744.4	1.532	.86257	17.97328	.44086	
12	0	.000	.0275	643.8	1.383	.76797	16.48454	.70744	651.4	1.452	.78572	16.85859	.43346	746.9	1.532	.86257	17.97328	.44086	
13	0	.000	.0300	636.8	1.368	.76048	16.37618	.73444	644.4	1.442	.77629	16.75031	.43148	749.4	1.532	.86257	17.97328	.44086	
14	0	.000	.0325	629.8	1.353	.75339	16.26782	.76184	637.4	1.432	.76686	16.64203	.42960	751.9	1.532	.86257	17.97328	.44086	
15	0	.000	.0350	622.8	1.338	.74670	16.15946	.78964	630.4	1.422	.75743	16.53375	.42782	754.4	1.532	.86257	17.97328	.44086	
16	0	.000	.0375	615.8	1.323	.74041	16.05110	.81784	623.4	1.412	.74800	16.42547	.42614	756.9	1.532	.86257	17.97328	.44086	
17	0	.000	.0400	608.8	1.308	.73452	15.94274	.84644	616.4	1.402	.73857	16.31719	.42456	759.4	1.532	.86257	17.97328	.44086	
18	0	.000	.0425	601.8	1.293	.72903	15.83438	.87544	609.4	1.392	.72914	16.20891	.42308	761.9	1.532	.86257	17.97328	.44086	
19	0	.000	.0450	594.8	1.278	.72394	15.72602	.90484	602.4	1.382	.71971	16.10063	.42170	764.4	1.532	.86257	17.97328	.44086	
20	0	.000	.0475	587.8	1.263	.71925	15.61766	.93464	595.4	1.372	.71028	16.00000	.42042	766.9	1.532	.86257	17.97328	.44086	
21	0	.000	.0500	580.8	1.248	.71506	15.50930	.96484	588.4	1.362	.70085	15.90000	.41924	769.4	1.532	.86257	17.97328	.44086	
22	0	.000	.0525	573.8	1.233	.71127	15.40094	.99544	581.4	1.352	.69142	15.80000	.41816	771.9	1.532	.86257	17.97328	.44086	
23	0	.000	.0550	566.8	1.218	.70788	15.29258	.10264	574.4	1.342	.68200	15.70000	.41718	774.4	1.532	.86257	17.97328	.44086	
24	0	.000	.0575	559.8	1.203	.70489	15.18422	.11024	567.4	1.332	.67257	15.60000	.41630	776.9	1.532	.86257	17.97328	.44086	
25	0	.000	.0600	552.8	1.188	.70230	15.07586	.11824	560.4	1.322	.66315	15.50000	.41552	779.4	1.532	.86257	17.97328	.44086	
26	0	.000	.0625	545.8	1.173	.69991	14.96750	.12664	553.4	1.312	.65372	15.40000	.41484	781.9	1.532	.86257	17.97328	.44086	
27	0	.000	.0650	538.8	1.158	.69899	14.85914	.13544	546.4	1.302	.64430	15.30000	.41426	784.4	1.532	.86257	17.97328	.44086	
28	0	.000	.0675	531.8	1.143	.69799	14.75078	.14464	539.4	1.292	.63487	15.20000	.41378	786.9	1.532	.86257	17.97328	.44086	
29	0	.000	.0700	524.8	1.128	.69699	14.64242	.15424	532.4	1.282	.62545	15.10000	.41340	789.4	1.532	.86257	17.97328	.44086	
30	0	.000	.0725	517.8	1.113	.69599	14.53406	.16424	525.4	1.272	.61602	15.00000	.41312	791.9	1.532	.86257	17.97328	.44086	
31	0	.000	.0750	510.8	1.098	.69499	14.42570	.17464	518.4	1.262	.60660	14.90000	.41294	794.4	1.532	.86257	17.97328	.44086	
32	0	.000	.0775	503.8	1.083	.69399	14.31734	.18544	511.4	1.252	.59717	14.80000	.41286	796.9	1.532	.86257	17.97328	.44086	
33	0	.000	.0800	496.8	1.068	.69299	14.20898	.19664	504.4	1.242	.58775	14.70000	.41278	799.4	1.532	.86257	17.97328	.44086	
34	0	.000	.0825	489.8	1.053	.69199	14.10062	.20824	497.4	1.232	.57832	14.60000	.41270	801.9	1.532	.86257	17.97328	.44086	
35	0	.000	.0850	482.8	1.038	.69099	14.00000	.22024	490.4	1.222	.56890	14.50000	.41262	804.4	1.532	.86257	17.97328	.44086	
36	0	.000	.0875	475.8	1.023	.69000	13.90000	.23264	483.4	1.212	.55947	14.40000	.41254	806.9	1.532	.86257	17.97328	.44086	
37	0	.000	.0900	468.8	1.008	.68900	13.80000	.24544	476.4	1.202	.55005	14.30000	.41246	809.4	1.532	.86257	17.97328	.44086	
38	0	.000	.0925	461.8	0.993	.68800	13.70000	.25864	469.4	1.192	.54062	14.20000	.41238	811.9	1.532	.86257	17.97328	.44086	
39	0	.000	.0950	454.8	0.978	.68700	13.60000	.27224	462.4	1.182	.53120	14.10000	.41230	814.4	1.532	.86257	17.97328	.44086	
40	0	.000	.0975	447.8	0.963	.68600	13.50000	.28624	455.4	1.172	.52177	14.00000	.41222	816.9	1.532	.86257	17.97328	.44086	
41	0	.000	.1000	440.8	0.948	.68500	13.40000	.30064	448.4	1.162	.51235	13.90000	.41214	819.4	1.532	.86257	17.97328	.44086	
42	0	.000	.1025	433.8	0.933	.68400	13.30000	.31544	441.4	1.152	.50292	13.80000	.41206	821.9	1.532	.86257	17.97328	.44086	
43	0	.000	.1050	426.8	0.918	.68300	13.20000	.33064	434.4	1.142	.49350	13.70000	.41198	824.4	1.532	.86257	17.97328	.44086	
44	0	.000	.1075	419.8	0.903	.68200	13.10000	.34624	427.4	1.132	.48407	13.60000	.41190	826.9	1.532	.86257	17.97328	.44086	
45	0	.000	.1100	412.8	0.888	.68100	13.00000	.36224	420.4	1.122	.47465	13.50000	.41182	829.4	1.532	.86257	17.97328	.44086	
46	0	.000	.1125	405.8	0.873	.68000	12.90000	.37864	413.4	1.112	.46522	13.40000	.41174	831.9	1.532	.86257	17.97328	.44086	
47	0	.000	.1150	398.8	0.858	.67900	12.80000	.39544	406.4	1.102	.45580	13.30000	.41166	834.4	1.532	.86257	17.97328	.44086	
48	0	.000	.1175	391.8	0.843	.67800	12.70000	.41264	399.4	1.092	.44637	13.20000	.41158	836.9	1.532	.86257	17.97328	.44086	
49	0	.000	.1200	384.8	0.828	.67700	12.60000	.43024	392.4	1.082	.43695	13.10000	.41150	839.4	1.532	.86257	17.97328	.44086	
50	0	.000	.1225	377.8	0.813	.67600	12.50000	.44824	385.4	1.072	.42752	13.00000	.41142	841.9	1.532	.86257	17.97328	.44086	

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VII.- DATA^a FOR 160° CONE; $M_{\infty} = 3.95$ - Concluded

(e) $\alpha = 20^\circ$ - Concluded

Orifice θ , deg	s , in.	s/d	s/s^*	$\Phi = 67.5^\circ, P_t = 5762.6 \text{ psf}$					$\Phi = 90.0^\circ, P_t = 5762.6 \text{ psf}$					
				P_t , psf	C_p	$P_t/P_{t,2}$	M_t	$P_t/\rho a$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t	$P_t/\rho a$
1	0	0.000	-0.000	731.1	1.558	-87617	43871	730.9	1.558	-87593	43918	730.9	18.01194	43918
2	0	0.025	-0.0493	727.9	1.551	-87623	43871	724.1	1.551	-87626	43918	724.1	18.01194	43918
3	0	0.050	-0.0986	724.5	1.544	-87625	43871	720.5	1.544	-87634	43918	720.5	18.01194	43918
4	0	0.075	-0.1479	721.1	1.537	-87625	43871	717.1	1.537	-87642	43918	717.1	18.01194	43918
5	0	0.100	-0.1971	717.1	1.530	-87617	43871	713.1	1.530	-87650	43918	713.1	18.01194	43918
6	0	0.125	-0.2463	713.1	1.523	-87623	43871	709.1	1.523	-87658	43918	709.1	18.01194	43918
7	0	0.150	-0.2956	709.1	1.516	-87642	43871	705.1	1.516	-87666	43918	705.1	18.01194	43918
8	0	0.175	-0.3448	705.1	1.509	-87642	43871	701.1	1.509	-87674	43918	701.1	18.01194	43918
9	0	0.200	-0.3941	701.1	1.502	-87642	43871	697.1	1.502	-87682	43918	697.1	18.01194	43918
10	0	0.225	-0.4434	697.1	1.495	-87642	43871	693.1	1.495	-87690	43918	693.1	18.01194	43918
11	0	0.250	-0.4926	693.1	1.488	-87642	43871	689.1	1.488	-87698	43918	689.1	18.01194	43918
12	0	0.275	-0.5419	689.1	1.481	-87642	43871	685.1	1.481	-87706	43918	685.1	18.01194	43918
13	0	0.300	-0.5911	685.1	1.474	-87642	43871	681.1	1.474	-87714	43918	681.1	18.01194	43918
14	0	0.325	-0.6404	681.1	1.467	-87642	43871	677.1	1.467	-87722	43918	677.1	18.01194	43918
15	0	0.350	-0.6897	677.1	1.460	-87642	43871	673.1	1.460	-87730	43918	673.1	18.01194	43918
16	0	0.375	-0.7389	673.1	1.453	-87642	43871	669.1	1.453	-87738	43918	669.1	18.01194	43918
17	0	0.400	-0.7882	669.1	1.446	-87642	43871	665.1	1.446	-87746	43918	665.1	18.01194	43918
18	0	0.425	-0.8375	665.1	1.439	-87642	43871	661.1	1.439	-87754	43918	661.1	18.01194	43918
19	0	0.450	-0.8867	661.1	1.432	-87642	43871	657.1	1.432	-87762	43918	657.1	18.01194	43918
20	0	0.475	-0.9360	657.1	1.425	-87642	43871	653.1	1.425	-87770	43918	653.1	18.01194	43918
21	0	0.500	-0.9852	653.1	1.418	-87642	43871	649.1	1.418	-87778	43918	649.1	18.01194	43918
22	180	0.220	-0.025	757.5	1.618	-91350	43871	747.7	1.599	-89793	43918	747.7	16.11982	59388
23	180	0.210	-0.050	753.5	1.611	-91350	43871	743.7	1.592	-89801	43918	743.7	16.11982	59388
24	180	0.200	-0.075	749.5	1.604	-91350	43871	739.7	1.585	-89809	43918	739.7	16.11982	59388
25	180	0.190	-0.100	745.5	1.597	-91350	43871	735.7	1.578	-89817	43918	735.7	16.11982	59388
26	180	0.180	-0.125	741.5	1.590	-91350	43871	731.7	1.569	-89825	43918	731.7	16.11982	59388
27	180	0.170	-0.150	737.5	1.583	-91350	43871	727.7	1.560	-89833	43918	727.7	16.11982	59388
28	180	0.160	-0.175	733.5	1.576	-91350	43871	723.7	1.552	-89841	43918	723.7	16.11982	59388
29	180	0.150	-0.200	729.5	1.569	-91350	43871	719.7	1.545	-89849	43918	719.7	16.11982	59388
30	180	0.140	-0.225	725.5	1.562	-91350	43871	715.7	1.538	-89857	43918	715.7	16.11982	59388
31	180	0.130	-0.250	721.5	1.555	-91350	43871	711.7	1.531	-89865	43918	711.7	16.11982	59388
32	180	0.120	-0.275	717.5	1.548	-91350	43871	707.7	1.524	-89873	43918	707.7	16.11982	59388
33	180	0.110	-0.300	713.5	1.541	-91350	43871	703.7	1.517	-89881	43918	703.7	16.11982	59388
34	180	0.100	-0.325	709.5	1.534	-91350	43871	699.7	1.510	-89889	43918	699.7	16.11982	59388
35	180	0.090	-0.350	705.5	1.527	-91350	43871	695.7	1.503	-89897	43918	695.7	16.11982	59388
36	180	0.080	-0.375	701.5	1.520	-91350	43871	691.7	1.496	-89905	43918	691.7	16.11982	59388
37	180	0.070	-0.400	697.5	1.513	-91350	43871	687.7	1.489	-89913	43918	687.7	16.11982	59388
38	180	0.060	-0.425	693.5	1.506	-91350	43871	683.7	1.482	-89921	43918	683.7	16.11982	59388
39	180	0.050	-0.450	689.5	1.499	-91350	43871	679.7	1.475	-89929	43918	679.7	16.11982	59388
40	180	0.040	-0.475	685.5	1.492	-91350	43871	675.7	1.468	-89937	43918	675.7	16.11982	59388
41	180	0.030	-0.500	681.5	1.485	-91350	43871	671.7	1.461	-89945	43918	671.7	16.11982	59388
42	270	0.270	-0.025	821.4	1.762	-98436	43871	811.7	1.599	-88346	43918	811.7	18.01194	43918
43	270	0.260	-0.050	817.4	1.755	-98436	43871	807.7	1.592	-88354	43918	807.7	18.01194	43918
44	270	0.250	-0.075	813.4	1.748	-98436	43871	803.7	1.585	-88362	43918	803.7	18.01194	43918
45	270	0.240	-0.100	809.4	1.741	-98436	43871	799.7	1.578	-88370	43918	799.7	18.01194	43918
46	90	0.230	-0.125	805.4	1.734	-98436	43871	795.7	1.571	-88378	43918	795.7	18.01194	43918
47	90	0.220	-0.150	801.4	1.727	-98436	43871	791.7	1.564	-88386	43918	791.7	18.01194	43918
48	90	0.210	-0.175	797.4	1.720	-98436	43871	787.7	1.557	-88394	43918	787.7	18.01194	43918
49	90	0.200	-0.200	793.4	1.713	-98436	43871	783.7	1.550	-88402	43918	783.7	18.01194	43918

TABLE VIII.- DATA^a FOR 160° CONE; $M_\infty = 4.63$ (a) $\alpha = 0^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0.0^\circ, P_t = 7878.9 \text{ psf}$			
				P_t , psf	C_p	$P_t/P_{t,2}$	M_t
1	0	.000	.0000	634.4	1.757	.97510	.19014
2	0	.000	.0000	634.4	1.752	.97264	.19946
3	0	.000	.0000	631.2	1.748	.97019	.20839
4	0	.000	.0000	631.2	1.748	.97019	.20839
5	0	.000	.0000	631.2	1.748	.97019	.20839
6	0	.000	.0000	628.0	1.734	.96282	.23129
7	0	.000	.0000	628.0	1.734	.96282	.23129
8	0	.000	.0000	623.2	1.725	.95791	.24963
9	0	.000	.0000	623.2	1.725	.95791	.24963
10	0	.000	.0000	613.4	1.720	.95545	.25599
11	0	.000	.0000	613.4	1.720	.95545	.25599
12	0	.000	.0000	615.2	1.711	.95254	.26186
13	0	.000	.0000	615.2	1.711	.95254	.26186
14	0	.000	.0000	609.6	1.696	.94826	.28374
15	0	.000	.0000	609.6	1.696	.94826	.28374
16	0	.000	.0000	599.2	1.656	.92106	.32159
17	0	.000	.0000	599.2	1.656	.92106	.32159
18	0	.000	.0000	592.8	1.638	.91646	.34476
19	0	.000	.0000	592.8	1.638	.91646	.34476
20	0	.000	.0000	572.0	1.578	.88731	.39308
21	0	.000	.0000	572.0	1.578	.88731	.39308
22	0	.000	.0000	559.3	1.541	.85966	.43262
23	0	.000	.0000	559.3	1.541	.85966	.43262
24	0	.000	.0000	540.1	1.486	.83019	.46985
25	0	.000	.0000	540.1	1.486	.83019	.46985
26	0	.000	.0000	508.1	1.394	.79318	.52578
27	0	.000	.0000	508.1	1.394	.79318	.52578
28	0	.000	.0000	443.2	1.178	.68874	.72100
29	0	.000	.0000	443.2	1.178	.68874	.72100
30	0	.000	.0000	443.0	1.173	.68383	.72730
31	0	.000	.0000	438.4	1.169	.67816	.74060
32	0	.000	.0000	433.7	1.165	.67269	.75278
33	0	.000	.0000	433.7	1.165	.67269	.75278
34	0	.000	.0000	432.1	1.155	.66702	.76430
35	0	.000	.0000	430.5	1.150	.66156	.77430
36	0	.000	.0000	427.3	1.146	.65611	.78383
37	0	.000	.0000	427.3	1.146	.65611	.78383
38	0	.000	.0000	424.9	1.137	.65070	.79289
39	0	.000	.0000	424.9	1.137	.65070	.79289
40	0	.000	.0000	419.3	1.114	.64538	.80130
41	0	.000	.0000	419.3	1.114	.64538	.80130
42	0	.000	.0000	409.7	1.086	.63997	.80927
43	0	.000	.0000	409.7	1.086	.63997	.80927
44	0	.000	.0000	403.3	1.068	.63456	.81689
45	0	.000	.0000	403.3	1.068	.63456	.81689
46	0	.000	.0000	398.6	1.051	.62915	.82422
47	0	.000	.0000	398.6	1.051	.62915	.82422
48	0	.000	.0000	393.7	1.036	.62374	.83135
49	0	.000	.0000	393.7	1.036	.62374	.83135
50	0	.000	.0000	388.7	1.022	.61833	.83822
51	0	.000	.0000	388.7	1.022	.61833	.83822
52	0	.000	.0000	384.1	1.009	.61292	.84509
53	0	.000	.0000	384.1	1.009	.61292	.84509
54	0	.000	.0000	379.4	1.003	.60751	.85196
55	0	.000	.0000	379.4	1.003	.60751	.85196
56	0	.000	.0000	375.4	1.022	.60210	.85883
57	0	.000	.0000	375.4	1.022	.60210	.85883
58	0	.000	.0000	370.7	1.009	.59669	.86570
59	0	.000	.0000	370.7	1.009	.59669	.86570
60	0	.000	.0000	366.0	1.003	.59128	.87257
61	0	.000	.0000	366.0	1.003	.59128	.87257
62	0	.000	.0000	361.3	1.003	.58587	.87944
63	0	.000	.0000	361.3	1.003	.58587	.87944
64	0	.000	.0000	356.6	1.003	.58046	.88631
65	0	.000	.0000	356.6	1.003	.58046	.88631
66	0	.000	.0000	351.9	1.003	.57505	.89318
67	0	.000	.0000	351.9	1.003	.57505	.89318
68	0	.000	.0000	347.2	1.003	.56964	.90005
69	0	.000	.0000	347.2	1.003	.56964	.90005
70	0	.000	.0000	342.5	1.003	.56423	.90692
71	0	.000	.0000	342.5	1.003	.56423	.90692
72	0	.000	.0000	337.8	1.003	.55882	.91379
73	0	.000	.0000	337.8	1.003	.55882	.91379
74	0	.000	.0000	333.1	1.003	.55341	.92066
75	0	.000	.0000	333.1	1.003	.55341	.92066
76	0	.000	.0000	328.4	1.003	.54800	.92753
77	0	.000	.0000	328.4	1.003	.54800	.92753
78	0	.000	.0000	323.7	1.003	.54259	.93440
79	0	.000	.0000	323.7	1.003	.54259	.93440
80	0	.000	.0000	319.0	1.003	.53718	.94127
81	0	.000	.0000	319.0	1.003	.53718	.94127
82	0	.000	.0000	314.3	1.003	.53177	.94814
83	0	.000	.0000	314.3	1.003	.53177	.94814
84	0	.000	.0000	309.6	1.003	.52636	.95501
85	0	.000	.0000	309.6	1.003	.52636	.95501
86	0	.000	.0000	304.9	1.003	.52095	.96188
87	0	.000	.0000	304.9	1.003	.52095	.96188
88	0	.000	.0000	300.2	1.003	.51554	.96875
89	0	.000	.0000	300.2	1.003	.51554	.96875
90	0	.000	.0000	295.5	1.003	.51013	.97562
91	0	.000	.0000	295.5	1.003	.51013	.97562
92	0	.000	.0000	290.8	1.003	.50472	.98249
93	0	.000	.0000	290.8	1.003	.50472	.98249
94	0	.000	.0000	286.1	1.003	.49931	.98936
95	0	.000	.0000	286.1	1.003	.49931	.98936
96	0	.000	.0000	281.4	1.003	.49390	.99623
97	0	.000	.0000	281.4	1.003	.49390	.99623
98	0	.000	.0000	276.7	1.003	.48849	.10000
99	0	.000	.0000	276.7	1.003	.48849	.10000
100	0	.000	.0000	272.0	1.003	.48308	.10000

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VIII.- DATA^a FOR 160° CONE; $M_{\infty} = 4.63$ - Continued

(b) $\alpha = 5^\circ$

Orifice α , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ, p_t = 7878.9 \text{ psf}$				$\Phi = 22.5^\circ, p_t = 7878.9 \text{ psf}$				$\Phi = 45.0^\circ, p_t = 7878.9 \text{ psf}$						
				p_{t1} , psf	C_p	p_{t1}/p_{t2}	p_{t1}/p_{∞}	M_{t1}	p_{t1} , psf	C_p	p_{t1}/p_{t2}	p_{t1}/p_{∞}	M_{t1}	p_{t1} , psf	C_p	p_{t1}/p_{t2}	p_{t1}/p_{∞}	M_{t1}
1	0	-0.00	-0.000	631.2	1.744	.97019	27.22825	.20839	631.1	1.748	.97012	27.22635	.20863	629.7	1.744	.96800	27.16687	.21605
2	0	-0.20	-0.025	626.4	1.734	.96282	27.02145	.23229	626.3	1.734	.96275	27.01957	.23230	625.1	1.739	.96500	27.00992	.22437
3	0	-0.40	-0.050	624.2	1.725	.95791	26.83356	.25329	624.7	1.729	.96030	26.95064	.25327	624.5	1.735	.96309	26.96309	.22437
4	0	-0.60	-0.075	621.6	1.720	.95545	26.68165	.27599	619.9	1.721	.95784	26.88172	.27598	624.8	1.730	.96063	26.96061	.22402
5	0	-0.80	-0.100	618.4	1.711	.95054	26.47679	.29932	618.3	1.711	.95947	26.67493	.29936	621.8	1.721	.95572	26.82211	.22520
6	0	-1.00	-0.125	614.4	1.697	.94326	26.22533	.32355	614.3	1.697	.95410	26.46815	.32350	615.2	1.702	.95326	26.75316	.22620
7	0	-1.20	-0.150	610.4	1.688	.93819	26.13244	.34838	610.4	1.688	.93819	26.33030	.34838	612.2	1.703	.94097	26.84631	.22803
8	0	-1.40	-0.175	605.6	1.674	.93089	25.93088	.37368	605.6	1.688	.93819	26.33030	.37368	609.0	1.684	.93606	26.72050	.23089
9	0	-1.60	-0.200	602.4	1.655	.91598	25.57807	.39938	602.4	1.655	.91598	25.77888	.39938	604.2	1.670	.92869	26.58679	.23417
10	0	-1.80	-0.225	598.4	1.631	.89841	25.25287	.42562	598.4	1.631	.89841	25.57209	.42562	600.2	1.670	.92869	26.58679	.23417
11	0	-2.00	-0.250	594.4	1.601	.87813	24.95348	.45242	594.6	1.631	.90135	25.29638	.45242	596.6	1.624	.90412	26.42822	.23766
12	0	-2.20	-0.275	590.4	1.566	.85457	24.67775	.47972	590.4	1.611	.88447	25.07208	.47972	598.2	1.624	.90412	26.42822	.23766
13	0	-2.40	-0.300	586.4	1.526	.82792	24.42541	.50742	586.4	1.578	.84332	24.82638	.50742	594.6	1.611	.88447	26.27050	.24117
14	0	-2.60	-0.325	582.4	1.481	.79841	24.19616	.53552	582.4	1.548	.80732	24.58208	.53552	594.6	1.588	.86447	26.11728	.24467
15	0	-2.80	-0.350	578.4	1.431	.76592	23.98954	.56402	578.4	1.508	.77262	24.34768	.56402	594.6	1.566	.83447	25.96422	.24817
16	0	-3.00	-0.375	574.4	1.376	.73041	23.80241	.59292	574.4	1.478	.73762	24.12538	.59292	594.6	1.526	.80447	25.81077	.25167
17	0	-3.20	-0.400	570.4	1.316	.69192	23.63346	.62222	570.4	1.421	.73762	24.12538	.62222	594.6	1.466	.77447	25.65732	.25517
18	0	-3.40	-0.425	566.4	1.251	.65041	23.48141	.65202	566.4	1.350	.69462	23.88954	.65202	594.6	1.401	.73447	25.50387	.25867
19	0	-3.60	-0.450	562.4	1.181	.60592	23.34541	.68232	562.4	1.283	.65782	23.66808	.68232	594.6	1.326	.69447	25.35042	.26217
20	0	-3.80	-0.475	558.4	1.106	.55841	23.22441	.71322	558.4	1.211	.61322	23.45768	.71322	594.6	1.259	.65447	25.19697	.26567
21	0	-4.00	-0.500	554.4	1.026	.50792	23.11741	.74462	554.4	1.134	.56562	23.25638	.74462	594.6	1.194	.60447	25.04352	.26917
22	180	-0.00	-0.000	643.2	1.201	.67790	19.02531	.76640	641.0	1.201	.67790	19.02531	.76640	641.0	1.201	.67790	19.02531	.76640
23	180	-0.20	-0.025	641.6	1.178	.98628	27.68002	.12060	641.6	1.178	.98628	27.68002	.12060	641.6	1.178	.98628	27.68002	.12060
24	180	-0.40	-0.050	639.6	1.154	.98376	27.60002	.12360	639.6	1.154	.98376	27.60002	.12360	639.6	1.154	.98376	27.60002	.12360
25	180	-0.60	-0.075	637.6	1.130	.98124	27.53809	.12660	637.6	1.130	.98124	27.53809	.12660	637.6	1.130	.98124	27.53809	.12660
26	180	-0.80	-0.100	635.6	1.106	.97872	27.46684	.12960	635.6	1.106	.97872	27.46684	.12960	635.6	1.106	.97872	27.46684	.12960
27	180	-1.00	-0.125	633.6	1.082	.97620	27.39559	.13260	633.6	1.082	.97620	27.39559	.13260	633.6	1.082	.97620	27.39559	.13260
28	180	-1.20	-0.150	631.6	1.058	.97368	27.32434	.13560	631.6	1.058	.97368	27.32434	.13560	631.6	1.058	.97368	27.32434	.13560
29	180	-1.40	-0.175	629.6	1.034	.97116	27.25309	.13860	629.6	1.034	.97116	27.25309	.13860	629.6	1.034	.97116	27.25309	.13860
30	180	-1.60	-0.200	627.6	1.010	.96864	27.18184	.14160	627.6	1.010	.96864	27.18184	.14160	627.6	1.010	.96864	27.18184	.14160
31	180	-1.80	-0.225	625.6	0.986	.96612	27.11059	.14460	625.6	0.986	.96612	27.11059	.14460	625.6	0.986	.96612	27.11059	.14460
32	180	-2.00	-0.250	623.6	0.962	.96360	27.03934	.14760	623.6	0.962	.96360	27.03934	.14760	623.6	0.962	.96360	27.03934	.14760
33	180	-2.20	-0.275	621.6	0.938	.96108	26.96809	.15060	621.6	0.938	.96108	26.96809	.15060	621.6	0.938	.96108	26.96809	.15060
34	180	-2.40	-0.300	619.6	0.914	.95876	26.89684	.15360	619.6	0.914	.95876	26.89684	.15360	619.6	0.914	.95876	26.89684	.15360
35	180	-2.60	-0.325	617.6	0.890	.95652	26.82559	.15660	617.6	0.890	.95652	26.82559	.15660	617.6	0.890	.95652	26.82559	.15660
36	180	-2.80	-0.350	615.6	0.866	.95428	26.75434	.15960	615.6	0.866	.95428	26.75434	.15960	615.6	0.866	.95428	26.75434	.15960
37	180	-3.00	-0.375	613.6	0.842	.95204	26.68309	.16260	613.6	0.842	.95204	26.68309	.16260	613.6	0.842	.95204	26.68309	.16260
38	180	-3.20	-0.400	611.6	0.818	.94980	26.61184	.16560	611.6	0.818	.94980	26.61184	.16560	611.6	0.818	.94980	26.61184	.16560
39	180	-3.40	-0.425	609.6	0.794	.94756	26.54059	.16860	609.6	0.794	.94756	26.54059	.16860	609.6	0.794	.94756	26.54059	.16860
40	180	-3.60	-0.450	607.6	0.770	.94532	26.46934	.17160	607.6	0.770	.94532	26.46934	.17160	607.6	0.770	.94532	26.46934	.17160
41	180	-3.80	-0.475	605.6	0.746	.94308	26.39809	.17460	605.6	0.746	.94308	26.39809	.17460	605.6	0.746	.94308	26.39809	.17460
42	270	-0.00	-0.000	643.2	1.783	.98874	27.74887	.12060	641.6	1.778	.98622	27.67809	.12060	640.2	1.774	.98410	27.60834	.27967
43	270	-0.20	-0.025	641.6	1.778	.98628	27.68002	.12360	640.0	1.773	.98376	27.60924	.12360	638.6	1.769	.98165	27.53809	.28317
44	270	-0.40	-0.050	639.6	1.768	.98376	27.60002	.12660	638.0	1.768	.98124	27.53809	.12660	636.6	1.764	.97910	27.46684	.28667
45	270	-0.60	-0.075	637.6	1.758	.98124	27.53809	.12960	636.0	1.758	.97872	27.46684	.12960	634.6	1.759	.97697	27.39559	.29017
46	270	-0.80	-0.100	635.6	1.748	.97872	27.46684	.13260	634.0	1.748	.97620	27.39559	.13260	632.6	1.744	.97445	27.32434	.29367
47	270	-1.00	-0.125	633.6	1.738	.97620	27.39559	.13560	632.0	1.738	.97368	27.32434	.13560	630.6	1.739	.97220	27.25309	.29717
48	270	-1.20	-0.150	631.6	1.728	.97368	27.32434	.13860	630.0	1.728	.97116	27.25309	.13860	628.6	1.730	.96997	27.18184	.30067
49	270	-1.40	-0.175	629.6	1.718	.97116	27.25309	.14160	628.0	1.718	.96864	27.18184	.14160	626.6	1.721	.96772	27.11059	.30417
50	270	-1.60	-0.200	627.6	1.708	.96864	27.18184	.14460	626.0	1.708	.96612	27.11059	.14460	624.6	1.712	.96584	27.03934	.30767

a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VIII.- DATA^a FOR 160° CONE; $M_{\infty} = 4.63$ - Continued(b) $\alpha = 5^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ$, $p_t = 7878.9$ psf				$\phi = 90.0^\circ$, $p_t = 7878.9$ psf					
				p_{t1} psf	C_p	p_{t1}/p_{t2}	p_{t1}/p_{∞}	M_{t1}	p_{t1} psf	C_p	p_{t1}/p_{t2}	p_{t1}/p_{∞}	M_{t1}
1	0	.000	.0000	630.3	1.745	.98687	27.19142	.21302	631.2	1.748	.97019	27.22825	.20839
2	0	.025	.0493	628.7	1.741	.98642	27.12240	.22145	629.6	1.743	.96773	27.15931	.21698
3	0	.050	.0985	627.1	1.736	.98636	27.05339	.22960	628.0	1.743	.95927	27.09038	.22527
4	0	.075	.1478	625.4	1.731	.98604	26.98436	.23763	626.4	1.734	.95082	27.02145	.23372
5	0	.100	.1963	623.3	1.727	.98568	26.91536	.24517	624.0	1.725	.95191	26.95232	.24203
6	0	.125	.2436	621.5	1.722	.98528	26.84635	.25263	621.6	1.720	.94364	26.88369	.25028
7	0	.150	.2896	617.5	1.709	.98420	26.77734	.26009	618.2	1.712	.93535	26.81465	.25858
8	0	.175	.3348	615.9	1.704	.98346	26.70832	.26755	615.2	1.702	.92704	26.74561	.26683
9	0	.200	.3791	612.9	1.693	.98268	26.63931	.27501	612.0	1.693	.92063	26.67679	.27508
10	0	.225	.4226	609.1	1.683	.98183	26.57029	.28247	608.8	1.684	.91421	26.60786	.28314
11	0	.250	.4653	607.9	1.681	.98127	26.50128	.28993	608.8	1.684	.90760	26.53892	.29120
12	0	.275	.5072	604.6	1.658	.97970	26.43226	.29739	604.0	1.670	.90104	26.47000	.29926
13	0	.300	.5491	593.5	1.640	.97815	26.36324	.30485	598.4	1.670	.89443	26.40118	.30732
14	0	.325	.5912	587.1	1.621	.97660	26.29422	.31231	590.4	1.662	.88782	26.33231	.31538
15	0	.350	.6325	580.5	1.603	.97505	26.22520	.31977	583.0	1.654	.88120	26.26340	.32344
16	0	.375	.6739	572.7	1.586	.97350	26.15618	.32723	584.1	1.646	.87459	26.19448	.33150
17	0	.400	.7154	564.1	1.568	.97195	26.08716	.33469	581.8	1.638	.86797	26.12553	.33956
18	0	.425	.7569	551.5	1.551	.97040	26.01814	.34215	579.6	1.630	.86136	26.05660	.34762
19	0	.450	.7984	547.1	1.534	.96885	25.94912	.34961	576.9	1.622	.85475	25.98768	.35568
20	0	.475	.8399	542.9	1.517	.96730	25.88010	.35707	574.9	1.614	.84814	25.91876	.36374
21	0	.500	.8814	538.9	1.500	.96575	25.81108	.36453	572.8	1.606	.84153	25.84984	.37180
22	0	.525	.9229	535.1	1.483	.96420	25.74206	.37199	570.6	1.598	.83492	25.78092	.37986
23	0	.550	.9644	531.1	1.466	.96265	25.67304	.37945	568.4	1.590	.82831	25.71200	.38792
24	0	.575	1.0059	527.1	1.449	.96110	25.60402	.38691	566.2	1.582	.82170	25.64308	.39598
25	0	.600	1.0474	523.1	1.432	.95955	25.53500	.39437	564.0	1.574	.81509	25.57416	.40404
26	0	.625	1.0889	519.1	1.415	.95800	25.46600	.40183	561.8	1.566	.80848	25.50524	.41210
27	0	.650	1.1304	515.1	1.398	.95645	25.39700	.40929	559.6	1.558	.80187	25.43632	.42016
28	0	.675	1.1719	511.1	1.381	.95490	25.32800	.41675	557.4	1.550	.79526	25.36740	.42822
29	0	.700	1.2134	507.1	1.364	.95335	25.25900	.42421	555.2	1.542	.78865	25.29848	.43628
30	0	.725	1.2549	503.1	1.347	.95180	25.19000	.43167	553.0	1.534	.78204	25.22956	.44434
31	0	.750	1.2964	500.0	1.330	.95025	25.12100	.43913	550.8	1.526	.77543	25.16064	.45240
32	0	.775	1.3379	496.0	1.313	.94870	25.05200	.44659	548.6	1.518	.76882	25.09172	.46046
33	0	.800	1.3794	492.0	1.296	.94715	24.98300	.45405	546.4	1.510	.76221	25.02280	.46852
34	0	.825	1.4209	488.0	1.279	.94560	24.91400	.46151	544.2	1.502	.75560	24.95388	.47658
35	0	.850	1.4624	484.0	1.262	.94405	24.84500	.46897	542.0	1.494	.74899	24.88496	.48464
36	0	.875	1.5039	480.0	1.245	.94250	24.77600	.47643	539.8	1.486	.74238	24.81604	.49270
37	0	.900	1.5454	476.0	1.228	.94095	24.70700	.48389	537.6	1.478	.73577	24.74712	.50076
38	0	.925	1.5869	472.0	1.211	.93940	24.63800	.49135	535.4	1.470	.72916	24.67820	.50882
39	0	.950	1.6284	468.0	1.194	.93785	24.56900	.49881	533.2	1.462	.72255	24.60928	.51688
40	0	.975	1.6699	464.0	1.177	.93630	24.50000	.50627	531.0	1.454	.71594	24.54036	.52494
41	0	1.000	1.7114	460.0	1.160	.93475	24.43100	.51373	528.8	1.446	.70933	24.47144	.53300
42	0	1.025	1.7529	456.0	1.143	.93320	24.36200	.52119	526.6	1.438	.70272	24.40252	.54106
43	0	1.050	1.7944	452.0	1.126	.93165	24.29300	.52865	524.4	1.430	.69611	24.33360	.54912
44	0	1.075	1.8359	448.0	1.109	.93010	24.22400	.53611	522.2	1.422	.68950	24.26468	.55718
45	0	1.100	1.8774	444.0	1.092	.92855	24.15500	.54357	520.0	1.414	.68289	24.19576	.56524
46	0	1.125	1.9189	440.0	1.075	.92700	24.08600	.55103	517.8	1.406	.67628	24.12684	.57330
47	0	1.150	1.9604	436.0	1.058	.92545	24.01700	.55849	515.6	1.398	.66967	24.05792	.58136
48	0	1.175	2.0019	432.0	1.041	.92390	23.94800	.56595	513.4	1.390	.66306	23.98900	.58942
49	0	1.200	2.0434	428.0	1.024	.92235	23.87900	.57341	511.2	1.382	.65645	23.92008	.59748
50	0	1.225	2.0849	424.0	1.007	.92080	23.81000	.58087	509.0	1.374	.64984	23.85116	.60554
51	0	1.250	2.1264	420.0	0.990	.91925	23.74100	.58829	506.8	1.366	.64323	23.78224	.61360
52	0	1.275	2.1679	416.0	0.973	.91770	23.67200	.59571	504.6	1.358	.63662	23.71332	.62166
53	0	1.300	2.2094	412.0	0.956	.91615	23.60300	.60313	502.4	1.350	.63001	23.64440	.62972
54	0	1.325	2.2509	408.0	0.939	.91460	23.53400	.61055	500.2	1.342	.62340	23.57548	.63778
55	0	1.350	2.2924	404.0	0.922	.91305	23.46500	.61797	498.0	1.334	.61679	23.50656	.64584
56	0	1.375	2.3339	400.0	0.905	.91150	23.39600	.62539	495.8	1.326	.61018	23.43764	.65390
57	0	1.400	2.3754	396.0	0.888	.90995	23.32700	.63281	493.6	1.318	.60357	23.36872	.66196
58	0	1.425	2.4169	392.0	0.871	.90840	23.25800	.64023	491.4	1.310	.59696	23.29980	.67002
59	0	1.450	2.4584	388.0	0.854	.90685	23.18900	.64765	489.2	1.302	.59035	23.23088	.67808
60	0	1.475	2.4999	384.0	0.837	.90530	23.12000	.65507	487.0	1.294	.58374	23.16196	.68614
61	0	1.500	2.5414	380.0	0.820	.90375	23.05100	.66249	484.8	1.286	.57713	23.09304	.69420
62	0	1.525	2.5829	376.0	0.803	.90220	22.98200	.66991	482.6	1.278	.57052	23.02412	.70226
63	0	1.550	2.6244	372.0	0.786	.90065	22.91300	.67733	480.4	1.270	.56391	22.95520	.71032
64	0	1.575	2.6659	368.0	0.769	.89910	22.84400	.68475	478.2	1.262	.55730	22.88628	.71838
65	0	1.600	2.7074	364.0	0.752	.89755	22.77500	.69217	476.0	1.254	.55069	22.81736	.72644
66	0	1.625	2.7489	360.0	0.735	.89600	22.70600	.69959	473.8	1.246	.54408	22.74844	.73450
67	0	1.650	2.7904	356.0	0.718	.89445	22.63700	.70701	471.6	1.238	.53747	22.67952	.74256
68	0	1.675	2.8319	352.0	0.701	.89290	22.56800	.71443	469.4	1.230	.53086	22.61060	.75062
69	0	1.700	2.8734	348.0	0.684	.89135	22.49900	.72185	467.2	1.222	.52425	22.54168	.75868
70	0	1.725	2.9149	344.0	0.667	.88980	22.43000	.72927	465.0	1.214	.51764	22.47276	.76674
71	0	1.750	2.9564	340.0	0.650	.88825	22.36100	.73669	462.8	1.206	.51103	22.40384	.77480
72	0	1.775	2.9979	336.0	0.633	.88670	22.29200	.74411	460.6	1.198	.50442	22.33492	.78286
73	0	1.800	3.0394	332.0	0.616	.88515	22.22300	.75153	458.4	1.190	.49781	22.26600	.79092
74	0	1.825	3.0809	328.0	0.599	.88360	22.15400	.75895	456.2	1.182	.49120	22.19708	.79898
75	0	1.850	3.1224	324.0	0.582	.88205	22.08500	.76637	454.0	1.174	.48459	22.12816	.80704
76	0	1.875	3.1639	320.0	0.565	.88050	22.01600	.77379	451.8	1.166	.47798	22.05924	.81510
77	0	1.900	3.2054	316.0	0.548	.87895	21.94700	.78121	449.6	1.158	.47137	21.99032	.82316
78	0	1.925	3.2469	312.0	0.531	.87740	21.87800	.78863	447.4	1.150	.46476	21.92140	.83122
79	0	1.950	3.2884	308.0	0.514	.87585	21.80900	.79605	445.2	1.142	.45815	21.85248	.83928
80	0	1.975	3.3299	304.0	0.497	.87430	21.74000	.80347	443.0	1.134	.45154	21.78356	.84734
81	0	2.000	3.3714	300.0	0.480	.87275	21.67100	.81089	440.8	1.126	.44493	21.71464	.85540
82	0	2.025	3.4129	296.0	0.463	.87120	21.60200	.81831	438.6	1.118	.43832	21.64572	.86346
83	0	2.050	3.4544	292.0	0.446	.86965	21.53300	.82573	436.4	1.110	.43171	21.57680	.87152
84	0	2.075	3.4959	288.0	0.429	.86810	21.46400	.83315	434.2	1.102	.42510	21.50788	.87958
85	0	2.100	3.5374	284.0	0.412	.86655	21.39500	.84057	432.0	1.094	.41849	21.43896	.88764

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VIII.- DATA^a FOR 160° CONE; $M_{\infty} = 4.63$ - Continued(c) $\alpha = 10^\circ$

Orifice e, deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, p_t = 7878.9 \text{ psf}$					$\phi = 22.5^\circ, p_t = 7878.9 \text{ psf}$					$\phi = 45.0^\circ, p_t = 7878.9 \text{ psf}$				
				$p_{t, \text{ psf}}$	C_p	$p_t/p_{t,2}$	$p_t/\rho_{t,0}$	M_t	$p_{t, \text{ psf}}$	C_p	$p_t/p_{t,2}$	$p_t/\rho_{t,0}$	M_t	$p_{t, \text{ psf}}$	C_p	$p_t/p_{t,2}$	$p_t/\rho_{t,0}$	M_t
1	0	.000	.0000	615.4	1.703	.94502	26.55000	28.268	615.2	1.702	.94569	26.56077	.28357	615.4	1.703	.94595	26.56485	.28285
2	0	.025	.0043	639.0	1.684	.93519	26.50036	1.684	1.684	1.684	.93587	26.50036	.30918	610.6	1.689	.93858	26.54128	.30228
3	0	.050	.0086	659.0	1.667	.92682	26.46277	1.667	1.667	1.667	.92750	26.46277	.33728	607.4	1.695	.94127	26.53167	.31697
4	0	.075	.0129	680.3	1.651	.92031	26.43816	1.651	1.651	1.651	.92358	25.92034	.33491	604.2	1.670	.92876	26.50566	.33266
5	0	.100	.0171	701.1	1.636	.91489	25.41953	1.636	1.636	1.636	.91867	25.78246	.35023	592.7	1.661	.92384	25.92592	.33531
6	0	.125	.0213	723.9	1.621	.91062	25.58454	1.621	1.621	1.621	.91532	25.66459	.36127	586.2	1.647	.91647	25.92068	.33821
7	0	.150	.0256	749.1	1.606	.90738	25.73716	1.606	1.606	1.606	.91209	25.43778	.37736	581.7	1.634	.91156	25.92766	.34613
8	0	.175	.0299	776.4	1.591	.90463	25.87922	1.591	1.591	1.591	.90939	25.43778	.39089	576.0	1.621	.90761	25.93466	.35405
9	0	.200	.0342	805.3	1.576	.90233	26.01285	1.576	1.576	1.576	.90715	25.43778	.40309	570.3	1.608	.90527	25.94169	.36197
10	0	.225	.0384	836.3	1.562	.90048	26.13927	1.562	1.562	1.562	.90530	25.43778	.41489	564.6	1.595	.90338	25.94872	.36990
11	0	.250	.0426	868.4	1.548	.89909	26.25957	1.548	1.548	1.548	.89388	25.43778	.42625	558.9	1.582	.89277	25.95575	.37782
12	0	.275	.0467	901.9	1.535	.89813	26.37417	1.535	1.535	1.535	.89317	24.61053	.43727	553.2	1.569	.89233	25.96278	.38574
13	0	.300	.0508	936.7	1.522	.89763	26.48324	1.522	1.522	1.522	.89267	24.61053	.44790	547.5	1.556	.89199	25.96981	.39366
14	0	.325	.0549	972.9	1.509	.89758	26.58707	1.509	1.509	1.509	.89252	23.64541	.45822	541.8	1.543	.89189	25.97684	.40158
15	0	.350	.0589	1010.5	1.505	.89761	26.68618	1.505	1.505	1.505	.89259	23.64541	.46815	536.1	1.530	.89199	25.98387	.40950
16	0	.375	.0628	1049.6	1.499	.89842	26.78093	1.499	1.499	1.499	.89279	23.23179	.47761	530.4	1.517	.89265	25.99090	.41742
17	0	.400	.0667	1090.1	1.494	.89942	26.87184	1.494	1.494	1.494	.89305	22.74923	.48668	524.7	1.504	.89345	25.99793	.42534
18	0	.425	.0705	1131.9	1.489	.90064	26.95867	1.489	1.489	1.489	.89343	22.27423	.49536	519.0	1.491	.89436	26.00496	.43326
19	0	.450	.0743	1175.0	1.484	.90207	27.04199	1.484	1.484	1.484	.89391	21.80809	.50368	513.3	1.478	.89538	26.01199	.44118
20	0	.475	.0780	1219.4	1.479	.90361	27.12136	1.479	1.479	1.479	.89445	21.35174	.51163	507.6	1.465	.89642	26.01899	.44910
21	0	.500	.0815	1265.1	1.474	.90526	27.19749	1.474	1.474	1.474	.89504	20.90509	.51921	501.9	1.452	.89750	26.02592	.45702
22	0	.525	.0849	1312.1	1.469	.90699	27.27012	1.469	1.469	1.469	.89568	18.46932	.52646	496.2	1.439	.89864	26.03285	.46494
23	0	.550	.0882	1360.3	1.464	.90879	27.33912	1.464	1.464	1.464	.89637	18.04282	.53332	490.5	1.426	.89980	26.03978	.47286
24	0	.575	.0915	1409.6	1.459	.91064	27.40436	1.459	1.459	1.459	.89710	17.62726	.54000	484.8	1.413	.90100	26.04670	.48078
25	0	.600	.0947	1460.1	1.454	.91254	27.46574	1.454	1.454	1.454	.89787	17.22266	.54650	479.1	1.400	.90222	26.05362	.48870
26	0	.625	.0978	1511.7	1.449	.91448	27.52324	1.449	1.449	1.449	.89868	16.82904	.55284	473.4	1.387	.90345	26.06054	.49662
27	0	.650	.1008	1564.4	1.444	.91646	27.57684	1.444	1.444	1.444	.89951	16.44542	.55904	467.7	1.374	.90469	26.06746	.50454
28	0	.675	.1037	1618.2	1.439	.91848	27.62654	1.439	1.439	1.439	.89995	16.07180	.56514	462.0	1.361	.90593	26.07438	.51246
29	0	.700	.1065	1673.1	1.434	.92053	27.67234	1.434	1.434	1.434	.90040	15.70818	.57114	456.3	1.348	.90717	26.08130	.52038
30	0	.725	.1093	1729.1	1.429	.92261	27.71424	1.429	1.429	1.429	.90086	15.35456	.57704	450.6	1.335	.90841	26.08822	.52830
31	0	.750	.1120	1786.1	1.424	.92471	27.75224	1.424	1.424	1.424	.90133	15.01094	.58284	444.9	1.322	.90965	26.09514	.53622
32	0	.775	.1146	1844.1	1.419	.92683	27.78634	1.419	1.419	1.419	.90180	14.67732	.58864	439.2	1.309	.91089	26.10206	.54414
33	0	.800	.1171	1903.1	1.414	.92897	27.81654	1.414	1.414	1.414	.90227	14.35370	.59434	433.5	1.296	.91213	26.10898	.55206
34	0	.825	.1195	1963.1	1.409	.93113	27.84284	1.409	1.409	1.409	.90274	14.04008	.60004	427.8	1.283	.91337	26.11590	.56000
35	0	.850	.1218	2024.1	1.404	.93330	27.86524	1.404	1.404	1.404	.90321	13.73646	.60574	422.1	1.270	.91461	26.12282	.56792
36	0	.875	.1241	2086.1	1.400	.93548	27.88374	1.400	1.400	1.400	.90368	13.44284	.61144	416.4	1.257	.91585	26.12974	.57584
37	0	.900	.1263	2149.1	1.395	.93767	27.89834	1.395	1.395	1.395	.90415	13.15922	.61714	410.7	1.244	.91709	26.13666	.58376
38	0	.925	.1284	2213.1	1.390	.93987	27.90904	1.390	1.390	1.390	.90462	12.88560	.62284	405.0	1.231	.91833	26.14358	.59168
39	0	.950	.1305	2278.1	1.385	.94207	27.91584	1.385	1.385	1.385	.90509	12.62200	.62854	400.0	1.218	.91957	26.15050	.60000
40	0	.975	.1325	2344.1	1.380	.94427	27.91874	1.380	1.380	1.380	.90556	12.36838	.63424	395.0	1.205	.92081	26.15742	.60832
41	0	1.000	.1345	2411.1	1.375	.94647	27.91774	1.375	1.375	1.375	.90603	12.12476	.64004	390.0	1.192	.92205	26.16434	.61664
42	0	1.025	.1364	2479.1	1.370	.94867	27.91284	1.370	1.370	1.370	.90650	11.89114	.64584	385.0	1.179	.92329	26.17126	.62500
43	0	1.050	.1382	2548.1	1.365	.95087	27.90404	1.365	1.365	1.365	.90697	11.66752	.65164	380.0	1.166	.92453	26.17818	.63332
44	0	1.075	.1400	2618.1	1.360	.95307	27.89134	1.360	1.360	1.360	.90744	11.45390	.65744	375.0	1.153	.92577	26.18510	.64164
45	0	1.100	.1417	2689.1	1.355	.95527	27.87474	1.355	1.355	1.355	.90791	11.25028	.66324	370.0	1.140	.92699	26.19202	.65000
46	0	1.125	.1434	2761.1	1.350	.95747	27.85424	1.350	1.350	1.350	.90838	11.05666	.66904	365.0	1.127	.92821	26.19894	.65832
47	0	1.150	.1450	2834.1	1.345	.95967	27.82984	1.345	1.345	1.345	.90885	10.87304	.67484	360.0	1.114	.92943	26.20586	.66664
48	0	1.175	.1466	2908.1	1.340	.96187	27.79954	1.340	1.340	1.340	.90932	10.69942	.68064	355.0	1.101	.93065	26.21278	.67500
49	0	1.200	.1481	2983.1	1.335	.96407	27.76424	1.335	1.335	1.335	.90979	10.53580	.68644	350.0	1.088	.93187	26.21970	.68332
50	0	1.225	.1496	3059.1	1.330	.96627	27.72394	1.330	1.330	1.330	.91026	10.38218	.69224	345.0	1.075	.93309	26.22662	.69164

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VIII.- DATA^a FOR 160° CONE; $M_{\infty} = 4.63$ - Continued(c) $\alpha = 10^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ$, $P_t = 7869.4$ psf				$\phi = 90.0^\circ$, $P_t = 7878.9$ psf					
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,0}$	M_L	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,0}$	M_L
1	0	0.000	-0.000	614.4	1.702	94555	26.53693	-28394	615.8	1.704	94655	26.56475	-28125
2	0	0.000	-0.000	611.2	1.693	94053	26.39871	-29699	612.8	1.699	94409	26.47878	-28788
3	0	0.000	-0.000	608.0	1.684	93551	26.26050	-30959	614.6	1.699	94409	26.47878	-28788
4	0	0.000	-0.000	604.8	1.674	93049	26.12229	-32176	616.4	1.699	94409	26.47878	-28788
5	0	0.000	-0.000	601.6	1.664	92547	25.98408	-33393	618.2	1.699	94409	26.47878	-28788
6	0	0.000	-0.000	598.4	1.654	92045	25.84587	-34610	620.0	1.699	94409	26.47878	-28788
7	0	0.000	-0.000	595.2	1.644	91543	25.70766	-35827	621.8	1.699	94409	26.47878	-28788
8	0	0.000	-0.000	592.0	1.634	91041	25.56945	-37044	623.6	1.699	94409	26.47878	-28788
9	0	0.000	-0.000	588.8	1.624	90539	25.43124	-38261	625.4	1.699	94409	26.47878	-28788
10	0	0.000	-0.000	585.6	1.614	90037	25.29303	-39478	627.2	1.699	94409	26.47878	-28788
11	0	0.000	-0.000	582.4	1.604	89535	25.15482	-40695	629.0	1.699	94409	26.47878	-28788
12	0	0.000	-0.000	579.2	1.594	89033	25.01661	-41912	630.8	1.699	94409	26.47878	-28788
13	0	0.000	-0.000	576.0	1.584	88531	24.87840	-43129	632.6	1.699	94409	26.47878	-28788
14	0	0.000	-0.000	572.8	1.574	88029	24.74019	-44346	634.4	1.699	94409	26.47878	-28788
15	0	0.000	-0.000	569.6	1.564	87527	24.60198	-45563	636.2	1.699	94409	26.47878	-28788
16	0	0.000	-0.000	566.4	1.554	87025	24.46377	-46780	638.0	1.699	94409	26.47878	-28788
17	0	0.000	-0.000	563.2	1.544	86523	24.32556	-47997	639.8	1.699	94409	26.47878	-28788
18	0	0.000	-0.000	560.0	1.534	86021	24.18735	-49214	641.6	1.699	94409	26.47878	-28788
19	0	0.000	-0.000	556.8	1.524	85519	24.04914	-50431	643.4	1.699	94409	26.47878	-28788
20	0	0.000	-0.000	553.6	1.514	85017	23.91093	-51648	645.2	1.699	94409	26.47878	-28788
21	0	0.000	-0.000	550.4	1.504	84515	23.77272	-52865	647.0	1.699	94409	26.47878	-28788
22	0	0.000	-0.000	547.2	1.494	84013	23.63451	-54082	648.8	1.699	94409	26.47878	-28788
23	0	0.000	-0.000	544.0	1.484	83511	23.49630	-55299	650.6	1.699	94409	26.47878	-28788
24	0	0.000	-0.000	540.8	1.474	83009	23.35809	-56516	652.4	1.699	94409	26.47878	-28788
25	0	0.000	-0.000	537.6	1.464	82507	23.21988	-57733	654.2	1.699	94409	26.47878	-28788
26	0	0.000	-0.000	534.4	1.454	82005	23.08167	-58950	656.0	1.699	94409	26.47878	-28788
27	0	0.000	-0.000	531.2	1.444	81503	22.94346	-60167	657.8	1.699	94409	26.47878	-28788
28	0	0.000	-0.000	528.0	1.434	81001	22.80525	-61384	659.6	1.699	94409	26.47878	-28788
29	0	0.000	-0.000	524.8	1.424	80499	22.66704	-62601	661.4	1.699	94409	26.47878	-28788
30	0	0.000	-0.000	521.6	1.414	80000	22.52883	-63818	663.2	1.699	94409	26.47878	-28788
31	0	0.000	-0.000	518.4	1.404	79497	22.39062	-65035	665.0	1.699	94409	26.47878	-28788
32	0	0.000	-0.000	515.2	1.394	79000	22.25241	-66252	666.8	1.699	94409	26.47878	-28788
33	0	0.000	-0.000	512.0	1.384	78497	22.11420	-67469	668.6	1.699	94409	26.47878	-28788
34	0	0.000	-0.000	508.8	1.374	78000	21.97599	-68686	670.4	1.699	94409	26.47878	-28788
35	0	0.000	-0.000	505.6	1.364	77497	21.83778	-69903	672.2	1.699	94409	26.47878	-28788
36	0	0.000	-0.000	502.4	1.354	77000	21.69957	-71120	674.0	1.699	94409	26.47878	-28788
37	0	0.000	-0.000	499.2	1.344	76497	21.56136	-72337	675.8	1.699	94409	26.47878	-28788
38	0	0.000	-0.000	496.0	1.334	76000	21.42315	-73554	677.6	1.699	94409	26.47878	-28788
39	0	0.000	-0.000	492.8	1.324	75497	21.28494	-74771	679.4	1.699	94409	26.47878	-28788
40	0	0.000	-0.000	489.6	1.314	75000	21.14673	-75988	681.2	1.699	94409	26.47878	-28788
41	0	0.000	-0.000	486.4	1.304	74497	21.00852	-77205	683.0	1.699	94409	26.47878	-28788
42	0	0.000	-0.000	483.2	1.294	74000	20.87031	-78422	684.8	1.699	94409	26.47878	-28788
43	0	0.000	-0.000	480.0	1.284	73497	20.73210	-79639	686.6	1.699	94409	26.47878	-28788
44	0	0.000	-0.000	476.8	1.274	73000	20.59389	-80856	688.4	1.699	94409	26.47878	-28788
45	0	0.000	-0.000	473.6	1.264	72497	20.45568	-82073	690.2	1.699	94409	26.47878	-28788
46	0	0.000	-0.000	470.4	1.254	72000	20.31747	-83290	692.0	1.699	94409	26.47878	-28788
47	0	0.000	-0.000	467.2	1.244	71497	20.17926	-84507	693.8	1.699	94409	26.47878	-28788
48	0	0.000	-0.000	464.0	1.234	71000	20.04105	-85724	695.6	1.699	94409	26.47878	-28788
49	0	0.000	-0.000	460.8	1.224	70497	19.90284	-86941	697.4	1.699	94409	26.47878	-28788

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VIII.- DATA^a FOR 160° CONE; $M_{\infty} = 4.63$ - Continued

(d) $\alpha = 15^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0, 0^\circ, \text{pt} = 7869.4 \text{ psf}$				
				P_t , psf	C_p	$P_t/P_{t,2}$	P_t/P_{∞}	M_t
1	0	.300	.0000	587.7	1.631	.90755	25.77022	.37487
2	0	.400	.0025	581.7	1.608	.89525	25.12510	.40075
3	0	.500	.0050	575.7	1.585	.88300	24.48000	.42662
4	0	.600	.0075	569.5	1.562	.87075	23.83490	.45247
5	0	.700	.0100	563.3	1.539	.85850	23.19000	.47832
6	0	.800	.0125	557.1	1.516	.84625	22.54510	.50417
7	0	.900	.0150	550.9	1.493	.83400	21.90020	.53002
8	0	1.000	.0175	544.7	1.470	.82175	21.25530	.55587
9	0	1.100	.0200	538.5	1.447	.80950	20.61040	.58172
10	0	1.200	.0225	532.3	1.424	.79725	19.96550	.60757
11	0	1.300	.0250	526.1	1.401	.78500	19.32060	.63342
12	0	1.400	.0275	519.9	1.378	.77275	18.67570	.65927
13	0	1.500	.0300	513.7	1.355	.76050	18.03080	.68512
14	0	1.600	.0325	507.5	1.332	.74825	17.38590	.71097
15	0	1.700	.0350	501.3	1.309	.73600	16.74100	.73682
16	0	1.800	.0375	495.1	1.286	.72375	16.09610	.76267
17	0	1.900	.0400	488.9	1.263	.71150	15.45120	.78852
18	0	2.000	.0425	482.7	1.240	.69925	14.80630	.81437
19	0	2.100	.0450	476.5	1.217	.68700	14.16140	.84022
20	0	2.200	.0475	470.3	1.194	.67475	13.51650	.86607
21	0	2.300	.0500	464.1	1.171	.66250	12.87160	.89192
22	0	2.400	.0525	457.9	1.148	.65025	12.22670	.91777
23	0	2.500	.0550	451.7	1.125	.63800	11.58180	.94362
24	0	2.600	.0575	445.5	1.102	.62575	10.93690	.96947
25	0	2.700	.0600	439.3	1.079	.61350	10.29200	.99532
26	0	2.800	.0625	433.1	1.056	.60125	9.64710	1.02117
27	0	2.900	.0650	426.9	1.033	.58900	9.00220	1.04702
28	0	3.000	.0675	420.7	1.010	.57675	8.35730	1.07287
29	0	3.100	.0700	414.5	.987	.56450	7.71240	1.09872
30	0	3.200	.0725	408.3	.964	.55225	7.06750	1.12457
31	0	3.300	.0750	402.1	.941	.54000	6.42260	1.15042
32	0	3.400	.0775	395.9	.918	.52775	5.77770	1.17627
33	0	3.500	.0800	389.7	.895	.51550	5.13280	1.20212
34	0	3.600	.0825	383.5	.872	.50325	4.48790	1.22797
35	0	3.700	.0850	377.3	.849	.49100	3.84300	1.25382
36	0	3.800	.0875	371.1	.826	.47875	3.19810	1.27967
37	0	3.900	.0900	364.9	.803	.46650	2.55320	1.30552
38	0	4.000	.0925	358.7	.780	.45425	1.90830	1.33137
39	0	4.100	.0950	352.5	.757	.44200	1.26340	1.35722
40	0	4.200	.0975	346.3	.734	.42975	.61850	1.38307
41	0	4.300	.1000	340.1	.711	.41750	.0	1.40892
42	0	4.400	.1025	333.9	.688	.40525	.0	1.43477
43	0	4.500	.1050	327.7	.665	.39300	.0	1.46062
44	0	4.600	.1075	321.5	.642	.38075	.0	1.48647
45	0	4.700	.1100	315.3	.619	.36850	.0	1.51232
46	0	4.800	.1125	309.1	.596	.35625	.0	1.53817
47	0	4.900	.1150	302.9	.573	.34400	.0	1.56402
48	0	5.000	.1175	296.7	.550	.33175	.0	1.58987
49	0	5.100	.1200	290.5	.527	.31950	.0	1.61572
50	0	5.200	.1225	284.3	.504	.30725	.0	1.64157

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VIII.- DATA^a FOR 160° CONE; $M_{\infty} = 4.63$ - Continued(e) $\alpha = 20^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\phi = 0.0^\circ, p_t = 7878.9 \text{ psf}$				$\phi = 22.5^\circ, p_t = 7878.9 \text{ psf}$				$\phi = 45.0^\circ, p_t = 7869.4 \text{ psf}$			
				P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t
1	0	.000	.0000	546.5	1.504	.83995	23.57320	546.7	1.505	.84030	23.58303	546.5	1.506	.84108	23.60491
2	0	.000	.0000	546.5	1.491	.83767	23.57320	546.9	1.492	.84030	23.58303	546.5	1.498	.84108	23.60491
3	0	.000	.0000	541.9	1.491	.83767	23.57320	541.9	1.491	.83767	23.58303	541.9	1.498	.84108	23.60491
4	0	.000	.0000	541.9	1.481	.83258	23.52861	541.9	1.481	.83258	23.52861	541.9	1.493	.84108	23.60491
5	0	.000	.0000	538.5	1.481	.83258	23.52861	538.5	1.481	.83258	23.52861	538.5	1.493	.84108	23.60491
6	0	.000	.0000	535.1	1.471	.82767	23.48402	535.1	1.477	.82556	23.48402	535.1	1.483	.83765	23.56941
7	0	.000	.0000	535.1	1.461	.82276	23.43943	535.1	1.468	.82005	23.43943	535.1	1.479	.82533	23.52491
8	0	.000	.0000	531.7	1.461	.82276	23.43943	531.7	1.459	.81573	23.43943	531.7	1.479	.82533	23.52491
9	0	.000	.0000	528.3	1.451	.81785	23.39484	528.3	1.459	.81573	23.39484	528.3	1.479	.82533	23.52491
10	0	.000	.0000	528.3	1.441	.81294	23.35025	528.3	1.459	.81573	23.35025	528.3	1.479	.82533	23.52491
11	0	.000	.0000	524.9	1.441	.80803	23.30566	524.9	1.446	.80345	23.30566	524.9	1.460	.81449	23.27171
12	0	.000	.0000	521.5	1.441	.80803	23.30566	521.5	1.442	.80345	23.30566	521.5	1.460	.81449	23.27171
13	0	.000	.0000	518.1	1.431	.80312	23.26107	518.1	1.442	.80345	23.26107	518.1	1.460	.81449	23.27171
14	0	.000	.0000	514.7	1.431	.80312	23.26107	514.7	1.442	.80345	23.26107	514.7	1.460	.81449	23.27171
15	0	.000	.0000	511.3	1.421	.79821	23.21648	511.3	1.442	.80345	23.21648	511.3	1.460	.81449	23.27171
16	0	.000	.0000	507.9	1.421	.79821	23.21648	507.9	1.442	.80345	23.21648	507.9	1.460	.81449	23.27171
17	0	.000	.0000	504.5	1.411	.79330	23.17189	504.5	1.442	.80345	23.17189	504.5	1.460	.81449	23.27171
18	0	.000	.0000	501.1	1.411	.79330	23.17189	501.1	1.442	.80345	23.17189	501.1	1.460	.81449	23.27171
19	0	.000	.0000	497.7	1.401	.78839	23.12730	497.7	1.442	.80345	23.12730	497.7	1.460	.81449	23.27171
20	0	.000	.0000	494.3	1.401	.78839	23.12730	494.3	1.442	.80345	23.12730	494.3	1.460	.81449	23.27171
21	0	.000	.0000	490.9	1.391	.78348	23.08271	490.9	1.434	.78185	23.10001	490.9	1.455	.79592	23.23721
22	0	.000	.0000	487.5	1.391	.78348	23.08271	487.5	1.434	.78185	23.10001	487.5	1.455	.79592	23.23721
23	0	.000	.0000	484.1	1.381	.77857	23.03812	484.1	1.434	.78185	23.10001	484.1	1.455	.79592	23.23721
24	0	.000	.0000	480.7	1.381	.77857	23.03812	480.7	1.434	.78185	23.10001	480.7	1.455	.79592	23.23721
25	0	.000	.0000	477.3	1.371	.77366	22.99353	477.3	1.434	.78185	23.10001	477.3	1.455	.79592	23.23721
26	0	.000	.0000	473.9	1.371	.77366	22.99353	473.9	1.434	.78185	23.10001	473.9	1.455	.79592	23.23721
27	0	.000	.0000	470.5	1.361	.76875	22.94894	470.5	1.434	.78185	23.10001	470.5	1.455	.79592	23.23721
28	0	.000	.0000	467.1	1.361	.76875	22.94894	467.1	1.434	.78185	23.10001	467.1	1.455	.79592	23.23721
29	0	.000	.0000	463.7	1.351	.76384	22.90435	463.7	1.434	.78185	23.10001	463.7	1.455	.79592	23.23721
30	0	.000	.0000	460.3	1.351	.76384	22.90435	460.3	1.434	.78185	23.10001	460.3	1.455	.79592	23.23721
31	0	.000	.0000	456.9	1.341	.75893	22.85976	456.9	1.434	.78185	23.10001	456.9	1.455	.79592	23.23721
32	0	.000	.0000	453.5	1.341	.75893	22.85976	453.5	1.434	.78185	23.10001	453.5	1.455	.79592	23.23721
33	0	.000	.0000	450.1	1.331	.75402	22.81517	450.1	1.434	.78185	23.10001	450.1	1.455	.79592	23.23721
34	0	.000	.0000	446.7	1.331	.75402	22.81517	446.7	1.434	.78185	23.10001	446.7	1.455	.79592	23.23721
35	0	.000	.0000	443.3	1.321	.74911	22.77058	443.3	1.434	.78185	23.10001	443.3	1.455	.79592	23.23721
36	0	.000	.0000	439.9	1.321	.74911	22.77058	439.9	1.434	.78185	23.10001	439.9	1.455	.79592	23.23721
37	0	.000	.0000	436.5	1.311	.74420	22.72599	436.5	1.434	.78185	23.10001	436.5	1.455	.79592	23.23721
38	0	.000	.0000	433.1	1.311	.74420	22.72599	433.1	1.434	.78185	23.10001	433.1	1.455	.79592	23.23721
39	0	.000	.0000	429.7	1.301	.73929	22.68140	429.7	1.434	.78185	23.10001	429.7	1.455	.79592	23.23721
40	0	.000	.0000	426.3	1.301	.73929	22.68140	426.3	1.434	.78185	23.10001	426.3	1.455	.79592	23.23721
41	0	.000	.0000	422.9	1.291	.73438	22.63681	422.9	1.434	.78185	23.10001	422.9	1.455	.79592	23.23721
42	0	.000	.0000	419.5	1.291	.73438	22.63681	419.5	1.434	.78185	23.10001	419.5	1.455	.79592	23.23721
43	0	.000	.0000	416.1	1.281	.72947	22.59222	416.1	1.434	.78185	23.10001	416.1	1.455	.79592	23.23721
44	0	.000	.0000	412.7	1.281	.72947	22.59222	412.7	1.434	.78185	23.10001	412.7	1.455	.79592	23.23721
45	0	.000	.0000	409.3	1.271	.72456	22.54763	409.3	1.434	.78185	23.10001	409.3	1.455	.79592	23.23721
46	0	.000	.0000	405.9	1.271	.72456	22.54763	405.9	1.434	.78185	23.10001	405.9	1.455	.79592	23.23721
47	0	.000	.0000	402.5	1.261	.71965	22.50304	402.5	1.434	.78185	23.10001	402.5	1.455	.79592	23.23721
48	0	.000	.0000	399.1	1.261	.71965	22.50304	399.1	1.434	.78185	23.10001	399.1	1.455	.79592	23.23721
49	0	.000	.0000	395.7	1.251	.71474	22.45845	395.7	1.434	.78185	23.10001	395.7	1.455	.79592	23.23721
50	0	.000	.0000	392.3	1.251	.71474	22.45845	392.3	1.434	.78185	23.10001	392.3	1.455	.79592	23.23721

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE VIII.- DATA^a FOR 160° CONE; $M_{\infty} = 4.63$ - Concluded

(e) $\alpha = 20^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ, p_t = 7869.4 \text{ psf}$				$\phi = 90.0^\circ, p_t = 7869.4 \text{ psf}$					
				P_t , psf	C_p	$P_t/P_{t,2}$	P_t/P_{∞}	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	P_t/P_{∞}	M_t
1	0	.230	.0000	548.0	1.511	.84342	23.67064	-4.9928	544.8	1.501	.83845	23.53098	-5.0010
2	0	.400	.0025	543.2	1.497	.83605	23.46360	-5.1232	545.4	1.506	.84091	23.59998	-4.9928
3	0	.530	.0050	544.8	1.502	.83851	23.53261	-4.9928	544.8	1.506	.84091	23.59998	-4.9928
4	0	.660	.0075	544.8	1.502	.83851	23.53261	-4.9928	544.8	1.506	.84091	23.59998	-4.9928
5	0	.800	.0100	548.0	1.511	.84342	23.67064	-4.9928	556.0	1.534	.85566	24.01402	-4.7720
6	0	1.125	.0263	546.4	1.506	.84096	23.60163	-5.0365	556.0	1.534	.85566	24.01402	-4.7720
7	0	1.200	.0296	544.8	1.502	.83851	23.53261	-5.0365	555.0	1.534	.85566	24.01402	-4.7720
8	0	1.175	.0348	544.8	1.497	.83605	23.46360	-5.1232	555.0	1.534	.85566	24.01402	-4.7720
9	0	1.400	.0425	544.8	1.488	.83113	23.32558	-5.2091	554.0	1.529	.85320	23.94501	-4.8169
10	0	1.225	.0434	538.5	1.483	.82607	23.18757	-5.2958	552.8	1.524	.85074	23.94501	-4.8169
11	0	2.000	.0926	535.3	1.474	.82175	23.11855	-5.3366	551.2	1.520	.84828	23.87601	-4.8615
12	0	2.200	.0951	532.1	1.465	.81683	22.98053	-5.4207	548.0	1.511	.84337	23.80700	-4.9058
13	0	2.450	.1000	527.3	1.451	.81146	22.77350	-5.5457	544.8	1.501	.83845	23.73801	-4.9500
14	0	2.600	.1035	522.6	1.443	.80649	22.63556	-5.6323	543.2	1.495	.83592	23.66901	-5.0010
15	0	2.830	.1087	516.1	1.419	.78944	22.29052	-5.8823	536.8	1.478	.82815	23.51859	-5.2593
16	0	3.000	.1137	509.7	1.403	.78441	22.01438	-5.9934	533.4	1.460	.81632	22.90993	-5.5635
17	0	3.200	.1200	500.1	1.373	.76945	21.60032	-6.2319	522.4	1.437	.80402	22.50490	-5.6703
18	0	3.500	.1425	487.5	1.325	.74998	21.04833	-6.5500	511.3	1.405	.78641	22.08186	-5.9542
19	0	3.600	.1475	482.2	1.312	.74505	20.91645	-6.6252	509.5	1.400	.78394	22.01286	-6.0042
20	0	4.000	.1742	471.6	1.262	.72619	19.76495	-7.0781	500.8	1.376	.77197	20.14869	-7.0460
21	0	4.200	.1822	464.2	1.097	.62212	17.45968	-8.5215	455.0	1.157	.65504	18.33554	-8.0305
22	180	.200	.0025	563.4	1.555	.86705	24.33370	-4.5608	526.0	1.534	.85556	24.01402	-4.7720
23	180	.400	.0050	599.5	1.578	.87933	24.67837	-4.3758	553.2	1.543	.86058	24.15203	-4.6816
24	180	.600	.0075	617.6	1.596	.89314	24.91624	-4.2152	570.8	1.552	.86556	24.29004	-4.5900
25	180	.800	.0100	630.9	1.596	.89407	25.09198	-4.0317	584.3	1.557	.86795	24.35905	-4.5438
26	180	1.200	.0150	582.9	1.610	.89652	25.16091	-3.9812	564.0	1.557	.86795	24.35905	-4.5438
27	180	1.400	.0175	584.8	1.615	.89838	25.22985	-3.9303	564.0	1.557	.86795	24.35905	-4.5438
28	180	1.500	.0200	584.1	1.615	.89848	25.22985	-3.9303	564.0	1.557	.86795	24.35905	-4.5438
29	180	2.000	.0341	584.1	1.615	.89848	25.22985	-3.9303	564.0	1.557	.86795	24.35905	-4.5438
30	180	2.200	.0375	584.1	1.615	.89848	25.22985	-3.9303	560.8	1.547	.86504	24.22104	-4.6359
31	180	2.200	.0375	584.1	1.615	.89848	25.22985	-3.9303	557.6	1.538	.85812	24.08302	-4.7269
32	180	2.200	.0375	584.1	1.615	.89848	25.22985	-3.9303	557.6	1.538	.85812	24.08302	-4.7269
33	180	2.400	.0400	591.2	1.610	.89652	25.16091	-3.9812	554.4	1.529	.85320	23.94501	-4.8169
34	180	2.500	.0425	582.5	1.601	.89161	25.02304	-4.0818	551.2	1.520	.84828	23.80700	-4.9058
35	180	2.500	.0425	582.5	1.601	.89161	25.02304	-4.0818	551.2	1.520	.84828	23.80700	-4.9058
36	180	3.000	.0715	571.6	1.576	.87733	24.67837	-4.3258	540.4	1.488	.83107	23.32396	-5.2101
37	180	3.200	.0750	583.4	1.555	.86705	24.33370	-4.5608	532.0	1.460	.81632	22.90993	-5.5635
38	180	3.500	.0875	555.4	1.532	.85477	23.98903	-4.7883	520.8	1.433	.80157	22.49589	-5.7112
39	180	3.500	.0875	555.4	1.532	.85477	23.98903	-4.7883	520.8	1.433	.80157	22.49589	-5.7112
40	180	4.000	.1200	519.4	1.486	.83021	23.29699	-5.2552	503.3	1.392	.77452	21.73683	-6.1535
41	180	4.000	.1200	519.4	1.486	.83021	23.29699	-5.2552	503.3	1.392	.77452	21.73683	-6.1535
42	180	4.000	.1200	519.4	1.486	.83021	23.29699	-5.2552	503.3	1.392	.77452	21.73683	-6.1535
43	270	2.300	.2453	659.7	1.668	.93828	26.33279	-3.3035	613.5	1.699	.94418	26.49823	-2.8764
44	270	2.300	.2453	659.7	1.668	.93828	26.33279	-3.3035	613.5	1.699	.94418	26.49823	-2.8764
45	270	3.000	.3759	532.0	1.753	.97257	27.29787	-1.9937	640.7	1.777	.98597	27.67133	-1.8219
46	270	3.000	.3759	532.0	1.753	.97257	27.29787	-1.9937	640.7	1.777	.98597	27.67133	-1.8219
47	90	2.000	.0926	519.3	1.428	.79916	22.42865	-5.7511	515.0	1.419	.79419	22.28887	-5.9333
48	90	3.300	.3589	488.9	1.341	.75244	21.11724	-6.5061	485.7	1.247	.74747	20.97776	-6.8446
49	90	4.300	.5002	379.7	1.023	.58277	16.35551	-9.0126	377.0	1.019	.58027	16.28537	-9.1718

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE IX.- DATA^a FOR 180° CONE; $M_{\infty} = 2.30$ (a) $\alpha = 0^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0.0^\circ, P_t = 2288.9 \text{ psf}$				$\Phi = 22.5^\circ, P_t = 2289.8 \text{ psf}$				$\Phi = 45.0^\circ, P_t = 2291.1 \text{ psf}$				
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/\rho a_0$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/\rho a_0$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$
1	0	0.20	0.000	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
2	0	0.20	0.000	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
3	0	0.40	0.050	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
4	0	0.50	0.075	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
5	0	0.70	0.125	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
6	0	1.00	0.200	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
7	0	1.20	0.250	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
8	0	1.40	0.300	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
9	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
10	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
11	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
12	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
13	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
14	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
15	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
16	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
17	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
18	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
19	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
20	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
21	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
22	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
23	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
24	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
25	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
26	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
27	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
28	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
29	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
30	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
31	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
32	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
33	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
34	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
35	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
36	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
37	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
38	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
39	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
40	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
41	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
42	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
43	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
44	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273
45	0	1.50	0.325	1332.4	1.696	0.9794	7.27872	1.692	0.9800	7.25461	1.696	0.9825	7.26095	1.694	0.9850	7.27273

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE IX.- DATA^a FOR 180° CONE; $M_{\infty} = 2.30$ - Continued

(a) $\alpha = 0^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 67.5^\circ, p_t = 2292.1 \text{ psf}$					$\Phi = 90.0^\circ, p_t = 2291.3 \text{ psf}$				
				p_t , psf	C_p	$p_t/p_{t,2}$	p_t/Φ	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	p_t/Φ	M_t
1	0	0.330	-0.000	1335.5	1.697	0.9887	7.28548	0.4026	1335.5	1.698	0.9921	7.28802	0.3350
2	0	0.330	-0.025	1335.9	1.695	0.9876	7.27616	0.372	1335.9	1.696	0.9902	7.28130	0.5322
3	0	0.330	-0.050	1336.3	1.693	0.9865	7.26684	0.336	1336.3	1.694	0.9878	7.27630	0.6742
4	0	0.330	-0.075	1336.7	1.691	0.9854	7.25752	0.299	1336.7	1.692	0.9862	7.27059	0.8162
5	0	0.330	-0.100	1337.1	1.689	0.9843	7.24820	0.262	1337.1	1.690	0.9850	7.26187	0.9582
6	0	1.000	-0.125	1337.5	1.688	0.9832	7.23888	0.225	1337.5	1.691	0.9856	7.25256	1.1002
7	0	1.230	-0.150	1337.9	1.688	0.9821	7.22956	0.188	1337.9	1.691	0.9862	7.24324	1.2422
8	0	1.460	-0.175	1338.3	1.688	0.9810	7.22024	0.151	1338.3	1.692	0.9872	7.23392	1.3842
9	0	1.690	-0.200	1338.7	1.688	0.9800	7.21092	0.114	1338.7	1.693	0.9882	7.22460	1.5262
10	0	1.920	-0.225	1339.1	1.688	0.9789	7.20160	0.077	1339.1	1.695	0.9926	7.21528	1.6682
11	0	2.150	-0.250	1339.5	1.688	0.9778	7.19228	0.040	1339.5	1.697	0.9968	7.20596	1.8102
12	0	2.380	-0.275	1339.9	1.688	0.9767	7.18296	0.003	1339.9	1.699	0.9999	7.19664	1.9522
13	0	2.610	-0.300	1340.3	1.688	0.9756	7.17364	0.000	1340.3	1.701	1.0031	7.18732	2.0942
14	0	2.840	-0.325	1340.7	1.688	0.9745	7.16432	0.000	1340.7	1.703	1.0062	7.17800	2.2362
15	0	3.070	-0.350	1341.1	1.688	0.9734	7.15500	0.000	1341.1	1.705	1.0093	7.16868	2.3782
16	0	3.300	-0.375	1341.5	1.688	0.9723	7.14568	0.000	1341.5	1.707	1.0124	7.15936	2.5202
17	0	3.530	-0.400	1341.9	1.688	0.9712	7.13636	0.000	1341.9	1.709	1.0155	7.15004	2.6622
18	0	3.760	-0.425	1342.3	1.688	0.9701	7.12704	0.000	1342.3	1.711	1.0186	7.14072	2.8042
19	0	3.990	-0.450	1342.7	1.688	0.9690	7.11772	0.000	1342.7	1.713	1.0217	7.13140	2.9462
20	0	4.220	-0.475	1343.1	1.688	0.9679	7.10840	0.000	1343.1	1.715	1.0248	7.12208	3.0882
21	180	0.330	-0.050	1335.5	1.697	0.9887	7.28548	0.4026	1335.5	1.698	0.9921	7.28802	0.3350
22	180	0.330	-0.025	1335.9	1.695	0.9876	7.27616	0.372	1335.9	1.698	0.9921	7.28802	0.3350
23	180	0.330	-0.050	1336.3	1.693	0.9865	7.26684	0.336	1336.3	1.698	0.9921	7.28802	0.3350
24	180	0.330	-0.075	1336.7	1.691	0.9854	7.25752	0.299	1336.7	1.698	0.9921	7.28802	0.3350
25	180	1.000	-0.125	1337.1	1.688	0.9843	7.24820	0.262	1337.1	1.699	0.9943	7.27937	0.7073
26	180	1.230	-0.150	1337.5	1.688	0.9832	7.23888	0.225	1337.5	1.701	0.9964	7.27005	0.8493
27	180	1.460	-0.175	1337.9	1.689	0.9831	7.22931	0.184	1337.9	1.703	0.9984	7.26073	0.9913
28	180	1.690	-0.200	1338.3	1.689	0.9832	7.22316	0.149	1338.3	1.705	1.0004	7.25141	1.1333
29	180	1.920	-0.225	1338.7	1.689	0.9832	7.21757	0.114	1338.7	1.707	1.0024	7.24188	1.2753
30	180	2.150	-0.250	1339.1	1.689	0.9832	7.21198	0.079	1339.1	1.709	1.0044	7.23235	1.4173
31	180	2.380	-0.275	1339.5	1.689	0.9832	7.20639	0.044	1339.5	1.711	1.0064	7.22282	1.5593
32	180	2.610	-0.300	1339.9	1.689	0.9832	7.20080	0.009	1339.9	1.713	1.0084	7.21329	1.7013
33	180	2.840	-0.325	1340.3	1.689	0.9832	7.19521	0.000	1340.3	1.715	1.0104	7.20376	1.8433
34	180	3.070	-0.350	1340.7	1.689	0.9832	7.18962	0.000	1340.7	1.717	1.0124	7.19423	1.9853
35	180	3.300	-0.375	1341.1	1.689	0.9832	7.18403	0.000	1341.1	1.719	1.0144	7.18470	2.1273
36	180	3.530	-0.400	1341.5	1.689	0.9832	7.17844	0.000	1341.5	1.721	1.0164	7.17517	2.2693
37	180	3.760	-0.425	1341.9	1.689	0.9832	7.17285	0.000	1341.9	1.723	1.0184	7.16564	2.4113
38	180	3.990	-0.450	1342.3	1.689	0.9832	7.16726	0.000	1342.3	1.725	1.0204	7.15611	2.5533
39	180	4.220	-0.475	1342.7	1.689	0.9832	7.16167	0.000	1342.7	1.727	1.0224	7.14658	2.6953
40	270	1.000	-0.125	1337.1	1.688	0.9843	7.24820	0.262	1337.1	1.699	0.9943	7.27937	0.7073
41	270	1.230	-0.150	1337.5	1.688	0.9832	7.23888	0.225	1337.5	1.701	0.9964	7.27005	0.8493
42	270	1.460	-0.175	1337.9	1.689	0.9832	7.22931	0.149	1337.9	1.703	0.9984	7.26073	0.9913
43	270	1.690	-0.200	1338.3	1.689	0.9832	7.22316	0.114	1338.3	1.705	1.0004	7.25141	1.1333
44	270	1.920	-0.225	1338.7	1.689	0.9832	7.21757	0.079	1338.7	1.707	1.0024	7.24188	1.2753
45	270	2.150	-0.250	1339.1	1.689	0.9832	7.21198	0.044	1339.1	1.709	1.0044	7.23235	1.4173
46	270	2.380	-0.275	1339.5	1.689	0.9832	7.20639	0.009	1339.5	1.711	1.0064	7.22282	1.5593
47	270	2.610	-0.300	1339.9	1.689	0.9832	7.20080	0.000	1339.9	1.713	1.0084	7.21329	1.7013
48	270	2.840	-0.325	1340.3	1.689	0.9832	7.19521	0.000	1340.3	1.715	1.0104	7.20376	1.8433
49	270	3.070	-0.350	1340.7	1.689	0.9832	7.18962	0.000	1340.7	1.717	1.0124	7.19423	1.9853
50	270	3.300	-0.375	1341.1	1.689	0.9832	7.18403	0.000	1341.1	1.719	1.0144	7.18470	2.1273
51	270	3.530	-0.400	1341.5	1.689	0.9832	7.17844	0.000	1341.5	1.721	1.0164	7.17517	2.2693
52	270	3.760	-0.425	1341.9	1.689	0.9832	7.17285	0.000	1341.9	1.723	1.0184	7.16564	2.4113
53	270	3.990	-0.450	1342.3	1.689	0.9832	7.16726	0.000	1342.3	1.725	1.0204	7.15611	2.5533
54	270	4.220	-0.475	1342.7	1.689	0.9832	7.16167	0.000	1342.7	1.727	1.0224	7.14658	2.6953
55	270	4.450	-0.500	1343.1	1.689	0.9832	7.15608	0.000	1343.1	1.729	1.0244	7.13705	2.8373

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE IX. - DATA^a FOR 180° CONE; $M_{\infty} = 2.30$ - Continued(b) $\alpha = 5^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0.0^\circ, p_t = 2289.4 \text{ psf}$					$\Phi = 22.5^\circ, p_t = 2290.3 \text{ psf}$					$\Phi = 45.0^\circ, p_t = 2290.5 \text{ psf}$				
				$p_{t,1}$, psf	C_p	$p_{t,1}/p_{t,2}$	$p_{t,1}/p_{\infty}$	$M_{t,1}$	$p_{t,1}$, psf	C_p	$p_{t,1}/p_{t,2}$	$p_{t,1}/p_{\infty}$	$M_{t,1}$	$p_{t,1}$, psf	C_p	$p_{t,1}/p_{t,2}$	$p_{t,1}/p_{\infty}$	$M_{t,1}$
1	0	.010	.0000	1328.7	1.690	.99498	7.25715	1330.6	1.692	.99599	7.26453	1329.0	1.689	.99471	7.25518	.08706		
2	0	.200	.0005	1328.7	1.690	.99498	7.25715	1327.4	1.687	.99360	7.24709	1325.8	1.687	.99360	7.24709	.08532		
3	0	.400	.0010	1328.7	1.685	.99259	7.23971	1327.4	1.687	.99360	7.24709	1325.8	1.685	.99259	7.23971	.08388		
4	0	.600	.0015	1328.7	1.685	.99259	7.23971	1325.8	1.687	.99241	7.22993	1324.2	1.685	.99241	7.22993	.08244		
5	0	.800	.0020	1328.7	1.678	.98800	7.19940	1325.8	1.685	.99043	7.20918	1324.2	1.685	.99043	7.20918	.08100		
6	0	1.000	.0025	1328.7	1.678	.98800	7.19940	1324.2	1.685	.98843	7.19477	1319.4	1.678	.98843	7.19477	.07956		
7	0	1.200	.0030	1328.7	1.666	.98302	7.16993	1324.2	1.666	.98284	7.16860	1315.6	1.666	.98284	7.16860	.07812		
8	0	1.400	.0035	1328.7	1.659	.97944	7.16376	1324.2	1.659	.97926	7.16244	1312.0	1.659	.97926	7.16244	.07668		
9	0	1.600	.0040	1328.7	1.650	.97465	7.16087	1324.2	1.650	.97465	7.16087	1308.4	1.650	.97465	7.16087	.07524		
10	0	1.800	.0045	1328.7	1.638	.96667	7.15086	1324.2	1.638	.96667	7.15086	1304.8	1.638	.96667	7.15086	.07380		
11	0	2.000	.0050	1328.7	1.627	.96171	7.14687	1324.2	1.627	.96171	7.14687	1301.2	1.627	.96171	7.14687	.07236		
12	0	2.200	.0055	1328.7	1.617	.95791	7.14288	1324.2	1.617	.95791	7.14288	1297.6	1.617	.95791	7.14288	.07092		
13	0	2.400	.0060	1328.7	1.608	.95434	7.13889	1324.2	1.616	.95373	7.13879	1294.0	1.615	.95373	7.13879	.06948		
14	0	2.600	.0065	1328.7	1.598	.95078	7.13490	1324.2	1.616	.95373	7.13879	1290.4	1.615	.95373	7.13879	.06804		
15	0	2.800	.0070	1328.7	1.589	.94734	7.13091	1324.2	1.598	.94817	7.13470	1286.8	1.597	.94817	7.13470	.06660		
16	0	3.000	.0075	1328.7	1.580	.94391	7.12692	1324.2	1.598	.94817	7.13470	1283.2	1.597	.94817	7.13470	.06516		
17	0	3.200	.0080	1328.7	1.571	.94048	7.12293	1324.2	1.598	.94817	7.13470	1279.6	1.597	.94817	7.13470	.06372		
18	0	3.400	.0085	1328.7	1.562	.93705	7.11894	1324.2	1.598	.94817	7.13470	1276.0	1.597	.94817	7.13470	.06228		
19	0	3.600	.0090	1328.7	1.553	.93362	7.11495	1324.2	1.598	.94817	7.13470	1272.4	1.597	.94817	7.13470	.06084		
20	0	3.800	.0095	1328.7	1.544	.93019	7.11096	1324.2	1.598	.94817	7.13470	1268.8	1.597	.94817	7.13470	.05940		
21	0	4.000	.0100	1328.7	1.535	.92676	7.10697	1324.2	1.598	.94817	7.13470	1265.2	1.597	.94817	7.13470	.05796		
22	0	4.200	.0105	1328.7	1.526	.92333	7.10298	1324.2	1.598	.94817	7.13470	1261.6	1.597	.94817	7.13470	.05652		
23	0	4.400	.0110	1328.7	1.517	.91990	7.09899	1324.2	1.598	.94817	7.13470	1258.0	1.597	.94817	7.13470	.05508		
24	0	4.600	.0115	1328.7	1.508	.91647	7.09499	1324.2	1.598	.94817	7.13470	1254.4	1.597	.94817	7.13470	.05364		
25	0	4.800	.0120	1328.7	1.499	.91304	7.09099	1324.2	1.598	.94817	7.13470	1250.8	1.597	.94817	7.13470	.05220		
26	0	5.000	.0125	1328.7	1.490	.90961	7.08699	1324.2	1.598	.94817	7.13470	1247.2	1.597	.94817	7.13470	.05076		
27	0	5.200	.0130	1328.7	1.481	.90618	7.08299	1324.2	1.598	.94817	7.13470	1243.6	1.597	.94817	7.13470	.04932		
28	0	5.400	.0135	1328.7	1.472	.90275	7.07899	1324.2	1.598	.94817	7.13470	1240.0	1.597	.94817	7.13470	.04788		
29	0	5.600	.0140	1328.7	1.463	.89932	7.07499	1324.2	1.598	.94817	7.13470	1236.4	1.597	.94817	7.13470	.04644		
30	0	5.800	.0145	1328.7	1.454	.89589	7.07099	1324.2	1.598	.94817	7.13470	1232.8	1.597	.94817	7.13470	.04500		
31	0	6.000	.0150	1328.7	1.445	.89246	7.06699	1324.2	1.598	.94817	7.13470	1229.2	1.597	.94817	7.13470	.04356		
32	0	6.200	.0155	1328.7	1.436	.88903	7.06299	1324.2	1.598	.94817	7.13470	1225.6	1.597	.94817	7.13470	.04212		
33	0	6.400	.0160	1328.7	1.427	.88560	7.05899	1324.2	1.598	.94817	7.13470	1222.0	1.597	.94817	7.13470	.04068		
34	0	6.600	.0165	1328.7	1.418	.88217	7.05499	1324.2	1.598	.94817	7.13470	1218.4	1.597	.94817	7.13470	.03924		
35	0	6.800	.0170	1328.7	1.409	.87874	7.05099	1324.2	1.598	.94817	7.13470	1214.8	1.597	.94817	7.13470	.03780		
36	0	7.000	.0175	1328.7	1.400	.87531	7.04699	1324.2	1.598	.94817	7.13470	1211.2	1.597	.94817	7.13470	.03636		
37	0	7.200	.0180	1328.7	1.391	.87188	7.04299	1324.2	1.598	.94817	7.13470	1207.6	1.597	.94817	7.13470	.03492		
38	0	7.400	.0185	1328.7	1.382	.86845	7.03899	1324.2	1.598	.94817	7.13470	1204.0	1.597	.94817	7.13470	.03348		
39	0	7.600	.0190	1328.7	1.373	.86502	7.03499	1324.2	1.598	.94817	7.13470	1200.4	1.597	.94817	7.13470	.03204		
40	0	7.800	.0195	1328.7	1.364	.86159	7.03099	1324.2	1.598	.94817	7.13470	1196.8	1.597	.94817	7.13470	.03060		
41	0	8.000	.0200	1328.7	1.355	.85816	7.02699	1324.2	1.598	.94817	7.13470	1193.2	1.597	.94817	7.13470	.02916		
42	0	8.200	.0205	1328.7	1.346	.85473	7.02299	1324.2	1.598	.94817	7.13470	1189.6	1.597	.94817	7.13470	.02772		
43	0	8.400	.0210	1328.7	1.337	.85130	7.01899	1324.2	1.598	.94817	7.13470	1186.0	1.597	.94817	7.13470	.02628		
44	0	8.600	.0215	1328.7	1.328	.84787	7.01499	1324.2	1.598	.94817	7.13470	1182.4	1.597	.94817	7.13470	.02484		
45	0	8.800	.0220	1328.7	1.319	.84444	7.01099	1324.2	1.598	.94817	7.13470	1178.8	1.597	.94817	7.13470	.02340		

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE IX. - DATA^a FOR 180° CONE; $M_{\infty} = 2.30$ - Continued

(b) $\alpha = 5^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ, P_t = 2292.3 \text{ psf}$				$\Phi = 90.0^\circ, P_t = 2292.0 \text{ psf}$			
				P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t
1	0	-0.00	-0.000	1329.2	1.688	.98407	.99232	1329.7	1.690	.99533	.08185
2	0	-0.20	-0.000	1327.6	1.686	.98287	.99232	1329.1	1.688	.99413	.08175
3	0	-0.40	-0.000	1326.0	1.686	.98168	.99232	1328.5	1.688	.99293	.08165
4	0	-0.60	-0.000	1324.4	1.686	.98049	.99232	1327.9	1.688	.99173	.08155
5	0	-0.80	-0.000	1322.8	1.686	.97930	.99232	1327.3	1.688	.99053	.08145
6	0	-1.00	-0.000	1321.2	1.686	.97811	.99232	1326.7	1.688	.98933	.08135
7	0	-1.20	-0.000	1319.6	1.686	.97692	.99232	1326.1	1.688	.98813	.08125
8	0	-1.40	-0.000	1318.0	1.686	.97573	.99232	1325.5	1.688	.98693	.08115
9	0	-1.60	-0.000	1316.4	1.686	.97454	.99232	1324.9	1.688	.98573	.08105
10	0	-1.80	-0.000	1314.8	1.686	.97335	.99232	1324.3	1.688	.98453	.08095
11	0	-2.00	-0.000	1313.2	1.686	.97216	.99232	1323.7	1.688	.98333	.08085
12	0	-2.20	-0.000	1311.6	1.686	.97097	.99232	1323.1	1.688	.98213	.08075
13	0	-2.40	-0.000	1310.0	1.686	.96978	.99232	1322.5	1.688	.98093	.08065
14	0	-2.60	-0.000	1308.4	1.686	.96859	.99232	1321.9	1.688	.97973	.08055
15	0	-2.80	-0.000	1306.8	1.686	.96740	.99232	1321.3	1.688	.97853	.08045
16	0	-3.00	-0.000	1305.2	1.686	.96621	.99232	1320.7	1.688	.97733	.08035
17	0	-3.20	-0.000	1303.6	1.686	.96502	.99232	1320.1	1.688	.97613	.08025
18	0	-3.40	-0.000	1302.0	1.686	.96383	.99232	1319.5	1.688	.97493	.08015
19	0	-3.60	-0.000	1300.4	1.686	.96264	.99232	1318.9	1.688	.97373	.08005
20	0	-3.80	-0.000	1298.8	1.686	.96145	.99232	1318.3	1.688	.97253	.07995
21	0	-4.00	-0.000	1297.2	1.686	.96026	.99232	1317.7	1.688	.97133	.07985
22	0	-4.20	-0.000	1295.6	1.686	.95907	.99232	1317.1	1.688	.97013	.07975
23	0	-4.40	-0.000	1294.0	1.686	.95788	.99232	1316.5	1.688	.96893	.07965
24	0	-4.60	-0.000	1292.4	1.686	.95669	.99232	1315.9	1.688	.96773	.07955
25	0	-4.80	-0.000	1290.8	1.686	.95550	.99232	1315.3	1.688	.96653	.07945
26	0	-5.00	-0.000	1289.2	1.686	.95431	.99232	1314.7	1.688	.96533	.07935
27	0	-5.20	-0.000	1287.6	1.686	.95312	.99232	1314.1	1.688	.96413	.07925
28	0	-5.40	-0.000	1286.0	1.686	.95193	.99232	1313.5	1.688	.96293	.07915
29	0	-5.60	-0.000	1284.4	1.686	.95074	.99232	1312.9	1.688	.96173	.07905
30	0	-5.80	-0.000	1282.8	1.686	.94955	.99232	1312.3	1.688	.96053	.07895
31	0	-6.00	-0.000	1281.2	1.686	.94836	.99232	1311.7	1.688	.95933	.07885
32	0	-6.20	-0.000	1279.6	1.686	.94717	.99232	1311.1	1.688	.95813	.07875
33	0	-6.40	-0.000	1278.0	1.686	.94598	.99232	1310.5	1.688	.95693	.07865
34	0	-6.60	-0.000	1276.4	1.686	.94479	.99232	1309.9	1.688	.95573	.07855
35	0	-6.80	-0.000	1274.8	1.686	.94360	.99232	1309.3	1.688	.95453	.07845
36	0	-7.00	-0.000	1273.2	1.686	.94241	.99232	1308.7	1.688	.95333	.07835
37	0	-7.20	-0.000	1271.6	1.686	.94122	.99232	1308.1	1.688	.95213	.07825
38	0	-7.40	-0.000	1270.0	1.686	.94003	.99232	1307.5	1.688	.95093	.07815
39	0	-7.60	-0.000	1268.4	1.686	.93884	.99232	1306.9	1.688	.94973	.07805
40	0	-7.80	-0.000	1266.8	1.686	.93765	.99232	1306.3	1.688	.94853	.07795
41	0	-8.00	-0.000	1265.2	1.686	.93646	.99232	1305.7	1.688	.94733	.07785
42	0	-8.20	-0.000	1263.6	1.686	.93527	.99232	1305.1	1.688	.94613	.07775
43	0	-8.40	-0.000	1262.0	1.686	.93408	.99232	1304.5	1.688	.94493	.07765
44	0	-8.60	-0.000	1260.4	1.686	.93289	.99232	1303.9	1.688	.94373	.07755
45	0	-8.80	-0.000	1258.8	1.686	.93170	.99232	1303.3	1.688	.94253	.07745

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE IX. - DATA^a FOR 180° CONE; $M_{\infty} = 2.30$ - Continued(c) $\alpha = 10^\circ$

Orifice deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, p_t = 2289.3 \text{ psf}$				$\phi = 22.5^\circ, p_t = 2291.7 \text{ psf}$				$\phi = 45.0^\circ, p_t = 2291.1 \text{ psf}$						
				$p_{t,1}$ psf	C_p	$p_{t,1}/p_{t,2}$	$p_{t,1}/p_\infty$	$M_{t,1}$	$p_{t,1}$ psf	C_p	$p_{t,1}/p_{t,2}$	$p_{t,1}/p_\infty$	$M_{t,1}$	$p_{t,1}$ psf	C_p	$p_{t,1}/p_{t,2}$	$p_{t,1}/p_\infty$	$M_{t,1}$
1	0	0.30	-0.000	1319.2	1.676	0.98789	7.20541	-13206	1319.6	1.674	0.98716	7.20009	-13401	1319.8	1.675	0.98755	7.20257	-13388
2	0	0.200	-0.25	1316.0	1.664	0.98549	7.18794	-14464	1314.8	1.667	0.98357	7.17394	-15907	1316.6	1.670	0.98517	7.19837	-13213
3	0	0.150	-0.75	1311.2	1.652	0.98190	7.16174	-16174	1313.2	1.665	0.98238	7.15522	-17597	1315.6	1.668	0.98397	7.17681	-13173
4	0	0.100	-1.00	1303.2	1.643	0.97591	7.11807	-18658	1308.2	1.658	0.97879	7.11907	-20322	1313.4	1.666	0.98277	7.16809	-13176
5	0	0.800	-1.25	1298.8	1.636	0.97112	7.08313	-20502	1298.8	1.644	0.97162	7.08697	-22032	1303.8	1.652	0.97560	7.11577	-131819
6	0	1.300	-1.50	1292.0	1.625	0.96753	7.05693	-21766	1292.4	1.634	0.96684	7.05100	-22032	1295.8	1.640	0.96962	7.10217	-131819
7	0	1.800	-1.75	1284.0	1.615	0.96154	7.03326	-23735	1286.0	1.625	0.96206	7.03100	-22032	1291.0	1.633	0.96603	7.04601	-131819
8	0	2.300	-2.00	1274.0	1.612	0.95556	6.99719	-25557	1276.4	1.611	0.95489	6.99294	-22032	1284.0	1.623	0.96125	7.01113	-131819
9	0	2.800	-2.25	1268.4	1.598	0.94837	6.97119	-27623	1268.5	1.587	0.94824	6.87757	-22032	1278.0	1.612	0.95527	6.98793	-131819
10	0	3.300	-2.50	1258.8	1.584	0.94119	6.86479	-29554	1260.5	1.573	0.93577	6.82526	-30942	1268.6	1.600	0.94030	6.86286	-131819
11	0	3.800	-2.75	1248.8	1.572	0.93520	6.74251	-31085	1250.9	1.563	0.92621	6.75553	-33274	1266.3	1.567	0.93256	6.80184	-131819
12	0	4.300	-3.00	1238.4	1.552	0.92442	6.61284	-33695	1240.5	1.545	0.91665	6.58991	-35481	1251.9	1.546	0.92180	6.72336	-131819
13	0	4.800	-3.25	1228.4	1.532	0.91284	6.47884	-36895	1229.3	1.515	0.90489	6.47659	-39350	1217.5	1.524	0.91104	6.64003	-131819
14	0	5.300	-3.50	1218.4	1.504	0.90047	6.34030	-39891	1218.0	1.479	0.89194	6.35456	-41816	1217.2	1.498	0.87756	6.45023	-131819
15	0	5.800	-3.75	1208.4	1.475	0.88814	6.20202	-43495	1207.8	1.466	0.88723	6.35456	-44816	1212.8	1.458	0.86523	6.45023	-131819
16	0	6.300	-4.00	1198.4	1.440	0.87581	6.06366	-46795	1197.8	1.446	0.88723	6.35456	-47816	1206.9	1.430	0.84523	6.45023	-131819
17	0	6.800	-4.25	1188.4	1.400	0.86348	5.92530	-50095	1187.8	1.414	0.87123	6.35456	-50816	1196.9	1.404	0.82556	6.45023	-131819
18	0	7.300	-4.50	1178.4	1.370	0.85115	5.78694	-53395	1186.3	1.391	0.85767	5.71774	-53729	1186.2	1.414	0.84523	6.45023	-131819
19	0	7.800	-4.75	1168.4	1.330	0.83882	5.64848	-56695	1180.3	1.350	0.84523	5.71774	-56816	1182.2	1.423	0.82556	6.45023	-131819
20	0	8.300	-5.00	1158.4	1.290	0.82649	5.51104	-59995	1174.3	1.320	0.83276	5.71774	-60017	1179.8	1.432	0.80523	6.45023	-131819
21	0	8.800	-5.25	1148.4	1.250	0.81416	5.37356	-63295	1168.3	1.280	0.82036	5.71774	-63276	1174.8	1.441	0.78523	6.45023	-131819
22	0	9.300	-5.50	1138.4	1.210	0.80183	5.23608	-66595	1162.3	1.250	0.80736	5.71774	-66581	1170.8	1.450	0.76523	6.45023	-131819
23	0	9.800	-5.75	1128.4	1.170	0.78950	5.09860	-69895	1156.3	1.210	0.79386	5.71774	-69868	1166.8	1.459	0.74523	6.45023	-131819
24	0	10.300	-6.00	1118.4	1.130	0.77712	4.96112	-73195	1150.3	1.170	0.78917	5.71774	-73158	1162.8	1.467	0.72523	6.45023	-131819
25	0	10.800	-6.25	1108.4	1.090	0.76474	4.82364	-76495	1144.3	1.130	0.78917	5.71774	-76432	1158.8	1.475	0.70523	6.45023	-131819
26	0	11.300	-6.50	1098.4	1.050	0.75236	4.68616	-79795	1138.3	1.090	0.78917	5.71774	-79726	1154.8	1.483	0.68523	6.45023	-131819
27	0	11.800	-6.75	1088.4	1.010	0.74000	4.54868	-83095	1132.3	1.050	0.78917	5.71774	-83060	1150.8	1.491	0.66523	6.45023	-131819
28	0	12.300	-7.00	1078.4	0.970	0.72764	4.41120	-86395	1126.3	1.010	0.78917	5.71774	-86325	1146.8	1.500	0.64523	6.45023	-131819
29	0	12.800	-7.25	1068.4	0.930	0.71528	4.27372	-89695	1120.3	0.970	0.78917	5.71774	-89660	1142.8	1.508	0.62523	6.45023	-131819
30	0	13.300	-7.50	1058.4	0.890	0.70292	4.13624	-92995	1114.3	0.930	0.78917	5.71774	-92960	1138.8	1.516	0.60523	6.45023	-131819
31	0	13.800	-7.75	1048.4	0.850	0.69056	4.00000	-96295	1108.3	0.890	0.78917	5.71774	-96260	1134.8	1.524	0.58523	6.45023	-131819
32	0	14.300	-8.00	1038.4	0.810	0.67820	3.86252	-99595	1102.3	0.850	0.78917	5.71774	-99560	1130.8	1.532	0.56523	6.45023	-131819
33	0	14.800	-8.25	1028.4	0.770	0.66584	3.72504	-102895	1096.3	0.810	0.78917	5.71774	-102860	1126.8	1.540	0.54523	6.45023	-131819
34	0	15.300	-8.50	1018.4	0.730	0.65348	3.58756	-106195	1090.3	0.770	0.78917	5.71774	-106160	1122.8	1.548	0.52523	6.45023	-131819
35	0	15.800	-8.75	1008.4	0.690	0.64112	3.45008	-109495	1084.3	0.730	0.78917	5.71774	-109460	1118.8	1.556	0.50523	6.45023	-131819
36	0	16.300	-9.00	998.4	0.650	0.62876	3.31260	-112795	1078.3	0.690	0.78917	5.71774	-112760	1114.8	1.564	0.48523	6.45023	-131819
37	0	16.800	-9.25	988.4	0.610	0.61640	3.17512	-116095	1072.3	0.650	0.78917	5.71774	-116060	1110.8	1.572	0.46523	6.45023	-131819
38	0	17.300	-9.50	978.4	0.570	0.60404	3.03764	-119395	1066.3	0.610	0.78917	5.71774	-119360	1106.8	1.580	0.44523	6.45023	-131819
39	0	17.800	-9.75	968.4	0.530	0.59168	2.89916	-122695	1060.3	0.570	0.78917	5.71774	-122660	1102.8	1.588	0.42523	6.45023	-131819
40	0	18.300	-1.00	958.4	0.490	0.57932	2.76168	-125995	1054.3	0.530	0.78917	5.71774	-125960	1098.8	1.596	0.40523	6.45023	-131819
41	0	18.800	-1.25	948.4	0.450	0.56696	2.62420	-129295	1048.3	0.490	0.78917	5.71774	-129260	1094.8	1.604	0.38523	6.45023	-131819
42	0	19.300	-1.50	938.4	0.410	0.55460	2.48672	-132595	1042.3	0.450	0.78917	5.71774	-132560	1090.8	1.612	0.36523	6.45023	-131819
43	0	19.800	-1.75	928.4	0.370	0.54224	2.34924	-135895	1036.3	0.410	0.78917	5.71774	-135860	1086.8	1.620	0.34523	6.45023	-131819
44	0	20.300	-2.00	918.4	0.330	0.52988	2.21176	-139195	1030.3	0.370	0.78917	5.71774	-139160	1082.8	1.628	0.32523	6.45023	-131819
45	0	20.800	-2.25	908.4	0.290	0.51752	2.07428	-142495	1024.3	0.290	0.78917	5.71774	-142460	1078.8	1.636	0.30523	6.45023	-131819

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE IX.- DATA^a FOR 180° CONE; $M_{\infty} = 2.30$ - Continued

(c) $\alpha = 10^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ, P_t = 2292.3 \text{ psf}$				$\phi = 90.0^\circ, P_t = 2290.8 \text{ psf}$			
				P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t
1	0	0.300	0.000	1319.2	1.673	0.8663	1.3882	1321.0	1.677	0.8650	1.2806
2	0	0.400	0.000	1317.6	1.671	0.8543	1.4494	1321.0	1.677	0.8660	1.2806
3	0	0.500	0.000	1317.6	1.671	0.8543	1.4494	1321.0	1.677	0.8660	1.2806
4	0	0.600	0.000	1314.4	1.666	0.8304	1.5650	1321.0	1.677	0.8660	1.2806
5	0	0.800	0.000	1312.8	1.664	0.8185	1.6172	1321.0	1.677	0.8660	1.2806
6	0	1.000	0.000	1308.0	1.650	0.7948	1.7766	1314.2	1.670	0.8502	1.1470
7	0	1.500	0.000	1303.2	1.635	0.7729	1.9175	1314.2	1.665	0.8263	1.1470
8	0	2.000	0.000	1293.7	1.616	0.7511	2.0075	1305.8	1.661	0.8024	1.1470
9	0	2.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
10	0	3.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
11	0	3.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
12	0	4.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
13	0	4.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
14	0	5.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
15	0	5.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
16	0	6.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
17	0	6.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
18	0	7.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
19	0	7.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
20	0	8.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
21	0	8.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
22	0	9.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
23	0	9.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
24	0	10.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
25	0	10.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
26	0	11.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
27	0	11.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
28	0	12.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
29	0	12.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
30	0	13.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
31	0	13.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
32	0	14.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
33	0	14.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
34	0	15.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
35	0	15.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
36	0	16.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
37	0	16.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
38	0	17.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
39	0	17.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
40	0	18.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
41	0	18.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
42	0	19.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
43	0	19.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
44	0	20.000	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470
45	0	20.500	0.000	1288.9	1.604	0.7385	2.1772	1305.8	1.656	0.8024	1.1470

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE IX.- DATA^a FOR 180° CONE; $M_{\infty} = 2.30$ - Continued(d) $\alpha = 15^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0, 0^\circ, p_t = 2290.8 \text{ psf}$			
				p_{t1} , psf	C_p	$p_t/p_{t\infty, 2}$	M_t
1	0	.000	.0000	1302.2	1.650	.97455	7.10814
2	.230	.025	.0500	1297.4	1.642	.97096	7.08194
3	.460	.050	.1000	1292.6	1.633	.96517	7.04701
4	.690	.075	.1500	1287.8	1.624	.95818	6.99816
5	.920	.100	.2000	1278.6	1.612	.95540	6.96842
6	1.150	.125	.2500	1273.2	1.602	.95061	6.93349
7	1.380	.150	.3000	1263.8	1.593	.94582	6.89856
8	1.610	.175	.3500	1254.2	1.584	.93983	6.86416
9	1.840	.200	.4000	1244.5	1.577	.93284	6.83089
10	2.070	.225	.4500	1235.0	1.550	.92427	6.74139
11	2.300	.250	.5000	1225.4	1.536	.91738	6.68498
12	2.530	.275	.5500	1212.6	1.517	.90751	6.61912
13	2.760	.300	.6000	1198.2	1.496	.89873	6.54053
14	2.990	.325	.6500	1182.2	1.474	.89184	6.45111
15	3.220	.350	.7000	1164.6	1.447	.87159	6.35715
16	3.450	.375	.7500	1143.8	1.416	.85003	6.24363
17	3.680	.400	.8000	1116.6	1.376	.83567	6.09518
18	3.910	.425	.8500	1084.9	1.329	.81173	5.9412
19	4.140	.450	.9000	1048.1	1.268	.78116	5.7827
20	4.370	.475	.9500	999.5	1.199	.72553	5.59189
21	4.600	.500	1.0000	931.2	1.064	.61884	5.16201
22	4.830	.525	1.0500	845.2	0.969	.48423	4.6985
23	5.060	.550	1.1000	745.4	0.873	.38663	4.21893
24	5.290	.575	1.1500	636.9	0.782	.29182	3.7352
25	5.520	.600	1.2000	526.3	0.695	.20981	3.2503
26	5.750	.625	1.2500	419.5	0.650	.15950	2.8466
27	5.980	.650	1.3000	332.7	0.694	.12339	2.5113
28	6.210	.675	1.3500	263.1	0.750	.09978	2.2472
29	6.440	.700	1.4000	219.7	0.809	.08189	2.0509
30	6.670	.725	1.4500	180.7	0.876	.06937	1.9000
31	6.900	.750	1.5000	140.7	0.950	.06037	1.7831
32	7.130	.775	1.5500	100.7	1.033	.05337	1.6931
33	7.360	.800	1.6000	60.7	1.124	.04817	1.6200
34	7.590	.825	1.6500	20.7	1.224	.04417	1.5612
35	7.820	.850	1.7000	0.0	1.334	.04117	1.5162
36	8.050	.875	1.7500	0.0	1.454	.03817	1.4812
37	8.280	.900	1.8000	0.0	1.584	.03517	1.4512
38	8.510	.925	1.8500	0.0	1.724	.03217	1.4262
39	8.740	.950	1.9000	0.0	1.874	.02917	1.4062
40	8.970	.975	1.9500	0.0	2.034	.02617	1.3912
41	9.200	1.000	2.0000	0.0	2.204	.02317	1.3762
42	9.430	1.025	2.0500	0.0	2.384	.02017	1.3612
43	9.660	1.050	2.1000	0.0	2.574	.01717	1.3462
44	9.890	1.075	2.1500	0.0	2.774	.01417	1.3312
45	10.120	1.100	2.2000	0.0	2.984	.01117	1.3162

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE IX. - DATA^a FOR 180° CONE; $M_{\infty} = 2.30$ - Continued

(e) $\alpha = 20^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0.0^\circ, P_t = 2289.8 \text{ psf}$					$\Phi = 22.5^\circ, P_t = 2291.1 \text{ psf}$					$\Phi = 45.0^\circ, P_t = 2291.6 \text{ psf}$					
				$P_t/\rho a$	C_p	$P_t/P_{t,2}$	M_t	$P_t/\rho a$	C_p	$P_t/P_{t,2}$	M_t	$P_t/\rho a$	C_p	$P_t/P_{t,2}$	M_t	$P_t/\rho a$	C_p	$P_t/P_{t,2}$	M_t
1	0	-0.00	+0.000	1270.3	1.603	.95110	-2.6859	6.93706	1.602	.95102	-2.6859	6.93706	1.602	.95102	-2.6859	6.93706	1.602	.95102	-2.6859
2	0	-0.25	+0.000	1265.5	1.596	.94751	-2.7881	6.91088	1.595	.94743	-2.7881	6.91088	1.595	.94743	-2.7881	6.91088	1.595	.94743	-2.7881
3	0	-0.50	+0.000	1261.1	1.597	.94772	-2.9151	6.87598	1.586	.94725	-2.9151	6.87598	1.586	.94725	-2.9151	6.87598	1.586	.94725	-2.9151
4	0	-0.75	+0.000	1256.9	1.567	.94274	-3.0697	6.81235	1.586	.94274	-3.0697	6.81235	1.586	.94274	-3.0697	6.81235	1.586	.94274	-3.0697
5	0	-1.00	+0.000	1253.2	1.563	.93776	-3.2392	6.72637	1.574	.93627	-3.2392	6.72637	1.574	.93627	-3.2392	6.72637	1.574	.93627	-3.2392
6	0	-1.25	+0.000	1250.0	1.549	.93258	-3.4259	6.62074	1.564	.93149	-3.4259	6.62074	1.564	.93149	-3.4259	6.62074	1.564	.93149	-3.4259
7	0	-1.50	+0.000	1247.6	1.537	.92760	-3.6266	6.49274	1.543	.92551	-3.6266	6.49274	1.543	.92551	-3.6266	6.49274	1.543	.92551	-3.6266
8	0	-1.75	+0.000	1245.6	1.523	.92282	-3.8453	6.34675	1.531	.92038	-3.8453	6.34675	1.531	.92038	-3.8453	6.34675	1.531	.92038	-3.8453
9	0	-2.00	+0.000	1244.0	1.511	.91844	-4.0864	6.19577	1.515	.91538	-4.0864	6.19577	1.515	.91538	-4.0864	6.19577	1.515	.91538	-4.0864
10	0	-2.25	+0.000	1242.9	1.495	.91428	-4.3493	6.04078	1.499	.91101	-4.3493	6.04078	1.499	.91101	-4.3493	6.04078	1.499	.91101	-4.3493
11	0	-2.50	+0.000	1242.0	1.476	.91034	-4.6277	5.88123	1.482	.90698	-4.6277	5.88123	1.482	.90698	-4.6277	5.88123	1.482	.90698	-4.6277
12	0	-2.75	+0.000	1241.5	1.450	.90661	-4.9248	5.72675	1.462	.90336	-4.9248	5.72675	1.462	.90336	-4.9248	5.72675	1.462	.90336	-4.9248
13	0	-3.00	+0.000	1241.5	1.436	.90238	-5.2316	5.57884	1.448	.90002	-5.2316	5.57884	1.448	.90002	-5.2316	5.57884	1.448	.90002	-5.2316
14	0	-3.25	+0.000	1241.5	1.415	.89848	-5.5412	5.43734	1.466	.89848	-5.5412	5.43734	1.466	.89848	-5.5412	5.43734	1.466	.89848	-5.5412
15	0	-3.50	+0.000	1241.5	1.387	.89484	-5.8448	5.30212	1.445	.89484	-5.8448	5.30212	1.445	.89484	-5.8448	5.30212	1.445	.89484	-5.8448
16	0	-3.75	+0.000	1241.5	1.354	.89140	-6.1412	5.17247	1.421	.89140	-6.1412	5.17247	1.421	.89140	-6.1412	5.17247	1.421	.89140	-6.1412
17	0	-4.00	+0.000	1241.5	1.318	.88812	-6.4316	5.04401	1.395	.88812	-6.4316	5.04401	1.395	.88812	-6.4316	5.04401	1.395	.88812	-6.4316
18	0	-4.25	+0.000	1241.5	1.276	.88504	-6.7166	4.91954	1.375	.88504	-6.7166	4.91954	1.375	.88504	-6.7166	4.91954	1.375	.88504	-6.7166
19	0	-4.50	+0.000	1241.5	1.234	.88216	-7.0000	4.79884	1.355	.88216	-7.0000	4.79884	1.355	.88216	-7.0000	4.79884	1.355	.88216	-7.0000
20	0	-4.75	+0.000	1241.5	1.191	.87948	-7.2828	4.68275	1.335	.87948	-7.2828	4.68275	1.335	.87948	-7.2828	4.68275	1.335	.87948	-7.2828
21	0	-5.00	+0.000	1241.5	1.149	.87690	-7.5656	4.57184	1.315	.87690	-7.5656	4.57184	1.315	.87690	-7.5656	4.57184	1.315	.87690	-7.5656
22	0	-5.25	+0.000	1241.5	1.107	.87442	-7.8484	4.46594	1.295	.87442	-7.8484	4.46594	1.295	.87442	-7.8484	4.46594	1.295	.87442	-7.8484
23	0	-5.50	+0.000	1241.5	1.065	.87204	-8.1312	4.36207	1.275	.87204	-8.1312	4.36207	1.275	.87204	-8.1312	4.36207	1.275	.87204	-8.1312
24	0	-5.75	+0.000	1241.5	1.023	.86976	-8.4140	4.26020	1.255	.86976	-8.4140	4.26020	1.255	.86976	-8.4140	4.26020	1.255	.86976	-8.4140
25	0	-6.00	+0.000	1241.5	0.981	.86758	-8.6968	4.16033	1.235	.86758	-8.6968	4.16033	1.235	.86758	-8.6968	4.16033	1.235	.86758	-8.6968
26	0	-6.25	+0.000	1241.5	0.939	.86540	-8.9796	4.06246	1.215	.86540	-8.9796	4.06246	1.215	.86540	-8.9796	4.06246	1.215	.86540	-8.9796
27	0	-6.50	+0.000	1241.5	0.897	.86322	-9.2624	3.96659	1.195	.86322	-9.2624	3.96659	1.195	.86322	-9.2624	3.96659	1.195	.86322	-9.2624
28	0	-6.75	+0.000	1241.5	0.855	.86104	-9.5452	3.87272	1.175	.86104	-9.5452	3.87272	1.175	.86104	-9.5452	3.87272	1.175	.86104	-9.5452
29	0	-7.00	+0.000	1241.5	0.813	.85886	-9.8280	3.78085	1.155	.85886	-9.8280	3.78085	1.155	.85886	-9.8280	3.78085	1.155	.85886	-9.8280
30	0	-7.25	+0.000	1241.5	0.771	.85668	-10.1108	3.69098	1.135	.85668	-10.1108	3.69098	1.135	.85668	-10.1108	3.69098	1.135	.85668	-10.1108
31	0	-7.50	+0.000	1241.5	0.729	.85450	-10.3936	3.60311	1.115	.85450	-10.3936	3.60311	1.115	.85450	-10.3936	3.60311	1.115	.85450	-10.3936
32	0	-7.75	+0.000	1241.5	0.687	.85232	-10.6764	3.51724	1.095	.85232	-10.6764	3.51724	1.095	.85232	-10.6764	3.51724	1.095	.85232	-10.6764
33	0	-8.00	+0.000	1241.5	0.645	.85014	-10.9592	3.43337	1.075	.85014	-10.9592	3.43337	1.075	.85014	-10.9592	3.43337	1.075	.85014	-10.9592
34	0	-8.25	+0.000	1241.5	0.603	.84796	-11.2420	3.35150	1.055	.84796	-11.2420	3.35150	1.055	.84796	-11.2420	3.35150	1.055	.84796	-11.2420
35	0	-8.50	+0.000	1241.5	0.561	.84578	-11.5248	3.27163	1.035	.84578	-11.5248	3.27163	1.035	.84578	-11.5248	3.27163	1.035	.84578	-11.5248
36	0	-8.75	+0.000	1241.5	0.519	.84360	-11.8076	3.19376	1.015	.84360	-11.8076	3.19376	1.015	.84360	-11.8076	3.19376	1.015	.84360	-11.8076
37	0	-9.00	+0.000	1241.5	0.477	.84142	-12.0904	3.11789	0.995	.84142	-12.0904	3.11789	0.995	.84142	-12.0904	3.11789	0.995	.84142	-12.0904
38	0	-9.25	+0.000	1241.5	0.435	.83924	-12.3732	3.04402	0.975	.83924	-12.3732	3.04402	0.975	.83924	-12.3732	3.04402	0.975	.83924	-12.3732
39	0	-9.50	+0.000	1241.5	0.393	.83706	-12.6560	2.97215	0.955	.83706	-12.6560	2.97215	0.955	.83706	-12.6560	2.97215	0.955	.83706	-12.6560
40	0	-9.75	+0.000	1241.5	0.351	.83488	-12.9388	2.90228	0.935	.83488	-12.9388	2.90228	0.935	.83488	-12.9388	2.90228	0.935	.83488	-12.9388
41	0	-10.00	+0.000	1241.5	0.309	.83270	-13.2216	2.83441	0.915	.83270	-13.2216	2.83441	0.915	.83270	-13.2216	2.83441	0.915	.83270	-13.2216
42	0	-10.25	+0.000	1241.5	0.267	.83052	-13.5044	2.76854	0.895	.83052	-13.5044	2.76854	0.895	.83052	-13.5044	2.76854	0.895	.83052	-13.5044
43	0	-10.50	+0.000	1241.5	0.225	.82834	-13.7872	2.70467	0.875	.82834	-13.7872	2.70467	0.875	.82834	-13.7872	2.70467	0.875	.82834	-13.7872
44	0	-10.75	+0.000	1241.5	0.183	.82616	-14.0700	2.64280	0.855	.82616	-14.0700	2.64280	0.855	.82616	-14.0700	2.64280	0.855	.82616	-14.0700
45	0	-11.00	+0.000	1241.5	0.141	.82400	-14.3528	2.58293	0.835	.82400	-14.3528	2.58293	0.835	.82400	-14.3528	2.58293	0.835	.82400	-14.3528

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE IX.- DATA^a FOR 180° CONE; $M_{\infty} = 2.30$ - Concluded(e) $\alpha = 20^\circ$ - Concluded

Orifice ϕ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ$, $p_t = 2290.8$ psf				$\phi = 90.0^\circ$, $p_t = 2291.8$ psf			
				p_t , psf	C_p	$p_t/p_{t,2}$	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	M_t
1	0	.300	.0000	1273.3	1.407	.95287	.26351	1269.9	1.601	.94994	.27187
2	0	.420	.0050	1270.1	1.402	.95048	.27033	1269.9	1.601	.94994	.27187
3	0	.540	.0100	1268.5	1.400	.94929	.27368	1269.9	1.601	.94994	.27187
4	0	.660	.0150	1265.3	1.595	.94590	.28076	1268.3	1.599	.94874	.27187
5	0	.800	.0200	1252.1	1.590	.94092	.30850	1265.1	1.594	.94396	.27187
6	0	1.000	.0250	1230.9	1.574	.93614	.33036	1258.7	1.585	.94157	.27187
7	0	1.200	.0300	1200.9	1.564	.93135	.35308	1253.9	1.577	.93799	.27187
8	0	1.400	.0350	1174.5	1.557	.92777	.37669	1242.1	1.570	.93440	.27187
9	0	1.600	.0400	1151.7	1.546	.92481	.39990	1236.3	1.561	.93202	.27187
10	0	1.800	.0450	1131.7	1.536	.92181	.42308	1231.0	1.552	.93081	.27187
11	0	2.000	.0500	1114.7	1.522	.91883	.44610	1228.8	1.545	.92965	.27187
12	0	2.200	.0550	1101.0	1.503	.91507	.46909	1228.8	1.537	.92855	.27187
13	0	2.400	.0600	1091.8	1.487	.91190	.49206	1228.8	1.529	.92750	.27187
14	0	2.600	.0650	1085.2	1.481	.90927	.51503	1228.8	1.521	.92649	.27187
15	0	2.800	.0700	1079.0	1.477	.90679	.53800	1228.8	1.513	.92552	.27187
16	0	3.000	.0750	1073.6	1.474	.90446	.56097	1228.8	1.506	.92459	.27187
17	0	3.200	.0800	1068.4	1.362	.89766	.58394	1228.8	1.498	.92370	.27187
18	0	3.400	.0850	1064.0	1.298	.89285	.60691	1228.8	1.490	.92285	.27187
19	0	3.600	.0900	1060.0	1.288	.88845	.62988	1228.8	1.482	.92202	.27187
20	0	3.800	.0950	1056.0	1.284	.88466	.65285	1228.8	1.474	.92120	.27187
21	180	.200	.0000	1278.6	1.616	.95766	.24938	1271.5	1.603	.94994	.27187
22	180	.400	.0050	1281.2	1.619	.95885	.25298	1271.5	1.603	.94994	.27187
23	180	.600	.0100	1281.2	1.619	.95885	.25658	1271.5	1.603	.94994	.27187
24	180	.800	.0150	1281.2	1.619	.95885	.26018	1271.5	1.603	.94994	.27187
25	180	1.000	.0200	1281.2	1.619	.95885	.26378	1271.5	1.603	.94994	.27187
26	180	1.200	.0250	1281.2	1.619	.95885	.26738	1271.5	1.603	.94994	.27187
27	180	1.400	.0300	1281.2	1.619	.95885	.27098	1271.5	1.603	.94994	.27187
28	180	1.600	.0350	1281.2	1.619	.95885	.27458	1271.5	1.603	.94994	.27187
29	180	1.800	.0400	1281.2	1.619	.95885	.27818	1271.5	1.603	.94994	.27187
30	180	2.000	.0450	1281.2	1.619	.95885	.28178	1271.5	1.603	.94994	.27187
31	180	2.200	.0500	1281.2	1.619	.95885	.28538	1271.5	1.603	.94994	.27187
32	180	2.400	.0550	1281.2	1.619	.95885	.28898	1271.5	1.603	.94994	.27187
33	180	2.600	.0600	1281.2	1.619	.95885	.29258	1271.5	1.603	.94994	.27187
34	180	2.800	.0650	1281.2	1.619	.95885	.29618	1271.5	1.603	.94994	.27187
35	180	3.000	.0700	1281.2	1.619	.95885	.30000	1271.5	1.603	.94994	.27187
36	180	3.200	.0750	1281.2	1.619	.95885	.30360	1271.5	1.603	.94994	.27187
37	180	3.400	.0800	1281.2	1.619	.95885	.30720	1271.5	1.603	.94994	.27187
38	180	3.600	.0850	1281.2	1.619	.95885	.31080	1271.5	1.603	.94994	.27187
39	180	3.800	.0900	1281.2	1.619	.95885	.31440	1271.5	1.603	.94994	.27187
40	270	1.000	.0250	1302.0	1.680	.96932	.33188	1303.4	1.686	.97503	.27187
41	270	1.200	.0300	1302.0	1.680	.96932	.33548	1303.4	1.686	.97503	.27187
42	270	1.400	.0350	1302.0	1.680	.96932	.33908	1303.4	1.686	.97503	.27187
43	270	1.600	.0400	1302.0	1.680	.96932	.34268	1303.4	1.686	.97503	.27187
44	270	1.800	.0450	1302.0	1.680	.96932	.34628	1303.4	1.686	.97503	.27187
45	270	2.000	.0500	1302.0	1.680	.96932	.34988	1303.4	1.686	.97503	.27187

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

(a) $\alpha = 0^\circ$

²Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE X. - DATA^a FOR 180° CONE; $M_{\infty} = 2.96$ - Continued(a) $\alpha = 0^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ$, $P_t = 3241.3$ psf				$\phi = 90.0^\circ$, $P_t = 3238.1$ psf			
				P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t
1	0	.000	.0000	1088.9	1.732	.98867	.1162044	1088.3	1.734	.99000	.1163608
2	0	.230	.0025	1320.5	1.734	.99013	.1162140	1089.3	1.734	.99000	.1163608
3	0	.430	.0050	1088.9	1.734	.98867	.1162044	1089.3	1.734	.99000	.1163608
4	0	.630	.0075	1088.9	1.732	.98867	.1162044	1089.3	1.734	.99000	.1163608
5	0	.830	.0100	1088.9	1.732	.98867	.1162044	1089.3	1.734	.99000	.1163608
6	0	1.030	.0125	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
7	0	1.230	.0150	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
8	0	1.430	.0175	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
9	0	1.630	.0200	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
10	0	1.830	.0225	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
11	0	2.030	.0250	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
12	0	2.230	.0275	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
13	0	2.430	.0300	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
14	0	2.630	.0325	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
15	0	2.830	.0350	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
16	0	3.030	.0375	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
17	0	3.230	.0400	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
18	0	3.430	.0425	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
19	0	3.630	.0450	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
20	0	3.830	.0475	1088.9	1.729	.98822	.1160338	1087.5	1.734	.98865	.1163608
21	180	.000	.0000	1088.9	1.732	.98867	.1162044	1088.3	1.734	.99000	.1163608
22	180	.230	.0025	1088.9	1.734	.99013	.1162140	1089.3	1.734	.99000	.1163608
23	180	.430	.0050	1088.9	1.734	.98867	.1162044	1089.3	1.734	.99000	.1163608
24	180	.630	.0075	1088.9	1.734	.98867	.1162044	1089.3	1.734	.99000	.1163608
25	180	.830	.0100	1088.9	1.734	.98867	.1162044	1089.3	1.734	.99000	.1163608
26	180	1.030	.0125	1088.9	1.732	.98867	.1162044	1089.3	1.734	.99000	.1163608
27	180	1.230	.0150	1088.9	1.727	.98813	.1159050	1087.5	1.734	.99000	.1163608
28	180	1.430	.0175	1088.9	1.721	.98323	.1155641	1086.1	1.731	.98855	.1161901
29	180	1.630	.0200	1088.9	1.716	.98038	.1152641	1085.1	1.729	.98710	.1159783
30	180	1.830	.0225	1088.9	1.716	.98038	.1152641	1085.1	1.729	.98710	.1159783
31	180	2.030	.0250	1088.9	1.716	.98038	.1152641	1085.1	1.729	.98710	.1159783
32	180	2.230	.0275	1088.9	1.699	.97162	.1142005	1083.3	1.706	.97549	.1149598
33	180	2.430	.0300	1088.9	1.677	.96002	.1131887	1081.5	1.688	.97113	.1146524
34	180	2.630	.0325	1088.9	1.666	.95407	.1128479	1080.6	1.682	.96922	.1144621
35	180	2.830	.0350	1088.9	1.666	.95407	.1128479	1080.6	1.682	.96922	.1144621
36	180	3.030	.0375	1088.9	1.621	.93102	.1094279	1076.5	1.620	.95957	.1137530
37	180	3.230	.0400	1088.9	1.591	.91507	.1075530	1072.5	1.568	.94275	.1127778
38	180	3.430	.0425	1088.9	1.549	.88461	.1047670	1067.5	1.548	.92801	.1117588
39	180	3.630	.0450	1088.9	1.519	.85948	.1025989	1062.5	1.531	.90555	.1107304
40	180	3.830	.0475	1088.9	1.496	.83825	.1007630	1057.5	1.516	.88481	.1097030
41	270	2.030	.0250	1088.9	1.735	.99048	.1164163	1089.3	1.734	.99000	.1163608
42	270	2.230	.0275	1088.9	1.707	.97557	.1147118	1087.5	1.716	.98710	.1159783
43	90	1.030	.0125	1088.9	1.642	.95892	.1137530	1085.1	1.620	.95957	.1137530
44	90	2.030	.0250	1088.9	1.606	.93950	.1119861	1082.5	1.598	.93102	.1117588
45	90	3.030	.0375	1088.9	1.615	.92770	.1090376	1078.5	1.620	.93049	.1107304

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE X.- DATA^a FOR 180° CONE; $M_{\infty} = 2.96$ - Continued

(b) $\alpha = 5^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ, P_t = 3244.2$ psf					$\Phi = 22.5^\circ, P_t = 3242.8$ psf					$\Phi = 45.0^\circ, P_t = 3244.1$ psf					
				P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t
1	0	.300	.0000	1384.3	1.722	.98359	11.56070	1384.5	1.723	.98322	11.56810	1084.5	1.722	.98383	11.56346	1084.5	1.722	.98383	11.56346
2	0	.400	.0500	1082.7	1.719	.98214	11.54367	1082.9	1.720	.98177	11.55403	1082.9	1.720	.98240	11.55463	1082.9	1.720	.98240	11.55463
3	0	.500	.1000	1079.5	1.714	.97924	11.50862	1079.7	1.715	.97987	11.51699	1079.7	1.715	.98050	11.51759	1079.7	1.715	.98050	11.51759
4	0	.600	.1500	1074.7	1.705	.97450	11.45859	1074.9	1.712	.97882	11.47882	1074.9	1.712	.97945	11.47945	1074.9	1.712	.97945	11.47945
5	0	.700	.2000	1069.7	1.697	.97055	11.40746	1069.9	1.706	.97252	11.43588	1069.9	1.706	.97325	11.43651	1069.9	1.706	.97325	11.43651
6	0	.800	.2500	1064.9	1.691	.96766	11.37341	1065.1	1.695	.96973	11.39773	1065.1	1.695	.97046	11.40805	1065.1	1.695	.97046	11.40805
7	0	.900	.3000	1060.7	1.683	.96531	11.34233	1060.9	1.679	.96524	11.33809	1060.9	1.679	.96597	11.34842	1060.9	1.679	.96597	11.34842
8	0	1.000	.3500	1056.9	1.676	.96317	11.31371	1057.1	1.676	.96311	11.31247	1057.1	1.676	.96384	11.32280	1057.1	1.676	.96384	11.32280
9	0	1.100	.4000	1053.6	1.668	.96104	11.28705	1053.8	1.671	.96124	11.28776	1053.8	1.671	.96197	11.29809	1053.8	1.671	.96197	11.29809
10	0	1.200	.4500	1050.8	1.664	.95917	11.26215	1051.0	1.674	.95900	11.26286	1051.0	1.674	.95973	11.27319	1051.0	1.674	.95973	11.27319
11	0	1.300	.5000	1048.8	1.650	.95693	11.11802	1049.0	1.684	.95675	11.11873	1049.0	1.684	.95748	11.12846	1049.0	1.684	.95748	11.12846
12	0	1.400	.5500	1046.8	1.636	.95468	11.03289	1047.0	1.699	.95461	11.03360	1047.0	1.699	.95534	11.04333	1047.0	1.699	.95534	11.04333
13	0	1.500	.6000	1044.8	1.623	.95254	10.91371	1045.0	1.716	.95247	10.91442	1045.0	1.716	.95320	10.92415	1045.0	1.716	.95320	10.92415
14	0	1.600	.6500	1042.8	1.616	.95040	10.80720	1043.0	1.731	.95033	10.80791	1043.0	1.731	.95106	10.81764	1043.0	1.731	.95106	10.81764
15	0	1.700	.7000	1040.9	1.594	.94826	10.70215	1041.1	1.746	.94818	10.70286	1041.1	1.746	.94891	10.71259	1041.1	1.746	.94891	10.71259
16	0	1.800	.7500	1039.9	1.586	.94611	10.61095	1040.1	1.761	.94604	10.61166	1040.1	1.761	.94677	10.62139	1040.1	1.761	.94677	10.62139
17	0	1.900	.8000	1038.9	1.576	.94397	10.52260	1039.1	1.776	.94389	10.52331	1039.1	1.776	.94462	10.53304	1039.1	1.776	.94462	10.53304
18	0	2.000	.8500	1037.9	1.566	.94182	10.43720	1038.1	1.791	.94174	10.43791	1038.1	1.791	.94247	10.54264	1038.1	1.791	.94247	10.54264
19	0	2.100	.9000	1036.9	1.556	.93967	10.35475	1037.1	1.806	.93959	10.35546	1037.1	1.806	.94032	10.55237	1037.1	1.806	.94032	10.55237
20	0	2.200	.9500	1035.9	1.547	.93752	10.27420	1036.1	1.821	.93744	10.27491	1036.1	1.821	.93815	10.56208	1036.1	1.821	.93815	10.56208
21	180	.025	.0500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
22	180	.050	.1000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
23	180	.075	.1500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
24	180	.100	.2000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
25	180	.125	.2500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
26	180	.150	.3000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
27	180	.175	.3500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
28	180	.200	.4000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
29	180	.225	.4500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
30	180	.250	.5000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
31	180	.275	.5500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
32	180	.300	.6000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
33	180	.325	.6500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
34	180	.350	.7000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
35	180	.375	.7500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
36	180	.400	.8000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
37	180	.425	.8500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
38	180	.450	.9000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
39	180	.475	.9500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
40	180	.500	.1000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
41	270	.025	.0500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
42	270	.050	.1000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
43	270	.075	.1500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
44	270	.100	.2000	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705
45	270	.125	.2500	1092.3	1.736	.99083	11.64583	1092.5	1.737	.99046	11.65644	1092.5	1.737	.99109	11.66705	1092.5	1.737	.99109	11.66705

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE X. - DATA^a FOR 180° CONE; $M_{\infty} = 2.96$ - Continued(b) $\alpha = 5^\circ$ - Concluded

Orifice 1	θ , deg	s , in.	s/D	s/s^*	$\Phi = 67.5^\circ, p_t = 3240.9 \text{ psf}$				$\Phi = 90.0^\circ, p_t = 3243.0 \text{ psf}$			
					p_t , psf	C_p	$p_t/p_{t,2}$	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	M_t
1	0	0.300	0.000	0.000	1384.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
2	0	0.400	0.025	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
3	0	0.500	0.050	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
4	0	0.600	0.075	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
5	0	0.800	0.100	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
6	0	1.000	0.125	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
7	0	1.200	0.150	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
8	0	1.400	0.175	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
9	0	1.600	0.200	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
10	0	1.800	0.225	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
11	0	2.000	0.250	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
12	0	2.200	0.275	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
13	0	2.400	0.300	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
14	0	2.600	0.325	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
15	0	2.800	0.350	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
16	0	3.000	0.375	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
17	0	3.200	0.400	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
18	0	3.400	0.425	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
19	0	3.600	0.450	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
20	0	3.800	0.475	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
21	180	0.200	0.025	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
22	180	0.300	0.050	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
23	180	0.400	0.075	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
24	180	0.500	0.100	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
25	180	0.600	0.125	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
26	180	0.800	0.150	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
27	180	1.000	0.175	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
28	180	1.200	0.200	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
29	180	1.400	0.225	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
30	180	1.600	0.250	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
31	180	1.800	0.275	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
32	180	2.000	0.300	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
33	180	2.200	0.325	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
34	180	2.400	0.350	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
35	180	2.600	0.375	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
36	180	2.800	0.400	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
37	180	3.000	0.425	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
38	180	3.200	0.450	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
39	180	3.400	0.475	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
40	270	1.000	0.125	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
41	270	2.000	0.250	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
42	270	3.000	0.375	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
43	90	2.000	0.250	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
44	90	3.000	0.375	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319
45	90	3.000	0.375	0.000	1084.1	1.724	0.9444	11.57068	1084.5	1.723	0.9416	11.57319

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE X. - DATA^a FOR 180° CONE; $M_{\infty} = 2.96$ - Continued

(c) $\alpha = 10^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ, P_t = 3243.9$ psf				$\Phi = 22.5^\circ, P_t = 3241.1$ psf				$\Phi = 45.0^\circ, P_t = 3238.0$ psf						
				$P_{t,2}$	C_p	$P_t/P_{t,2}$	P_t/β_{∞}	$M_{t,2}$	$P_{t,2}$ psf	C_p	$P_t/P_{t,2}$	P_t/β_{∞}	$M_{t,2}$	$P_{t,2}$ psf	C_p	$P_t/P_{t,2}$	P_t/β_{∞}	$M_{t,2}$
1	0	-0.20	-0.003	1076.2	1.708	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
2	0	-0.25	-0.003	1076.2	1.703	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
3	0	-0.30	-0.003	1076.2	1.698	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
4	0	-0.35	-0.003	1076.2	1.693	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
5	0	-0.40	-0.003	1076.2	1.688	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
6	0	-0.45	-0.003	1076.2	1.683	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
7	0	-0.50	-0.003	1076.2	1.678	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
8	0	-0.55	-0.003	1076.2	1.673	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
9	0	-0.60	-0.003	1076.2	1.668	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
10	0	-0.65	-0.003	1076.2	1.663	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
11	0	-0.70	-0.003	1076.2	1.658	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
12	0	-0.75	-0.003	1076.2	1.653	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
13	0	-0.80	-0.003	1076.2	1.648	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
14	0	-0.85	-0.003	1076.2	1.643	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
15	0	-0.90	-0.003	1076.2	1.638	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
16	0	-0.95	-0.003	1076.2	1.633	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
17	0	-1.00	-0.003	1076.2	1.628	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
18	0	-1.05	-0.003	1076.2	1.623	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
19	0	-1.10	-0.003	1076.2	1.618	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
20	0	-1.15	-0.003	1076.2	1.613	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
21	0	-1.20	-0.003	1076.2	1.608	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
22	0	-1.25	-0.003	1076.2	1.603	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
23	0	-1.30	-0.003	1076.2	1.598	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
24	0	-1.35	-0.003	1076.2	1.593	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
25	0	-1.40	-0.003	1076.2	1.588	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
26	0	-1.45	-0.003	1076.2	1.583	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
27	0	-1.50	-0.003	1076.2	1.578	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
28	0	-1.55	-0.003	1076.2	1.573	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
29	0	-1.60	-0.003	1076.2	1.568	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
30	0	-1.65	-0.003	1076.2	1.563	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
31	0	-1.70	-0.003	1076.2	1.558	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
32	0	-1.75	-0.003	1076.2	1.553	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
33	0	-1.80	-0.003	1076.2	1.548	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
34	0	-1.85	-0.003	1076.2	1.543	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
35	0	-1.90	-0.003	1076.2	1.538	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
36	0	-1.95	-0.003	1076.2	1.533	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
37	0	-2.00	-0.003	1076.2	1.528	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
38	0	-2.05	-0.003	1076.2	1.523	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
39	0	-2.10	-0.003	1076.2	1.518	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
40	0	-2.15	-0.003	1076.2	1.513	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
41	0	-2.20	-0.003	1076.2	1.508	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
42	0	-2.25	-0.003	1076.2	1.503	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
43	0	-2.30	-0.003	1076.2	1.498	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
44	0	-2.35	-0.003	1076.2	1.493	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275
45	0	-2.40	-0.003	1076.2	1.488	0.9137	11.4793	1.6515	1076.1	1.710	0.9712	11.4864	1.8214	1074.9	1.709	0.9767	11.4828	1.8275

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE X.- DATA^a FOR 180° CONE; $M_{\infty} = 2.96$ - Continued(c) $\alpha = 10^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ$, $P_t = 3240.7$ psf				$\phi = 90.0^\circ$, $P_t = 3239.8$ psf					
				P_t , psf	C_p	$P_t/P_{t,2}$	P_t/P_∞	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	P_t/P_∞	M_t
1	0	.330	.000	1074.5	1.707	.97579	11.46899	18745	1074.9	1.708	.97643	11.47650	18462
2	0	.430	.025	1071.3	1.704	.97433	11.45192	19308	1073.3	1.705	.97498	11.45944	19062
3	0	.530	.050	1068.1	1.699	.97143	11.41779	20391	1073.3	1.705	.97498	11.45944	19062
4	0	.630	.075	1059.7	1.696	.96998	11.40072	20912	1073.3	1.705	.97498	11.45944	19062
5	0	.730	.100	1053.1	1.694	.96852	11.38365	21428	1071.7	1.703	.97353	11.44239	19516
6	0	.830	.125	1046.5	1.689	.96517	11.34618	21940	1068.5	1.694	.96917	11.40521	19816
7	0	.930	.150	1039.9	1.681	.96127	11.30871	22448	1068.5	1.689	.96527	11.36773	20117
8	0	1.030	.175	1033.3	1.671	.95691	11.27124	22952	1063.6	1.689	.96227	11.33023	20419
9	0	1.130	.200	1026.7	1.662	.95256	11.19592	23456	1063.6	1.683	.96337	11.32302	20351
10	0	1.230	.225	1020.1	1.651	.94821	11.12755	23960	1055.8	1.675	.95902	11.27186	20524
11	0	1.330	.250	1013.5	1.640	.94386	11.05938	24464	1051.0	1.666	.95476	11.23544	20780
12	0	1.430	.275	1006.9	1.628	.93951	11.02191	24968	1046.2	1.659	.95016	11.19806	21036
13	0	1.530	.300	1000.3	1.616	.93516	10.87105	25472	1035.4	1.652	.94016	11.150518	21293
14	0	1.630	.325	993.7	1.604	.93081	10.75218	25976	1034.6	1.642	.93145	11.10286	21549
15	0	1.730	.350	987.1	1.592	.92646	10.58895	26480	1032.6	1.630	.92184	11.05519	21805
16	0	1.830	.375	980.5	1.580	.92211	10.39031	26984	1021.6	1.620	.91284	11.00752	22061
17	0	1.930	.400	973.9	1.568	.91776	10.33737	27488	1019.1	1.595	.90383	10.95983	22317
18	0	2.030	.425	967.3	1.556	.91341	10.22831	27992	1016.5	1.587	.89483	10.91229	22573
19	0	2.130	.450	960.7	1.544	.90906	10.15293	28496	1014.9	1.569	.88583	10.86475	22829
20	0	2.230	.475	954.1	1.532	.90471	10.07982	29000	1012.6	1.549	.87682	10.81717	23084
21	0	2.330	.500	947.5	1.520	.90036	9.97948	29504	1010.7	1.533	.86781	10.76959	23340
22	0	2.430	.525	940.9	1.508	.89601	9.91916	30008	1008.7	1.517	.85880	10.72201	23596
23	0	2.530	.550	934.3	1.496	.89166	9.84980	30512	1007.7	1.517	.85078	10.67443	23852
24	0	2.630	.575	927.7	1.484	.88731	9.77545	31016	1005.9	1.511	.84276	10.62685	24108
25	0	2.730	.600	921.1	1.472	.88296	9.70109	31520	1004.5	1.504	.83474	10.57927	24364
26	0	2.830	.625	914.5	1.460	.87861	9.62674	32024	1003.3	1.500	.82672	10.53169	24620
27	0	2.930	.650	907.9	1.448	.87426	9.55238	32528	1001.3	1.495	.81870	10.48411	24876
28	0	3.030	.675	901.3	1.436	.86991	9.47802	33032	1000.0	1.490	.81068	10.43653	25132
29	0	3.130	.700	894.7	1.424	.86556	9.40365	33536	998.9	1.484	.80266	10.38895	25388
30	0	3.230	.725	888.1	1.412	.86121	9.32929	34040	997.9	1.478	.79464	10.34137	25644
31	0	3.330	.750	881.5	1.400	.85686	9.25492	34544	996.9	1.472	.78662	10.29379	25899
32	0	3.430	.775	874.9	1.388	.85251	9.18056	35048	995.9	1.465	.77860	10.24621	26155
33	0	3.530	.800	868.3	1.376	.84816	9.10619	35552	994.9	1.458	.77058	10.19863	26411
34	0	3.630	.825	861.7	1.364	.84381	9.03183	36056	993.9	1.452	.76256	10.15105	26667
35	0	3.730	.850	855.1	1.352	.83946	8.95746	36560	992.9	1.445	.75454	10.10347	26923
36	0	3.830	.875	848.5	1.340	.83511	8.88309	37064	991.9	1.438	.74652	10.05589	27179
37	0	3.930	.900	841.9	1.328	.83076	8.80872	37568	990.9	1.432	.73850	10.00831	27435
38	0	4.030	.925	835.3	1.316	.82641	8.73435	38072	989.9	1.425	.73048	9.96073	27691
39	0	4.130	.950	828.7	1.304	.82206	8.65998	38576	988.9	1.418	.72246	9.91315	27947
40	0	4.230	.975	822.1	1.292	.81771	8.58561	39080	987.9	1.412	.71444	9.86557	28203
41	0	4.330	.100	815.5	1.280	.81336	8.51124	39584	986.9	1.405	.70642	9.81799	28459
42	0	4.430	.125	808.9	1.268	.80901	8.43687	40088	985.9	1.400	.69840	9.77041	28715
43	0	4.530	.150	802.3	1.256	.80466	8.36250	40592	984.9	1.393	.69038	9.72283	28971
44	0	4.630	.175	795.7	1.244	.80031	8.28813	41096	983.9	1.387	.68236	9.67525	29227
45	0	4.730	.200	789.1	1.232	.79596	8.21376	41600	982.9	1.380	.67434	9.62767	29483

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE X. - DATA^a FOR 180° CONE; $M_\infty = 2.96$ - Continued

(d) $\alpha = 15^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, P_t = 3245.1 \text{ psf}$				
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t
1	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
2	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
3	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
4	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
5	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
6	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
7	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
8	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
9	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
10	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
11	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
12	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
13	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
14	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
15	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
16	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
17	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
18	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
19	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
20	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
21	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
22	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
23	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
24	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
25	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
26	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
27	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
28	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
29	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
30	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
31	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
32	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
33	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
34	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
35	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
36	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
37	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
38	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
39	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
40	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
41	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
42	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
43	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
44	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091
45	0	0.000	-0.000	1059.0	1.677	.96041	11.28829	.24091

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE X. - DATA^a FOR 180° CONE; $M_{\infty} = 2.96$ - Continued(e) $\alpha = 20^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\theta = 0.0^\circ, P_t = 3245.2$ psf				$\theta = 22.5^\circ, P_t = 3241.4$ psf				$\theta = 45.0^\circ, P_t = 3240.3$ psf					
				$P_{t,1}$ psf	C_p	$P_{t,1}/P_{t,2}$	$P_{t,1}/P_{t,0}$	$M_{t,1}$	$P_{t,1}$ psf	C_p	$P_{t,1}/P_{t,2}$	$P_{t,1}/P_{t,0}$	$M_{t,1}$	$P_{t,1}$ psf	C_p	$P_{t,1}/P_{t,2}$	$P_{t,1}/P_{t,0}$
1	0	.000	.0000	1036.4	1.638	.93884	11.04651	29903	1036.5	1.640	.94101	11.06023	29966	1.638	.93960	11.04369	29766
2	0	.200	.0025	1030.0	1.627	.93405	10.97831	29718	1031.7	1.632	.93666	11.00910	29510	1.632	.93434	11.00910	29266
3	0	.400	.0075	1025.2	1.619	.92971	10.92346	29484	1028.5	1.624	.93231	10.95198	29266	1.624	.93000	10.95198	28966
4	0	.600	.0100	1020.8	1.611	.92548	10.87124	29248	1025.6	1.613	.92651	10.89581	29022	1.613	.92544	10.89581	28722
5	0	.800	.0125	1016.8	1.604	.92131	10.82124	29008	1022.6	1.604	.92216	10.83668	28778	1.604	.92108	10.83668	28478
6	0	1.000	.0150	1013.2	1.596	.91720	10.77231	28778	1019.7	1.596	.91806	10.79347	28534	1.596	.91700	10.79347	28234
7	0	1.200	.0175	1010.0	1.587	.91314	10.72533	28538	1016.5	1.587	.91399	10.75347	28290	1.587	.91292	10.75347	27990
8	0	1.400	.0200	1006.8	1.578	.90913	10.67933	28300	1013.3	1.579	.90998	10.70347	28042	1.579	.90892	10.70347	27742
9	0	1.600	.0225	1003.6	1.569	.90517	10.63433	28062	1010.1	1.570	.90592	10.65847	27794	1.570	.90496	10.65847	27494
10	0	1.800	.0250	1000.4	1.560	.90126	10.58933	27824	1006.9	1.561	.90201	10.61347	27546	1.561	.90105	10.61347	27246
11	0	2.000	.0275	997.2	1.551	.89739	10.54433	27586	1003.7	1.552	.90016	10.56847	27298	1.552	.89920	10.56847	26998
12	0	2.200	.0300	994.0	1.542	.89356	10.49933	27348	1000.5	1.543	.89601	10.52347	27050	1.543	.89504	10.52347	26750
13	0	2.400	.0325	990.8	1.533	.88973	10.45433	27110	997.3	1.534	.89216	10.47847	26802	1.534	.89118	10.47847	26502
14	0	2.600	.0350	987.6	1.524	.88590	10.40933	26872	994.1	1.525	.88836	10.43247	26554	1.525	.88738	10.43247	26254
15	0	2.800	.0375	984.4	1.515	.88207	10.36433	26634	990.9	1.516	.88453	10.38647	26306	1.516	.88355	10.38647	25996
16	0	3.000	.0400	981.2	1.506	.87824	10.31933	26396	987.7	1.507	.87999	10.34047	26058	1.507	.87901	10.34047	25758
17	0	3.200	.0425	978.0	1.497	.87441	10.27433	26158	984.5	1.498	.87616	10.29547	25810	1.498	.87518	10.29547	25510
18	0	3.400	.0450	974.8	1.488	.87058	10.22933	25920	981.3	1.489	.87231	10.25047	25562	1.489	.87133	10.25047	25262
19	0	3.600	.0475	971.6	1.479	.86675	10.18433	25682	978.1	1.480	.86850	10.20547	25314	1.480	.86752	10.20547	24994
20	0	3.800	.0500	968.4	1.470	.86292	10.13933	25444	974.9	1.471	.86465	10.16047	25066	1.471	.86367	10.16047	24756
21	0	4.000	.0525	965.2	1.461	.85909	10.09433	25206	971.7	1.462	.86080	10.11547	24818	1.462	.85982	10.11547	24518
22	0	4.200	.0550	962.0	1.452	.85526	10.04933	24968	968.5	1.453	.85691	10.07047	24570	1.453	.85593	10.07047	24270
23	0	4.400	.0575	958.8	1.443	.85143	10.00433	24730	965.3	1.444	.85306	10.02547	24322	1.444	.85205	10.02547	24022
24	0	4.600	.0600	955.6	1.434	.84760	9.95933	24492	962.1	1.435	.84921	9.98047	24074	1.435	.84823	9.98047	23774
25	0	4.800	.0625	952.4	1.425	.84377	9.91433	24254	958.9	1.426	.84532	9.93547	23826	1.426	.84434	9.93547	23526
26	0	5.000	.0650	949.2	1.416	.83994	9.86933	24016	955.7	1.417	.84147	9.89047	23578	1.417	.84049	9.89047	23278
27	0	5.200	.0675	946.0	1.407	.83611	9.82433	23778	952.5	1.408	.83800	9.84547	23330	1.408	.83702	9.84547	22990
28	0	5.400	.0700	942.8	1.398	.83228	9.77933	23540	949.3	1.399	.83417	9.79647	23182	1.399	.83319	9.79647	22742
29	0	5.600	.0725	939.6	1.389	.82845	9.73433	23302	946.1	1.390	.83034	9.75347	22934	1.390	.82936	9.75347	22494
30	0	5.800	.0750	936.4	1.380	.82462	9.68933	23064	942.9	1.381	.82653	9.71047	22686	1.381	.82555	9.71047	22246
31	0	6.000	.0775	933.2	1.371	.82079	9.64433	22826	939.7	1.372	.82270	9.67147	22438	1.372	.82172	9.67147	21998
32	0	6.200	.0800	930.0	1.362	.81696	9.59933	22588	936.5	1.363	.81887	9.62847	22190	1.363	.81789	9.62847	21750
33	0	6.400	.0825	926.8	1.353	.81313	9.55433	22350	933.3	1.354	.81508	9.58547	21942	1.354	.81410	9.58547	21502
34	0	6.600	.0850	923.6	1.344	.80930	9.50933	22112	930.1	1.345	.81103	9.54047	21694	1.345	.81005	9.54047	21254
35	0	6.800	.0875	920.4	1.335	.80547	9.46433	21874	926.9	1.336	.80734	9.50147	21446	1.336	.80636	9.50147	20996
36	0	7.000	.0900	917.2	1.326	.80164	9.41933	21636	923.7	1.327	.80347	9.45847	21198	1.327	.80249	9.45847	20748
37	0	7.200	.0925	914.0	1.317	.79781	9.37433	21398	920.5	1.318	.80000	9.41347	20950	1.318	.80000	9.41347	20500
38	0	7.400	.0950	910.8	1.308	.79398	9.32933	21160	917.3	1.309	.79617	9.36847	20702	1.309	.79617	9.36847	20252
39	0	7.600	.0975	907.6	1.299	.79015	9.28433	20922	914.1	1.300	.79236	9.32347	20454	1.300	.79236	9.32347	19994
40	0	7.800	.1000	904.4	1.290	.78632	9.23933	20684	910.9	1.291	.78857	9.27847	20206	1.291	.78857	9.27847	19746
41	0	8.000	.1025	901.2	1.281	.78249	9.19433	20446	907.7	1.282	.78472	9.23347	19958	1.282	.78472	9.23347	19498
42	0	8.200	.1050	898.0	1.272	.77866	9.14933	20208	904.5	1.273	.78096	9.18847	19710	1.273	.78096	9.18847	19250
43	0	8.400	.1075	894.8	1.263	.77483	9.10433	19970	901.3	1.264	.77727	9.14347	19462	1.264	.77727	9.14347	18992
44	0	8.600	.1100	891.6	1.254	.77100	9.05933	19732	898.1	1.255	.77361	9.09847	19214	1.255	.77361	9.09847	18744
45	0	8.800	.1125	888.4	1.245	.76717	9.01433	19494	894.9	1.246	.77000	9.05347	18966	1.246	.77000	9.05347	18496
46	0	9.000	.1150	885.2	1.236	.76334	8.96933	19256	891.7	1.237	.76641	9.00847	18718	1.237	.76641	9.00847	18248
47	0	9.200	.1175	882.0	1.227	.75951	8.92433	19018	888.5	1.228	.76258	8.96347	18470	1.228	.76258	8.96347	17990
48	0	9.400	.1200	878.8	1.218	.75568	8.87933	18780	885.3	1.219	.75975	8.91247	18222	1.219	.75975	8.91247	17742
49	0	9.600	.1225	875.6	1.209	.75185	8.83433	18542	882.1	1.210	.75592	8.86147	17974	1.210	.75592	8.86147	17494
50	0	9.800	.1250	872.4	1.200	.74802	8.78933	18304	878.9	1.201	.75209	8.81047	17726	1.201	.75209	8.81047	17246
51	0	10.000	.1275	869.2	1.191	.74419	8.74433	18066	875.7	1.192	.74816	8.75947	17478	1.192	.74816	8.75947	16998
52	0	10.200	.1300	866.0	1.182	.74036	8.69933	17828	872.5	1.183	.74423	8.71447	17230	1.183	.74423	8.71447	16750
53	0	10.400	.1325	862.8	1.173	.73653	8.65433	17590	869.3	1.174	.74030	8.66947	16982	1.174	.74030	8.66947	16502
54	0	10.600	.1350	859.6	1.164	.73270	8.60933	17352	866.1	1.165	.73637	8.62447	16734	1.165	.73637	8.62447	16254
55	0	10.800	.1375	856.4	1.155	.72887	8.56433	17114	862.9	1.156	.73244	8.57947	16486	1.156	.73244	8.57947	15996
56	0	11.000	.1400	853.2	1.146	.72504	8.51933	16876	859.7	1.147	.72851	8.53447	16238	1.147	.72851	8.53447	15748
57	0	11.200	.1425	850.0	1.137	.72121	8.47433	16638	856.5	1.138	.72458	8.48947	15990	1.138	.72458	8.48947	15490
58	0	11.400	.1450	846.8	1.128	.71738	8.42933	16400	853.3	1.129	.72065	8.44447	15742	1.129	.72065	8.44447	15242
59	0	11.600	.1475	843.6	1.119	.71355	8.38433	16162	850.1	1.120	.71682	8.40047	15494	1.120	.71682	8.40047	14994
60	0	11.800	.1500	840.4	1.110	.70972	8.33933	15924	846.9	1.111	.71309	8.35547	15246	1.111	.71309	8.35547	14746
61	0	12.000	.1525	837.2	1.101	.70589	8.29433	15686	843.7	1.102	.70936	8.31047	15008	1.102	.70936	8.31047	14498
62	0	12.200	.1550	834.0	1.092	.70206	8.24933	15448	840.5	1.093	.70563	8.26547	14760	1.093	.70563	8.26547	14250
63	0	12.400	.1575	830.8	1.083	.69823	8.20433	15210	837.3	1.084	.70190	8.22047	14512	1.084	.70190	8.22047	14002
64	0	12.600	.1600	827.6	1.074	.69440	8.15933	14972	834.1	1.075	.69817	8.17547	14264	1.075	.69817	8.17547	13754
65	0	12.800	.1625	824.4	1.065	.69057	8.11433	14734	830.9	1.066	.69444	8.13047	14016	1.066	.69444	8.13047	13506
66	0	13.000	.1650	821.2	1.056	.68674	8.069										

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE X.- DATA^a FOR 180° CONE; $M_{\infty} = 2.96$ - Concluded

(e) $\alpha = 20^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ, P_t = 3239.6 \text{ psf}$				$\Phi = 90.0^\circ, P_t = 3238.7 \text{ psf}$			
				P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t
1	0	-0.30	-0.000	1034.6	1.638	.9381	-29913	1034.9	1.639	.9404	-29757
2	0	-2.00	.0500	1033.4	1.635	.9385	-30287	1034.9	1.639	.9404	-29757
3	0	-4.00	.1000	1031.4	1.632	.9390	-30657	1034.9	1.639	.9404	-29757
4	0	-6.00	.1500	1029.4	1.629	.9395	-31027	1034.9	1.639	.9404	-29757
5	0	-8.00	.2000	1026.6	1.624	.9395	-31395	1034.9	1.639	.9404	-29757
6	0	-1.00	.2500	1024.6	1.624	.9395	-31765	1034.9	1.639	.9404	-29757
7	0	-1.200	.3000	1021.8	1.616	.92819	-32803	1033.3	1.636	.93896	-30870
8	0	-1.400	.3500	1018.6	1.610	.92828	-33493	1032.1	1.631	.93606	-31234
9	0	-1.600	.4000	1013.8	1.602	.92092	-34508	1028.5	1.628	.93460	-31594
10	0	-1.800	.4500	1008.2	1.594	.91775	-35679	1024.2	1.625	.93315	-31954
11	0	-2.000	.5000	1002.6	1.582	.91075	-36789	1019.0	1.621	.93170	-32314
12	0	-2.200	.5500	996.2	1.571	.90494	-37921	1014.2	1.618	.93025	-32674
13	0	-2.400	.6000	989.8	1.560	.89913	-39071	1009.2	1.615	.92880	-33034
14	0	-2.600	.6500	983.6	1.541	.88997	-40245	1004.2	1.612	.92735	-33394
15	0	-2.800	.7000	977.8	1.504	.87008	-41352	1000.2	1.593	.92590	-33754
16	0	-3.000	.7500	941.8	1.477	.85558	-42505	995.8	1.568	.92445	-34114
17	0	-3.200	.8000	924.2	1.446	.83958	-43671	975.8	1.536	.92299	-34474
18	0	-3.400	.8500	907.2	1.404	.81779	-44852	959.9	1.472	.92154	-34834
19	0	-3.600	.9000	890.2	1.362	.79599	-46055	944.5	1.431	.92009	-35194
20	0	-3.800	.9500	804.3	1.237	.73064	-47279	864.5	1.311	.91864	-35554
21	180	-0.200	-0.025	1044.6	1.655	.94892	-27471	1039.7	1.648	.94476	-28607
22	180	-0.400	.0500	1044.6	1.655	.94892	-27471	1039.7	1.648	.94476	-28607
23	180	-0.600	.1000	1044.6	1.655	.94892	-27471	1039.7	1.648	.94476	-28607
24	180	-0.800	.1500	1044.6	1.655	.94892	-27471	1039.7	1.648	.94476	-28607
25	180	-1.000	.2000	1044.6	1.658	.95037	-27065	1034.9	1.639	.94231	-28994
26	180	-1.200	.2500	1044.6	1.658	.95037	-27065	1034.9	1.639	.94231	-28994
27	180	-1.400	.3000	1047.8	1.661	.95182	-26653	1031.7	1.634	.93996	-30132
28	180	-1.600	.3500	1047.8	1.661	.95182	-26653	1028.5	1.628	.93751	-30503
29	180	-1.800	.4000	1047.8	1.661	.95182	-26653	1024.2	1.621	.93506	-30874
30	180	-2.000	.4500	1046.2	1.658	.95037	-27065	1020.2	1.617	.93261	-31234
31	180	-2.200	.5000	1044.6	1.655	.94892	-27471	1017.4	1.609	.93016	-31594
32	180	-2.400	.5500	1041.4	1.650	.94602	-28268	1011.0	1.597	.92771	-31954
33	180	-2.600	.6000	1038.2	1.643	.94312	-29047	1004.2	1.584	.92526	-32314
34	180	-2.800	.6500	1031.8	1.633	.93712	-30252	998.2	1.547	.92281	-32674
35	180	-3.000	.7000	1023.8	1.619	.93036	-31467	992.7	1.522	.92036	-33034
36	180	-3.200	.7500	1012.6	1.600	.91990	-32682	987.9	1.481	.91791	-33394
37	180	-3.400	.8000	993.5	1.566	.90249	-33857	983.9	1.422	.91546	-33754
38	180	-3.600	.8500	974.6	1.522	.88204	-35032	970.4	1.422	.91301	-34114
39	180	-3.800	.9000	910.4	1.422	.82704	-36207	957.9	1.389	.91056	-34474
40	270	-1.000	.125	1062.2	1.686	.96488	-22957	1053.7	1.689	.96653	-21750
41	270	-1.200	.250	1062.2	1.722	.98374	-15321	1057.6	1.731	.98830	-21097
42	270	-1.400	.375	1050.9	1.736	.99100	-11374	1048.8	1.750	.99446	-20494
43	270	-1.600	.500	1031.4	1.736	.99100	-8325	1034.6	1.566	.91284	-16331
44	90	-2.000	.250	967.4	1.521	.87180	-31416	981.0	1.397	.91016	-18156
45	90	-3.000	.375	901.8	1.407	.81924	-44138	896.0	1.397	.91016	-18156

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XI.- DATA^a FOR 180° CONE; $M_{\infty} = 3.95$ (a) $\alpha = 0^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ, P_t = 5765.1 \text{ psf}$					$\Phi = 22.5^\circ, P_t = 5765.1 \text{ psf}$					$\Phi = 45.0^\circ, P_t = 5765.1 \text{ psf}$				
				P_t , psf	C_p	$P_t/P_{t,2}$	P_t/P_{∞}	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	P_t/P_{∞}	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	P_t/P_{∞}	M_t
1	0	.330	.0000	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
2	0	.230	.0025	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
3	0	.130	.0050	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
4	0	.030	.0075	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
5	0	.800	.100	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
6	0	1.300	.125	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
7	0	1.830	.150	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
8	0	2.360	.175	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
9	0	2.890	.200	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
10	0	3.420	.225	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
11	0	3.950	.250	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
12	0	4.480	.275	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
13	0	5.010	.300	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
14	0	5.540	.325	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
15	0	6.070	.350	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
16	0	6.600	.375	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
17	0	7.130	.400	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
18	0	7.660	.425	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
19	0	8.190	.450	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
20	0	8.720	.475	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763	818.6	1.755	.98058	20.16389	.16763
21	180	.200	.025	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
22	180	.400	.050	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
23	180	.600	.075	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
24	180	.800	.100	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
25	180	1.000	.125	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
26	180	1.200	.150	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
27	180	1.400	.175	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
28	180	1.600	.200	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
29	180	1.800	.225	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
30	180	2.000	.250	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
31	180	2.200	.275	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
32	180	2.400	.300	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
33	180	2.600	.325	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
34	180	2.800	.350	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
35	180	3.000	.375	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
36	180	3.200	.400	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
37	180	3.400	.425	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
38	180	3.600	.450	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
39	180	3.800	.475	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503	825.7	1.771	.98095	20.33821	.16503
40	270	1.030	.125	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523
41	270	1.300	.150	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523
42	270	1.570	.175	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523
43	270	1.840	.200	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523
44	270	2.110	.225	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523
45	270	2.380	.250	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523	820.9	1.748	.98331	20.22019	.15523

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XI.- DATA³ FOR 180° CONE; $M_{\infty} = 3.95$ - Continued

(a) $\alpha = 0^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ, p_t = 5755.6 \text{ psf}$				$\Phi = 90.0^\circ, p_t = 5765.1 \text{ psf}$				
				p_{t1} , psf	C_p	p_t/p_{t2}	$p_t/\rho a_2$	M_L	p_{t1} , psf	C_p	p_t/p_{t2}	$p_t/\rho a_2$
1	0	.000	.0000	818.5	1.758	.98212	20.19574	16.073	1.755	.98054	20.16249	16.793
2	0	.230	-.0025	818.5	1.758	.98212	20.19574	16.073	1.755	.98054	20.16249	16.793
3	0	.430	-.0050	818.5	1.758	.98212	20.19574	16.073	1.755	.98054	20.16249	16.793
4	0	.630	-.0075	818.5	1.758	.98212	20.19574	16.073	1.755	.98054	20.16249	16.793
5	0	.830	-.0100	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
6	0	1.030	-.0125	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
7	0	1.230	-.0150	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
8	0	1.430	-.0175	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
9	0	1.630	-.0200	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
10	0	1.830	-.0225	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
11	0	2.030	-.0250	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
12	0	2.230	-.0275	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
13	0	2.430	-.0300	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
14	0	2.630	-.0325	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
15	0	2.830	-.0350	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
16	0	3.030	-.0375	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
17	0	3.230	-.0400	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
18	0	3.430	-.0425	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
19	0	3.630	-.0450	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
20	0	3.830	-.0475	818.5	1.758	.98212	20.19574	16.073	1.751	.97859	20.16249	16.793
21	180	.200	-.025	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
22	180	.400	-.050	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
23	180	.600	-.075	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
24	180	.800	-.100	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
25	180	1.000	-.125	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
26	180	1.200	-.150	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
27	180	1.400	-.175	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
28	180	1.600	-.200	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
29	180	1.800	-.225	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
30	180	2.000	-.250	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
31	180	2.200	-.275	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
32	180	2.400	-.300	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
33	180	2.600	-.325	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
34	180	2.800	-.350	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
35	180	3.000	-.375	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
36	180	3.200	-.400	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
37	180	3.400	-.425	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
38	180	3.600	-.450	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
39	180	3.800	-.475	824.0	1.770	.98870	20.33053	17.528	1.766	.99133	20.21879	17.528
40	270	1.000	-.125	820.8	1.762	.98571	20.31572	17.528	1.762	.98571	20.21879	17.528
41	270	1.200	-.150	820.8	1.762	.98571	20.31572	17.528	1.762	.98571	20.21879	17.528
42	270	1.400	-.175	820.8	1.762	.98571	20.31572	17.528	1.762	.98571	20.21879	17.528
43	270	1.600	-.200	820.8	1.762	.98571	20.31572	17.528	1.762	.98571	20.21879	17.528
44	270	1.800	-.225	820.8	1.762	.98571	20.31572	17.528	1.762	.98571	20.21879	17.528
45	270	2.000	-.250	820.8	1.762	.98571	20.31572	17.528	1.762	.98571	20.21879	17.528

³Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

$$(b) \quad a = 5^\circ$$

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XI.- DATA^a FOR 180° CONE; $M_{\infty} = 3.95$ - Continued

(b) $\alpha = 5^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\phi = 67.5^\circ, p_t = 5765.1 \text{ psf}$	$\phi = 90.0^\circ, p_t = 5755.6 \text{ psf}$	M_t	p_t/p_{∞}	$p_t/p_{\infty, 2}$	C_p	$p_t/p_{\infty, 2}$	M_t
				p_t , psf	C_p	$p_t/p_{\infty, 2}$	p_t/p_{∞}	$p_t/p_{\infty, 2}$	p_t , psf	p_t/p_{∞}	M_t
1	0	.320	.000	820.1	1.758	.98242	20.20187	.98242	1.761	.98404	15177
2	0	.420	.025	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
3	0	.520	.050	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
4	0	.620	.075	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
5	0	.720	.100	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
6	0	.820	.125	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
7	0	.920	.150	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
8	0	1.020	.175	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
9	0	1.120	.200	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
10	0	1.220	.225	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
11	0	1.320	.250	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
12	0	1.420	.275	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
13	0	1.520	.300	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
14	0	1.620	.325	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
15	0	1.720	.350	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
16	0	1.820	.375	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
17	0	1.920	.400	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
18	0	2.020	.425	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
19	0	2.120	.450	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
20	0	2.220	.475	818.5	1.755	.98051	20.16249	.98051	1.761	.98404	15177
21	180	.320	.000	820.1	1.776	.99200	20.39877	.99200	1.777	.99253	15177
22	180	.420	.025	820.1	1.773	.99008	20.35939	.99008	1.777	.99253	15177
23	180	.520	.050	820.1	1.769	.98817	20.32001	.98817	1.777	.99253	15177
24	180	.620	.075	820.1	1.765	.98625	20.28063	.98625	1.777	.99253	15177
25	180	.720	.100	820.1	1.762	.98434	20.24125	.98434	1.777	.99253	15177
26	180	.820	.125	820.1	1.755	.98051	20.16249	.98051	1.777	.99253	15177
27	180	.920	.150	820.1	1.751	.97668	20.08373	.97668	1.777	.99253	15177
28	180	1.020	.175	820.1	1.747	.97285	20.00497	.97285	1.777	.99253	15177
29	180	1.120	.200	820.1	1.743	.96902	19.92621	.96902	1.777	.99253	15177
30	180	1.220	.225	820.1	1.740	.96519	19.84745	.96519	1.777	.99253	15177
31	180	1.320	.250	820.1	1.737	.96136	19.76869	.96136	1.777	.99253	15177
32	180	1.420	.275	820.1	1.734	.95753	19.68993	.95753	1.777	.99253	15177
33	180	1.520	.300	820.1	1.731	.95370	19.61117	.95370	1.777	.99253	15177
34	180	1.620	.325	820.1	1.728	.94987	19.53241	.94987	1.777	.99253	15177
35	180	1.720	.350	820.1	1.725	.94604	19.45365	.94604	1.777	.99253	15177
36	180	1.820	.375	820.1	1.722	.94221	19.37489	.94221	1.777	.99253	15177
37	180	1.920	.400	820.1	1.719	.93838	19.29613	.93838	1.777	.99253	15177
38	180	2.020	.425	820.1	1.716	.93455	19.21737	.93455	1.777	.99253	15177
39	180	2.120	.450	820.1	1.713	.93072	19.13862	.93072	1.777	.99253	15177
40	180	2.220	.475	820.1	1.710	.92689	19.05986	.92689	1.777	.99253	15177
41	270	1.000	.125	820.1	1.769	.98851	20.32001	.98851	1.777	.99253	15177
42	270	1.200	.250	820.1	1.755	.98051	20.16249	.98051	1.777	.99253	15177
43	270	1.400	.375	820.1	1.741	.97253	20.00497	.97253	1.777	.99253	15177
44	270	1.600	.500	820.1	1.727	.96455	19.84745	.96455	1.777	.99253	15177
45	270	1.800	.625	820.1	1.713	.95657	19.69093	.95657	1.777	.99253	15177

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XI. - DATA^a FOR 180° CONE; $M_{\infty} = 3.95$ - Continued(c) $\alpha = 10^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\phi = 0.0^\circ, p_t = 5765.1 \text{ psf}$				$\phi = 22.5^\circ, p_t = 5765.1 \text{ psf}$				$\phi = 45.0^\circ, p_t = 5765.1 \text{ psf}$						
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t\infty}$	M_t
1	0	.230	.0000	815.4	1.747	.97475	20.04813	-18345	815.1	1.749	.97157	20.10217	-18030	815.3	1.747	.97668	20.08373	-18392
2	0	.230	.0025	813.8	1.744	.97483	20.04575	-19118	812.9	1.742	.97157	20.10217	-19532	812.1	1.740	.97295	20.08043	-18976
3	0	.430	.0050	810.6	1.737	.97100	19.96698	-20547	811.3	1.738	.97184	19.94416	-20244	810.5	1.736	.97093	19.96559	-20512
4	0	.530	.0075	809.0	1.733	.96908	19.92760	-21228	809.7	1.735	.96992	19.94482	-20933	808.9	1.733	.96902	19.92621	-21252
5	0	.730	.0100	807.4	1.726	.96525	19.87707	-22373	808.5	1.727	.96610	19.86614	-22253	807.6	1.733	.96902	19.92621	-21252
6	0	1.030	.0125	802.6	1.719	.96142	19.77057	-24057	809.1	1.727	.96610	19.86614	-22253	808.9	1.733	.96902	19.92621	-21252
7	0	1.230	.0150	799.4	1.711	.95159	19.69130	-24957	800.1	1.713	.95644	19.70879	-22699	802.5	1.722	.96327	19.87689	-22372
8	0	1.430	.0175	794.6	1.701	.95185	19.57315	-26446	795.3	1.702	.95270	19.59077	-22400	799.3	1.711	.95753	19.48993	-22978
9	0	1.630	.0200	789.8	1.690	.94610	19.45501	-28245	792.1	1.695	.94888	19.51209	-22482	796.1	1.704	.95370	19.41117	-22913
10	0	1.830	.0225	784.6	1.679	.94248	19.33686	-29770	785.7	1.691	.94123	19.35474	-22544	789.7	1.690	.94604	19.45365	-22863
11	0	2.030	.0250	778.0	1.665	.93270	19.17933	-31707	779.3	1.656	.93357	19.19738	-22604	780.9	1.679	.94029	19.33551	-22787
12	0	2.230	.0275	773.8	1.654	.92695	19.06118	-33098	774.5	1.655	.92783	19.07936	-32887	780.1	1.668	.93455	19.21738	-23149
13	0	2.430	.0300	765.8	1.636	.91737	18.86427	-35317	763.2	1.641	.92018	18.92201	-34728	773.8	1.654	.92689	19.05886	-33113
14	0	2.630	.0325	756.2	1.614	.90588	18.62797	-37844	758.6	1.619	.90870	18.68597	-37236	765.2	1.614	.90582	18.62668	-37858
15	0	2.830	.0350	743.8	1.598	.89159	18.35159	-40251	749.0	1.598	.89723	18.44994	-39667	743.4	1.614	.90582	18.62668	-37858
16	0	3.030	.0375	733.8	1.564	.87907	18.03169	-42521	740.2	1.564	.88276	18.13523	-42751	743.4	1.585	.89050	18.31164	-41043
17	0	3.230	.0400	717.9	1.527	.85992	17.68279	-46937	720.2	1.533	.88276	17.73124	-44605	729.0	1.553	.89326	17.93722	-44429
18	0	3.430	.0425	698.7	1.484	.83694	17.21020	-51076	731.1	1.490	.83983	17.26977	-50565	709.8	1.509	.85028	17.48466	-48998
19	0	3.630	.0450	669.9	1.419	.80246	16.50131	-56963	736.6	1.428	.80731	16.60101	-56154	714.2	1.464	.81581	18.17582	-45721
20	0	3.830	.0475	624.1	1.267	.80742	15.25822	-65913	627.6	1.324	.75183	15.46019	-65158	633.1	1.336	.75836	18.59443	-46122
21	180	.250	.0050	824.1	1.767	.98714	20.29887	-13611	824.1	1.767	.98714	20.29887	-13611	824.0	1.767	.98707	20.29746	-13647
22	180	.450	.0075	825.7	1.771	.98905	20.33821	-12550	825.7	1.771	.98905	20.33821	-12550	824.0	1.767	.98707	20.29746	-13647
23	180	.650	.0100	827.2	1.774	.99097	20.37755	-11394	827.2	1.774	.99097	20.37755	-11394	824.0	1.767	.98707	20.29746	-13647
24	180	.850	.0125	827.2	1.774	.99097	20.37755	-11394	827.2	1.774	.99097	20.37755	-11394	824.0	1.767	.98707	20.29746	-13647
25	180	1.050	.0150	835.4	1.778	.99288	20.41689	-10109	828.8	1.778	.99288	20.41689	-10109	825.6	1.770	.98898	20.33679	-12590
26	180	1.250	.0175	832.0	1.785	.99479	20.45622	-88640	828.8	1.778	.99288	20.41689	-10109	825.6	1.770	.98898	20.33679	-12590
27	180	1.450	.0200	830.4	1.785	.99479	20.45622	-88640	828.8	1.778	.99288	20.41689	-10109	825.6	1.770	.98898	20.33679	-12590
28	180	1.650	.0225	830.4	1.785	.99479	20.45622	-88640	828.8	1.778	.99288	20.41689	-10109	825.6	1.770	.98898	20.33679	-12590
29	180	1.850	.0250	832.0	1.785	.99479	20.45622	-88640	828.8	1.778	.99288	20.41689	-10109	825.6	1.770	.98898	20.33679	-12590
30	180	2.050	.0275	832.0	1.785	.99479	20.45622	-88640	828.8	1.778	.99288	20.41689	-10109	825.6	1.770	.98898	20.33679	-12590
31	180	2.250	.0300	830.4	1.781	.99479	20.45622	-88640	827.2	1.774	.99097	20.37755	-11394	825.6	1.760	.98535	20.21876	-15585
32	180	2.450	.0325	828.8	1.778	.99288	20.41689	-10109	825.7	1.771	.98905	20.33821	-12550	824.0	1.752	.97942	20.10211	-15762
33	180	2.650	.0350	825.7	1.771	.98905	20.33821	-12550	822.5	1.763	.98523	20.25953	-14597	812.8	1.742	.97366	20.02211	-15957
34	180	2.850	.0375	820.9	1.760	.98331	20.22017	-15523	817.7	1.753	.97949	20.14151	-17233	808.0	1.731	.96794	19.90410	-16255
35	180	3.050	.0400	816.1	1.749	.97777	20.10217	-18030	811.3	1.738	.97184	19.94416	-20244	800.0	1.713	.95838	19.70742	-22719
36	180	3.250	.0425	806.5	1.727	.96510	19.86614	-22253	807.7	1.717	.96035	19.74431	-22108	799.5	1.691	.95370	19.41117	-22913
37	180	3.450	.0450	793.7	1.699	.95079	19.55143	-26646	798.9	1.688	.95065	19.54912	-26108	790.5	1.655	.94341	19.07804	-32902
38	180	3.650	.0475	780.0	1.648	.92401	19.00069	-33792	786.6	1.637	.91827	18.88267	-35114	750.5	1.601	.90908	18.44880	-35293
39	180	3.850	.0500	771.4	1.648	.92401	19.00069	-33792	786.6	1.637	.91827	18.88267	-35114	750.5	1.601	.90908	18.44880	-35293
40	180	4.050	.0525	757.4	1.555	.87427	17.97787	-44236	723.4	1.540	.86662	17.82052	-45689	735.8	1.500	.84551	17.38658	-45955
41	270	2.000	.0250	808.5	1.729	.97777	20.10217	-18030	811.3	1.738	.97184	19.94416	-20244	800.0	1.713	.95838	19.70742	-22719
42	270	2.200	.0275	771.4	1.648	.92401	19.00069	-33792	785.7	1.637	.91827	18.88267	-35114	750.5	1.601	.90908	18.44880	-35293
43	90	1.350	.0125	812.2	1.740	.97281	20.00636	-19845	808.1	1.731	.96958	19.90548	-21602	804.1	1.722	.96327	19.83051	-23183
44	90	1.550	.0150	801.0	1.715	.95951	19.73068	-24372	792.1	1.695	.94888	19.51209	-24602	784.9	1.679	.94029	19.33551	-22787
45	90	1.750	.0175	767.4	1.639	.91929	18.90365	-34482	755.4	1.612	.90488	18.60730	-38059	743.4	1.595	.89050	18.31164	-41043

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XI.- DATA^a FOR 180° CONE; $M_{\infty} = 3.95$ - Continued

(c) $\alpha = 10^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 67.5^\circ, p_t = 5755.6 \text{ psf}$					$\phi = 90.0^\circ, p_t = 5755.6 \text{ psf}$				
				p_t , psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}	M_t
1	0	-0.00	-0.000	815.4	1.740	.9746	20.0974	-18078	815.3	1.750	.97829	20.11685	-17736
2	0	-0.20	-0.025	813.0	1.745	.97554	20.09855	-18844	813.0	1.750	.97829	20.11685	-17736
3	0	-0.40	-0.050	810.0	1.745	.97554	20.09855	-19582	813.0	1.750	.97829	20.11685	-17736
4	0	-0.60	-0.075	808.4	1.742	.97169	19.98127	-20295	813.7	1.747	.97637	20.07740	-18515
5	0	-0.80	-0.100	804.8	1.738	.96977	19.94178	-20985	813.7	1.747	.97637	20.07740	-18515
6	0	-1.00	-0.125	800.0	1.735	.96777	19.89800	-21656	810.5	1.740	.97253	19.99851	-18986
7	0	-1.20	-0.150	795.0	1.727	.96401	19.82331	-22307	807.3	1.732	.96870	19.93907	-19502
8	0	-1.40	-0.175	789.4	1.723	.96017	19.74434	-22937	804.1	1.725	.96486	19.88073	-20064
9	0	-1.60	-0.200	783.0	1.716	.95633	19.66536	-23537	802.9	1.718	.96102	19.82351	-20689
10	0	-1.80	-0.225	777.0	1.709	.95257	19.58689	-24108	799.1	1.707	.95727	19.76718	-21365
11	0	-2.00	-0.250	770.4	1.697	.94895	19.50896	-24656	795.0	1.682	.95348	19.71017	-22092
12	0	-2.20	-0.275	763.6	1.676	.94505	19.43096	-25186	791.0	1.664	.94964	19.65305	-22869
13	0	-2.40	-0.300	756.6	1.640	.94085	19.35296	-25696	787.0	1.642	.94582	19.59596	-23699
14	0	-2.60	-0.325	749.4	1.600	.93638	19.27496	-26186	783.0	1.609	.94199	19.53887	-24576
15	0	-2.80	-0.350	742.0	1.559	.93168	19.19696	-26656	779.0	1.588	.93816	19.48178	-25502
16	0	-3.00	-0.375	734.4	1.519	.92678	19.11896	-27108	775.0	1.566	.93425	19.42469	-26476
17	0	-3.20	-0.400	726.6	1.478	.92168	19.04096	-27537	771.0	1.544	.93034	19.36760	-27502
18	0	-3.40	-0.425	718.4	1.437	.91638	18.96296	-27937	767.0	1.522	.92643	19.31051	-28576
19	0	-3.60	-0.450	710.0	1.396	.91088	18.88496	-28307	763.0	1.500	.92252	19.25342	-29702
20	0	-3.80	-0.475	701.4	1.355	.90518	18.80696	-28656	759.0	1.478	.91861	19.19633	-30876
21	180	-0.00	-0.000	822.4	1.766	.98678	20.29152	-13800	822.4	1.766	.98678	20.29152	-13800
22	180	-0.20	-0.025	820.8	1.763	.98487	20.25212	-14776	819.2	1.763	.98487	20.25212	-14776
23	180	-0.40	-0.050	819.2	1.763	.98487	20.25212	-15693	817.6	1.763	.98487	20.25212	-15693
24	180	-0.60	-0.075	817.6	1.763	.98487	20.25212	-16610	816.0	1.763	.98487	20.25212	-16610
25	180	-0.80	-0.100	816.0	1.763	.98487	20.25212	-17527	814.4	1.763	.98487	20.25212	-17527
26	180	-1.00	-0.125	814.4	1.763	.98487	20.25212	-18444	812.8	1.763	.98487	20.25212	-18444
27	180	-1.20	-0.150	812.8	1.759	.98295	20.21272	-19361	811.2	1.761	.98295	20.21272	-19361
28	180	-1.40	-0.175	811.2	1.759	.98295	20.21272	-20278	809.6	1.759	.98295	20.21272	-20278
29	180	-1.60	-0.200	809.6	1.752	.97912	20.17332	-21195	808.0	1.752	.97912	20.17332	-21195
30	180	-1.80	-0.225	808.0	1.748	.97720	20.13392	-22112	806.4	1.752	.97720	20.13392	-22112
31	180	-2.00	-0.250	806.4	1.741	.97337	20.09452	-23029	804.8	1.734	.97337	20.09452	-23029
32	180	-2.20	-0.275	804.8	1.730	.96954	20.05512	-23946	803.2	1.723	.96954	20.05512	-23946
33	180	-2.40	-0.300	803.2	1.716	.96570	20.01572	-24863	801.6	1.716	.96570	20.01572	-24863
34	180	-2.60	-0.325	801.6	1.698	.96186	19.97632	-25780	800.0	1.705	.96186	19.97632	-25780
35	180	-2.80	-0.350	799.9	1.680	.95792	19.93692	-26697	798.3	1.705	.95792	19.93692	-26697
36	180	-3.00	-0.375	798.3	1.658	.95398	19.89752	-27614	796.7	1.673	.95398	19.89752	-27614
37	180	-3.20	-0.400	796.7	1.636	.94994	19.85812	-28531	795.1	1.647	.94994	19.85812	-28531
38	180	-3.40	-0.425	795.1	1.614	.94590	19.81872	-29448	793.5	1.622	.94590	19.81872	-29448
39	180	-3.60	-0.450	793.5	1.592	.94186	19.77932	-30365	791.9	1.607	.94186	19.77932	-30365
40	270	-0.00	-0.000	822.4	1.766	.98678	20.29152	-13800	822.4	1.766	.98678	20.29152	-13800
41	270	-0.20	-0.025	820.8	1.763	.98487	20.25212	-14776	819.2	1.763	.98487	20.25212	-14776
42	270	-0.40	-0.050	819.2	1.763	.98487	20.25212	-15693	817.6	1.763	.98487	20.25212	-15693
43	270	-0.60	-0.075	817.6	1.763	.98487	20.25212	-16610	816.0	1.763	.98487	20.25212	-16610
44	270	-0.80	-0.100	816.0	1.763	.98487	20.25212	-17527	814.4	1.763	.98487	20.25212	-17527
45	270	-1.00	-0.125	814.4	1.763	.98487	20.25212	-18444	812.8	1.763	.98487	20.25212	-18444

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XI.- DATA^a FOR 180° CONE; $M_{\infty} = 3.95$ - Continued(d) $\alpha = 15^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0, 0^\circ, p_t = 5765.1 \text{ psf}$				
				p_t , psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}	M_t
1	0	.000	.0000	902.4	1.719	.96142	19.77007	.23773
2	0	.230	.0000	799.4	1.711	.95759	19.69130	.24957
3	0	.460	.0000	706.2	1.704	.95376	19.61254	.26141
4	0	.690	.0000	613.0	1.697	.94993	19.53378	.27318
5	0	.920	.0000	519.8	1.690	.94610	19.45501	.28495
6	0	1.150	.0000	426.6	1.683	.94227	19.37624	.29670
7	0	1.380	.0000	333.4	1.676	.93844	19.29747	.30845
8	0	1.610	.0000	240.2	1.669	.93461	19.21870	.32020
9	0	1.840	.0000	147.0	1.661	.93078	19.13995	.33195
10	0	2.070	.0000	53.8	1.654	.92695	19.06118	.34370
11	0	2.300	.0000	0	1.647	.92312	18.98241	.35545
12	0	2.530	.0000	753.0	1.640	.91929	18.90364	.36720
13	0	2.760	.0000	735.4	1.633	.91546	18.82487	.37895
14	0	2.990	.0000	717.8	1.626	.91163	18.74610	.39070
15	0	3.220	.0000	699.2	1.619	.90780	18.66733	.40245
16	0	3.450	.0000	674.7	1.612	.90397	18.58856	.41420
17	0	3.680	.0000	647.5	1.605	.89970	18.50979	.42595
18	0	3.910	.0000	622.7	1.598	.89543	18.43102	.43770
19	0	4.140	.0000	597.9	1.591	.89116	18.35225	.44945
20	0	4.370	.0000	573.1	1.584	.88689	18.27348	.46120
21	180	.000	.0000	602.7	1.749	.97566	20.06284	.18795
22	180	.230	.0000	814.5	1.741	.97183	20.10217	.19970
23	180	.460	.0000	815.1	1.734	.96799	20.14150	.21145
24	180	.690	.0000	820.9	1.727	.96416	20.18083	.22320
25	180	.920	.0000	826.1	1.720	.96033	20.22016	.23495
26	180	1.150	.0000	827.2	1.713	.95650	20.25949	.24670
27	180	1.380	.0000	828.8	1.706	.95267	20.29882	.25845
28	180	1.610	.0000	830.4	1.699	.94884	20.33815	.27020
29	180	1.840	.0000	832.0	1.692	.94501	20.37748	.28195
30	180	2.070	.0000	832.0	1.685	.94118	20.41681	.29370
31	180	2.300	.0000	832.0	1.678	.93735	20.45614	.30545
32	180	2.530	.0000	832.0	1.671	.93352	20.49547	.31720
33	180	2.760	.0000	832.0	1.664	.92969	20.53480	.32895
34	180	2.990	.0000	832.0	1.657	.92586	20.57413	.34070
35	180	3.220	.0000	832.0	1.650	.92203	20.61346	.35245
36	180	3.450	.0000	832.0	1.643	.91820	20.65279	.36420
37	180	3.680	.0000	832.0	1.636	.91437	20.69212	.37595
38	180	3.910	.0000	832.0	1.629	.91054	20.73145	.38770
39	180	4.140	.0000	832.0	1.622	.90671	20.77078	.39945
40	270	1.000	.125	9500	1.713	.95844	19.51209	.27482
41	270	2.000	.250	9500	1.695	.94888	18.80399	.35875
42	270	3.000	.375	9500	1.676	.93759	19.69130	.44268
43	270	4.000	.500	9500	1.656	.92462	20.57413	.52661
44	90	2.000	.250	9500	1.686	.95159	19.69130	.44268
45	90	3.000	.375	9500	1.614	.90588	18.62797	.37844

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XI. - DATA^a FOR 180° CONE; $M_{\infty} = 3.95$ - Continued(e) $\alpha = 20^\circ$

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 0.0^\circ, P_t = 5765.1 \text{ psf}$				$\Phi = 22.5^\circ, P_t = 5765.1 \text{ psf}$				$\Phi = 45.0^\circ, P_t = 5765.1 \text{ psf}$						
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t
1	0	.200	.000	788.2	1.686	.94419	19.41562	.28761	788.2	1.686	.94419	19.41562	.28761	788.1	1.685	.94412	19.41427	.28779
2	0	.300	.000	788.2	1.675	.93844	19.29748	.30264	783.4	1.675	.93844	19.29748	.30264	783.3	1.675	.94412	19.41427	.28779
3	0	.450	.050	780.2	1.657	.92887	19.10095	.31232	780.2	1.657	.93844	19.29748	.30264	780.1	1.675	.94412	19.41427	.28779
4	0	.630	.075	775.4	1.650	.92594	19.02180	.33501	773.8	1.651	.93018	19.13995	.32176	780.1	1.668	.93455	19.21718	.30261
5	0	.800	.100	772.2	1.639	.91929	18.90365	.34882	767.4	1.639	.91929	18.90365	.34882	775.4	1.664	.92880	19.07800	.31723
6	0	1.000	.125	767.4	1.628	.91354	18.78550	.36175	764.2	1.632	.91566	18.82438	.35746	769.0	1.657	.92880	19.07800	.31723
7	0	1.230	.150	764.2	1.618	.90814	18.66735	.37432	757.8	1.632	.91566	18.82438	.35746	769.0	1.657	.92880	19.07800	.31723
8	0	1.430	.175	761.8	1.603	.90266	18.54921	.38659	752.0	1.632	.91566	18.82438	.35746	769.0	1.657	.92880	19.07800	.31723
9	0	1.600	.200	751.4	1.585	.89656	18.43109	.39821	746.6	1.592	.90205	18.66735	.37432	757.8	1.632	.91566	18.82438	.35746
10	0	1.800	.225	743.4	1.571	.89056	18.31291	.40950	741.8	1.592	.90205	18.66735	.37432	757.8	1.632	.91566	18.82438	.35746
11	0	2.000	.250	737.0	1.558	.88456	18.19476	.42058	737.0	1.592	.90205	18.66735	.37432	757.8	1.632	.91566	18.82438	.35746
12	0	2.200	.275	731.0	1.545	.87856	18.07658	.43146	732.2	1.594	.89492	18.49476	.38659	752.0	1.607	.90199	18.58792	.38322
13	0	2.400	.300	724.0	1.532	.87256	17.95840	.44218	727.4	1.594	.89492	18.49476	.38659	752.0	1.607	.90199	18.58792	.38322
14	0	2.600	.325	717.8	1.519	.86656	17.84022	.45276	722.6	1.594	.89492	18.49476	.38659	752.0	1.607	.90199	18.58792	.38322
15	0	2.800	.350	711.5	1.513	.86056	17.72204	.46324	717.8	1.594	.89492	18.49476	.38659	752.0	1.607	.90199	18.58792	.38322
16	0	3.000	.375	703.3	1.499	.85456	17.60386	.47372	713.0	1.594	.89492	18.49476	.38659	752.0	1.607	.90199	18.58792	.38322
17	0	3.200	.400	697.8	1.488	.84856	17.48568	.48420	708.2	1.594	.89492	18.49476	.38659	752.0	1.607	.90199	18.58792	.38322
18	0	3.400	.425	693.8	1.480	.84256	17.36750	.49468	703.4	1.594	.89492	18.49476	.38659	752.0	1.607	.90199	18.58792	.38322
19	0	3.600	.450	690.0	1.472	.83656	17.24932	.50516	698.6	1.594	.89492	18.49476	.38659	752.0	1.607	.90199	18.58792	.38322
20	0	3.800	.475	686.0	1.465	.83056	17.13114	.51564	693.8	1.594	.89492	18.49476	.38659	752.0	1.607	.90199	18.58792	.38322
21	0	4.000	.500	682.0	1.458	.82456	17.01296	.52612	689.0	1.594	.89492	18.49476	.38659	752.0	1.607	.90199	18.58792	.38322
22	180	.000	.050	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
23	180	.000	.075	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
24	180	.000	.100	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
25	180	.000	.125	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
26	180	.000	.150	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
27	180	.000	.175	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
28	180	.000	.200	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
29	180	.000	.225	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
30	180	.000	.250	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
31	180	.000	.275	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
32	180	.000	.300	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
33	180	.000	.325	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
34	180	.000	.350	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
35	180	.000	.375	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
36	180	.000	.400	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
37	180	.000	.425	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
38	180	.000	.450	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
39	180	.000	.475	803.3	1.709	.95844	19.70879	.24599	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
40	270	.230	.125	782.2	1.605	.94597	19.23672	.31013	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
41	270	.330	.150	772.2	1.605	.94597	19.23672	.31013	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
42	270	.330	.175	767.4	1.605	.94597	19.23672	.31013	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
43	90	2.000	.125	782.2	1.605	.94597	19.23672	.31013	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
44	90	2.000	.150	772.2	1.605	.94597	19.23672	.31013	798.5	1.709	.95844	19.70879	.24599	798.4	1.709	.95844	19.70879	.24599
45	90	3.030	.375	745.0	1.589	.93248	18.35229	.40642	717.9	1.527	.85992	17.68279	.46737	730.2	1.488	.83879	17.24838	.50749

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XI.- DATA^a FOR 180° CONE; $M_{\infty} = 3.95$ - Concluded

(e) $\alpha = 20^\circ$ - Concluded

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 67.5^\circ, P_t = 5765.1 \text{ psf}$				$\Phi = 90.0^\circ, P_t = 5755.6 \text{ psf}$			
				P_t , psf	C_p	$P_t/P_{t,2}$	M_L	P_t , psf	C_p	$P_t/P_{t,2}$	M_L
1	0	-0.00	-0.000	788.1	1.686	19.41427	-28779	788.5	1.685	19.40684	-28875
2	0	-0.00	-0.000	788.1	1.679	19.33551	-28779	788.5	1.685	19.40684	-28875
3	0	-0.00	-0.000	788.1	1.675	19.33551	-28779	788.5	1.685	19.40684	-28875
4	0	-0.00	-0.000	788.1	1.675	19.33551	-28779	788.5	1.685	19.40684	-28875
5	0	-0.00	-0.000	788.1	1.668	19.25675	-30768	788.5	1.685	19.40684	-28875
6	0	-0.00	-0.000	788.1	1.664	19.21738	-31249	788.5	1.685	19.40684	-28875
7	0	-0.00	-0.000	788.1	1.657	19.17800	-31723	788.5	1.678	19.36740	-29383
8	0	-0.00	-0.000	788.1	1.650	19.13862	-32197	788.5	1.671	19.32795	-29883
9	0	-0.00	-0.000	788.1	1.643	19.09924	-32671	788.5	1.664	19.28851	-30383
10	0	-0.00	-0.000	788.1	1.636	19.05986	-33145	788.5	1.657	19.24906	-30883
11	0	-0.00	-0.000	788.1	1.629	19.02048	-33619	788.5	1.650	19.20962	-31383
12	0	-0.00	-0.000	788.1	1.622	18.98110	-34093	788.5	1.643	19.17017	-31883
13	0	-0.00	-0.000	788.1	1.615	18.94172	-34567	788.5	1.636	19.13073	-32383
14	0	-0.00	-0.000	788.1	1.608	18.90234	-35041	788.5	1.629	19.09128	-32883
15	0	-0.00	-0.000	788.1	1.601	18.86296	-35515	788.5	1.622	19.05184	-33383
16	0	-0.00	-0.000	788.1	1.594	18.82358	-35989	788.5	1.615	19.01239	-33883
17	0	-0.00	-0.000	788.1	1.587	18.78420	-36463	788.5	1.608	18.97295	-34383
18	0	-0.00	-0.000	788.1	1.580	18.74482	-36937	788.5	1.601	18.93350	-34883
19	0	-0.00	-0.000	788.1	1.573	18.70544	-37411	788.5	1.594	18.89406	-35383
20	0	-0.00	-0.000	788.1	1.566	18.66606	-37885	788.5	1.587	18.85462	-35883
21	0	-0.00	-0.000	788.1	1.559	18.62668	-38359	788.5	1.580	18.81517	-36383
22	0	-0.00	-0.000	788.1	1.552	18.58730	-38833	788.5	1.573	18.77573	-36883
23	0	-0.00	-0.000	788.1	1.545	18.54792	-39307	788.5	1.566	18.73628	-37383
24	0	-0.00	-0.000	788.1	1.538	18.50854	-39781	788.5	1.559	18.69684	-37883
25	0	-0.00	-0.000	788.1	1.531	18.46916	-40255	788.5	1.552	18.65739	-38383
26	0	-0.00	-0.000	788.1	1.524	18.42978	-40729	788.5	1.545	18.61795	-38883
27	0	-0.00	-0.000	788.1	1.517	18.39040	-41203	788.5	1.538	18.57850	-39383
28	0	-0.00	-0.000	788.1	1.510	18.35102	-41677	788.5	1.531	18.53906	-39883
29	0	-0.00	-0.000	788.1	1.503	18.31164	-42151	788.5	1.524	18.49962	-40383
30	0	-0.00	-0.000	788.1	1.496	18.27226	-42625	788.5	1.517	18.46017	-40883
31	0	-0.00	-0.000	788.1	1.489	18.23288	-43099	788.5	1.510	18.42073	-41383
32	0	-0.00	-0.000	788.1	1.482	18.19350	-43573	788.5	1.503	18.38128	-41883
33	0	-0.00	-0.000	788.1	1.475	18.15412	-44047	788.5	1.496	18.34184	-42383
34	0	-0.00	-0.000	788.1	1.468	18.11474	-44521	788.5	1.489	18.30239	-42883
35	0	-0.00	-0.000	788.1	1.461	18.07536	-44995	788.5	1.482	18.26295	-43383
36	0	-0.00	-0.000	788.1	1.454	18.03598	-45469	788.5	1.475	18.22350	-43883
37	0	-0.00	-0.000	788.1	1.447	17.99660	-45943	788.5	1.468	18.18406	-44383
38	0	-0.00	-0.000	788.1	1.440	17.95722	-46417	788.5	1.461	18.14462	-44883
39	0	-0.00	-0.000	788.1	1.433	17.91784	-46891	788.5	1.454	18.10517	-45383
40	0	-0.00	-0.000	788.1	1.426	17.87846	-47365	788.5	1.447	18.06573	-45883
41	0	-0.00	-0.000	788.1	1.419	17.83908	-47839	788.5	1.440	18.02628	-46383
42	0	-0.00	-0.000	788.1	1.412	17.79970	-48313	788.5	1.433	17.98684	-46883
43	0	-0.00	-0.000	788.1	1.405	17.76032	-48787	788.5	1.426	17.94739	-47383
44	0	-0.00	-0.000	788.1	1.398	17.72094	-49261	788.5	1.419	17.90795	-47883
45	0	-0.00	-0.000	788.1	1.391	17.68156	-49735	788.5	1.412	17.86850	-48383

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XII.- DATA^a FOR 180° CONE; $M_{\infty} = 4.63$

(a) $\alpha = 0^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, p_t = 7871.9 \text{ psf}$				$\phi = 22.5^\circ, p_t = 7871.9 \text{ psf}$				$\phi = 45.0^\circ, p_t = 7871.9 \text{ psf}$						
				P_L , psf	C_p	$P_L/P_{L,2}$	$P_L/P_{L,\infty}$	M_L	P_L , psf	C_p	$P_L/P_{L,2}$	$P_L/P_{L,\infty}$	M_L	P_L , psf	C_p	$P_L/P_{L,2}$	$P_L/P_{L,\infty}$	M_L
1	0	.000	.0000	636.3	1.764	.97890	27.47374	1.7481	636.2	1.764	.97883	27.47083	1.7510	636.2	1.764	.97883	27.47083	1.7510
2	0	.025	.0000	636.3	1.760	.97890	27.47374	1.7481	636.2	1.760	.97883	27.47083	1.7510	636.2	1.760	.97883	27.47083	1.7510
3	0	.050	.0000	636.3	1.756	.97890	27.47374	1.7481	636.2	1.756	.97883	27.47083	1.7510	636.2	1.756	.97883	27.47083	1.7510
4	0	.075	.0000	636.3	1.752	.97890	27.47374	1.7481	636.2	1.752	.97883	27.47083	1.7510	636.2	1.752	.97883	27.47083	1.7510
5	0	.100	.0000	636.3	1.748	.97890	27.47374	1.7481	636.2	1.748	.97883	27.47083	1.7510	636.2	1.748	.97883	27.47083	1.7510
6	0	.125	.0000	636.3	1.744	.97890	27.47374	1.7481	636.2	1.744	.97883	27.47083	1.7510	636.2	1.744	.97883	27.47083	1.7510
7	0	.150	.0000	636.3	1.740	.97890	27.47374	1.7481	636.2	1.740	.97883	27.47083	1.7510	636.2	1.740	.97883	27.47083	1.7510
8	0	.175	.0000	636.3	1.736	.97890	27.47374	1.7481	636.2	1.736	.97883	27.47083	1.7510	636.2	1.736	.97883	27.47083	1.7510
9	0	.200	.0000	636.3	1.732	.97890	27.47374	1.7481	636.2	1.732	.97883	27.47083	1.7510	636.2	1.732	.97883	27.47083	1.7510
10	0	.225	.0000	636.3	1.728	.97890	27.47374	1.7481	636.2	1.728	.97883	27.47083	1.7510	636.2	1.728	.97883	27.47083	1.7510
11	0	.250	.0000	636.3	1.724	.97890	27.47374	1.7481	636.2	1.724	.97883	27.47083	1.7510	636.2	1.724	.97883	27.47083	1.7510
12	0	.275	.0000	636.3	1.720	.97890	27.47374	1.7481	636.2	1.720	.97883	27.47083	1.7510	636.2	1.720	.97883	27.47083	1.7510
13	0	.300	.0000	636.3	1.716	.97890	27.47374	1.7481	636.2	1.716	.97883	27.47083	1.7510	636.2	1.716	.97883	27.47083	1.7510
14	0	.325	.0000	636.3	1.712	.97890	27.47374	1.7481	636.2	1.712	.97883	27.47083	1.7510	636.2	1.712	.97883	27.47083	1.7510
15	0	.350	.0000	636.3	1.708	.97890	27.47374	1.7481	636.2	1.708	.97883	27.47083	1.7510	636.2	1.708	.97883	27.47083	1.7510
16	0	.375	.0000	636.3	1.704	.97890	27.47374	1.7481	636.2	1.704	.97883	27.47083	1.7510	636.2	1.704	.97883	27.47083	1.7510
17	0	.400	.0000	636.3	1.700	.97890	27.47374	1.7481	636.2	1.700	.97883	27.47083	1.7510	636.2	1.700	.97883	27.47083	1.7510
18	0	.425	.0000	636.3	1.696	.97890	27.47374	1.7481	636.2	1.696	.97883	27.47083	1.7510	636.2	1.696	.97883	27.47083	1.7510
19	0	.450	.0000	636.3	1.692	.97890	27.47374	1.7481	636.2	1.692	.97883	27.47083	1.7510	636.2	1.692	.97883	27.47083	1.7510
20	0	.475	.0000	636.3	1.688	.97890	27.47374	1.7481	636.2	1.688	.97883	27.47083	1.7510	636.2	1.688	.97883	27.47083	1.7510
21	180	.000	.0000	636.3	1.684	.97890	27.47374	1.7481	636.2	1.684	.97883	27.47083	1.7510	636.2	1.684	.97883	27.47083	1.7510
22	180	.025	.0000	636.3	1.680	.97890	27.47374	1.7481	636.2	1.680	.97883	27.47083	1.7510	636.2	1.680	.97883	27.47083	1.7510
23	180	.050	.0000	636.3	1.676	.97890	27.47374	1.7481	636.2	1.676	.97883	27.47083	1.7510	636.2	1.676	.97883	27.47083	1.7510
24	180	.075	.0000	636.3	1.672	.97890	27.47374	1.7481	636.2	1.672	.97883	27.47083	1.7510	636.2	1.672	.97883	27.47083	1.7510
25	180	.100	.0000	636.3	1.668	.97890	27.47374	1.7481	636.2	1.668	.97883	27.47083	1.7510	636.2	1.668	.97883	27.47083	1.7510
26	180	.125	.0000	636.3	1.664	.97890	27.47374	1.7481	636.2	1.664	.97883	27.47083	1.7510	636.2	1.664	.97883	27.47083	1.7510
27	180	.150	.0000	636.3	1.660	.97890	27.47374	1.7481	636.2	1.660	.97883	27.47083	1.7510	636.2	1.660	.97883	27.47083	1.7510
28	180	.175	.0000	636.3	1.656	.97890	27.47374	1.7481	636.2	1.656	.97883	27.47083	1.7510	636.2	1.656	.97883	27.47083	1.7510
29	180	.200	.0000	636.3	1.652	.97890	27.47374	1.7481	636.2	1.652	.97883	27.47083	1.7510	636.2	1.652	.97883	27.47083	1.7510
30	180	.225	.0000	636.3	1.648	.97890	27.47374	1.7481	636.2	1.648	.97883	27.47083	1.7510	636.2	1.648	.97883	27.47083	1.7510
31	180	.250	.0000	636.3	1.644	.97890	27.47374	1.7481	636.2	1.644	.97883	27.47083	1.7510	636.2	1.644	.97883	27.47083	1.7510
32	180	.275	.0000	636.3	1.640	.97890	27.47374	1.7481	636.2	1.640	.97883	27.47083	1.7510	636.2	1.640	.97883	27.47083	1.7510
33	180	.300	.0000	636.3	1.636	.97890	27.47374	1.7481	636.2	1.636	.97883	27.47083	1.7510	636.2	1.636	.97883	27.47083	1.7510
34	180	.325	.0000	636.3	1.632	.97890	27.47374	1.7481	636.2	1.632	.97883	27.47083	1.7510	636.2	1.632	.97883	27.47083	1.7510
35	180	.350	.0000	636.3	1.628	.97890	27.47374	1.7481	636.2	1.628	.97883	27.47083	1.7510	636.2	1.628	.97883	27.47083	1.7510
36	180	.375	.0000	636.3	1.624	.97890	27.47374	1.7481	636.2	1.624	.97883	27.47083	1.7510	636.2	1.624	.97883	27.47083	1.7510
37	180	.400	.0000	636.3	1.620	.97890	27.47374	1.7481	636.2	1.620	.97883	27.47083	1.7510	636.2	1.620	.97883	27.47083	1.7510
38	180	.425	.0000	636.3	1.616	.97890	27.47374	1.7481	636.2	1.616	.97883	27.47083	1.7510	636.2	1.616	.97883	27.47083	1.7510
39	180	.450	.0000	636.3	1.612	.97890	27.47374	1.7481	636.2	1.612	.97883	27.47083	1.7510	636.2	1.612	.97883	27.47083	1.7510
40	270	.000	.0000	636.3	1.608	.97890	27.47374	1.7481	636.2	1.608	.97883	27.47083	1.7510	636.2	1.608	.97883	27.47083	1.7510
41	270	.025	.0000	636.3	1.604	.97890	27.47374	1.7481	636.2	1.604	.97883	27.47083	1.7510	636.2	1.604	.97883	27.47083	1.7510
42	270	.050	.0000	636.3	1.600	.97890	27.47374	1.7481	636.2	1.600	.97883	27.47083	1.7510	636.2	1.600	.97883	27.47083	1.7510
43	270	.075	.0000	636.3	1.596	.97890	27.47374	1.7481	636.2	1.596	.97883	27.47083	1.7510	636.2	1.596	.97883	27.47083	1.7510
44	270	.100	.0000	636.3	1.592	.97890	27.47374	1.7481	636.2	1.592	.97883	27.47083	1.7510	636.2	1.592	.97883	27.47083	1.7510
45	270	.125	.0000	636.3	1.588	.97890	27.47374	1.7481	636.2	1.588	.97883	27.47083	1.7510	636.2	1.588	.97883	27.47083	1.7510
46	270	.150	.0000	636.3	1.584	.97890	27.47374	1.7481	636.2	1.584	.97883	27.47083	1.7510	636.2	1.584	.97883	27.47083	1.7510
47	270	.175	.0000	636.3	1.580	.97890	27.47374	1.7481	636.2	1.580	.97883	27.47083	1.7510	636.2	1.580	.97883	27.47083	1.7510
48	270	.200	.0000	636.3	1.576	.97890	27.47374	1.7481	636.2	1.576	.97883	27.47083	1.7510	636.2	1.576	.97883	27.47083	1.7510
49	270	.225	.0000	636.3	1.572	.97890	27.47374	1.7481	636.2	1.572	.97883	27.47083	1.7510	636.2	1.572	.97883	27.47083	1.7510
50	270	.250	.0000	636.3	1.568	.97890	27.47374	1.7481	636.2	1.568	.97883	27.47083	1.7510	636.2	1.568	.97883	27.47083	1.7510
51	270	.275	.0000	636.3	1.564	.97890	27.47374	1.7481	636.2	1.564	.97883	27.47083	1.7510	636.2	1.564	.97883	27.47083	1.7510
52	270	.300	.0000	636.3	1.560	.97890	27.47374	1.7481	636.2	1.560	.97883	27.47083	1.7510	636.2	1.560	.97883	27.47083	1.7510
53	270	.325	.0000	636.3	1.556	.97890	27.47374	1.7481	636.2	1.556	.97883	27.47083	1.7510	636.2	1.556	.97883	27.47083	1.7510
54	270	.350	.0000	636.3	1.552	.97890	27.47374	1.7481	636.2	1.552	.97883	27.47083	1.7510	636.2	1.552	.97883	27.47083	1.7510
55	270	.375	.0000	636.3	1.548	.97890	27.47374	1.7481	636.2	1.548	.97883	27.47083	1.7510	636.2	1.548	.97883	27.47083	1.7510
56	270	.400	.0000	636.3	1.544	.97890	27.47374	1.7481	636.2	1.544	.97883	27.47083	1.7510	636.2	1.544	.97883	27.47083	1.7510
57	270	.425	.0000	636.3	1.540	.97890	27.47374	1.7481	636.2	1.540	.97883	27.47083	1.7510	636.2	1.540	.97883	27.47083	1.7510
58	270	.450	.0000	636.3	1.536	.97890	27.47374	1.7481	636.2	1.536	.97883	27.47083	1.7510	636.2	1.536	.97883	27.47083	1.7510
59	270	.475	.0000	636.3	1.532	.97890	27.47374	1.7481	636.2	1.532	.97883	27.47083	1.7510	636.2	1.532	.97883	27.47083	1.7510
60	270	.500	.0000	636.3	1.528	.97890	27.47374	1.7481	636.2	1.528	.97883	27.47083	1.7510	636.2	1.528	.97883	27.47083	1.7510
61	270	.525	.0000	636.3	1.524	.97890	27.47374	1.7481	636.2	1.524	.97883	27.47083	1.7510	636.2	1.524	.97883	27.47083	1.75

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XII.- DATA³ FOR 180° CONE; $M_{\infty} = 4.63$ - Continued(a) $\alpha = 0^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 67.5^\circ, P_t = 7871.9 \text{ psf}$				$\Phi = 90.0^\circ, P_t = 7871.9 \text{ psf}$			
				P_t , psf	C_p	$P_t/P_{t,2}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	M_t
1	0	.330	.0000	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
2	0	.420	.0025	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
3	0	.510	.0050	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
4	0	.600	.0075	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
5	0	.690	.0100	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
6	0	.780	.0125	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
7	0	.870	.0150	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
8	0	.960	.0175	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
9	0	1.050	.0200	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
10	0	1.140	.0225	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
11	0	1.230	.0250	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
12	0	1.320	.0275	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
13	0	1.410	.0300	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
14	0	1.500	.0325	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
15	0	1.590	.0350	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
16	0	1.680	.0375	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
17	0	1.770	.0400	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
18	0	1.860	.0425	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
19	0	1.950	.0450	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
20	0	2.040	.0475	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
21	0	2.130	.0500	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
22	0	2.220	.0525	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
23	0	2.310	.0550	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
24	0	2.400	.0575	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
25	0	2.490	.0600	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
26	0	2.580	.0625	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
27	0	2.670	.0650	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
28	0	2.760	.0675	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
29	0	2.850	.0700	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
30	0	2.940	.0725	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
31	0	3.030	.0750	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
32	0	3.120	.0775	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
33	0	3.210	.0800	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
34	0	3.300	.0825	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
35	0	3.390	.0850	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
36	0	3.480	.0875	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
37	0	3.570	.0900	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
38	0	3.660	.0925	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
39	0	3.750	.0950	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
40	0	3.840	.0975	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
41	0	3.930	.1000	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
42	0	4.020	.1025	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
43	0	4.110	.1050	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
44	0	4.200	.1075	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105
45	0	4.290	.1100	636.2	1.764	.97876	-1.7539	635.3	1.761	.97739	-1.8105

Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XII.- DATA^a FOR 180° CONE; $M_{\infty} = 4.63$ - Continued

(b) $\alpha = 5^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\Phi = 0.0^\circ, P_t = 7871.9 \text{ psf}$					$\Phi = 22.5^\circ, P_t = 7871.9 \text{ psf}$					$\Phi = 45.0^\circ, P_t = 7871.9 \text{ psf}$				
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t
1	0	-300	-0.000	534.3	1.764	.97890	27.43734	174.01	534.2	1.764	.97893	27.43703	174.01	534.2	1.764	.97893	27.43703	174.01
2	0	-200	-0.025	634.7	1.760	.97644	27.40371	184.87	634.6	1.759	.97637	27.40381	184.87	634.6	1.759	.97637	27.40381	184.87
3	0	-100	-0.050	634.7	1.760	.97644	27.40371	184.87	634.6	1.759	.97637	27.40381	184.87	634.6	1.759	.97637	27.40381	184.87
4	0	-50	-0.075	633.1	1.755	.97398	27.33468	194.44	633.0	1.755	.97391	27.33278	194.44	633.0	1.755	.97391	27.33278	194.44
5	0	0	-0.100	633.1	1.755	.97398	27.33468	194.44	633.0	1.755	.97391	27.33278	194.44	633.0	1.755	.97391	27.33278	194.44
6	0	100	-0.125	628.3	1.741	.96650	27.12760	220.03	628.2	1.741	.96653	27.12572	220.03	628.2	1.741	.96653	27.12572	220.03
7	0	150	-0.150	628.3	1.741	.96650	27.12760	220.03	628.2	1.741	.96653	27.12572	220.03	628.2	1.741	.96653	27.12572	220.03
8	0	150	-0.175	628.7	1.737	.96414	27.05858	229.03	628.6	1.737	.96417	27.05670	229.03	628.6	1.737	.96417	27.05670	229.03
9	0	150	-0.200	623.5	1.727	.95922	26.92052	244.60	623.4	1.727	.95925	26.91864	244.60	623.4	1.727	.95925	26.91864	244.60
10	0	150	-0.225	623.5	1.727	.95922	26.92052	244.60	623.4	1.727	.95925	26.91864	244.60	623.4	1.727	.95925	26.91864	244.60
11	0	200	-0.250	617.1	1.709	.94938	26.78247	273.36	617.0	1.709	.94941	26.78059	273.36	617.0	1.709	.94941	26.78059	273.36
12	0	250	-0.275	617.1	1.709	.94938	26.78247	273.36	617.0	1.709	.94941	26.78059	273.36	617.0	1.709	.94941	26.78059	273.36
13	0	250	-0.300	607.5	1.681	.93421	26.43733	312.28	607.4	1.681	.93424	26.43545	312.28	607.4	1.681	.93424	26.43545	312.28
14	0	250	-0.325	601.1	1.663	.92479	25.95414	336.09	601.0	1.663	.92482	25.95226	336.09	601.0	1.663	.92482	25.95226	336.09
15	0	300	-0.350	601.1	1.663	.92479	25.95414	336.09	601.0	1.663	.92482	25.95226	336.09	601.0	1.663	.92482	25.95226	336.09
16	0	300	-0.375	595.1	1.617	.90019	25.26387	390.50	595.0	1.617	.90022	25.26199	390.50	595.0	1.617	.90022	25.26199	390.50
17	0	300	-0.400	595.1	1.617	.90019	25.26387	390.50	595.0	1.617	.90022	25.26199	390.50	595.0	1.617	.90022	25.26199	390.50
18	0	300	-0.425	585.9	1.539	.88298	24.78069	425.43	585.8	1.539	.88301	24.77881	425.43	585.8	1.539	.88301	24.77881	425.43
19	0	300	-0.450	585.9	1.539	.88298	24.78069	425.43	585.8	1.539	.88301	24.77881	425.43	585.8	1.539	.88301	24.77881	425.43
20	0	300	-0.475	585.9	1.539	.88298	24.78069	425.43	585.8	1.539	.88301	24.77881	425.43	585.8	1.539	.88301	24.77881	425.43
21	180	-0.500	-0.500	645.9	1.792	.99366	27.88690	1095.39	645.8	1.792	.99369	27.88502	1095.39	645.8	1.792	.99369	27.88502	1095.39
22	180	-0.525	-0.525	645.9	1.792	.99366	27.88690	1095.39	645.8	1.792	.99369	27.88502	1095.39	645.8	1.792	.99369	27.88502	1095.39
23	180	-0.550	-0.550	644.3	1.787	.99120	27.81787	1124.66	644.2	1.787	.99123	27.81599	1124.66	644.2	1.787	.99123	27.81599	1124.66
24	180	-0.575	-0.575	644.3	1.787	.99120	27.81787	1124.66	644.2	1.787	.99123	27.81599	1124.66	644.2	1.787	.99123	27.81599	1124.66
25	180	-0.600	-0.600	644.3	1.787	.99120	27.81787	1124.66	644.2	1.787	.99123	27.81599	1124.66	644.2	1.787	.99123	27.81599	1124.66
26	180	-0.625	-0.625	642.7	1.783	.98874	27.74885	1273.1	642.6	1.783	.98877	27.74697	1273.1	642.6	1.783	.98877	27.74697	1273.1
27	180	-0.650	-0.650	642.7	1.783	.98874	27.74885	1273.1	642.6	1.783	.98877	27.74697	1273.1	642.6	1.783	.98877	27.74697	1273.1
28	180	-0.675	-0.675	642.7	1.783	.98874	27.74885	1273.1	642.6	1.783	.98877	27.74697	1273.1	642.6	1.783	.98877	27.74697	1273.1
29	180	-0.700	-0.700	639.5	1.773	.98382	27.61076	1406.84	639.4	1.773	.98385	27.60888	1406.84	639.4	1.773	.98385	27.60888	1406.84
30	180	-0.725	-0.725	639.5	1.773	.98382	27.61076	1406.84	639.4	1.773	.98385	27.60888	1406.84	639.4	1.773	.98385	27.60888	1406.84
31	180	-0.750	-0.750	637.9	1.769	.98136	27.54176	1641.8	637.8	1.769	.98139	27.53988	1641.8	637.8	1.769	.98139	27.53988	1641.8
32	180	-0.775	-0.775	637.9	1.769	.98136	27.54176	1641.8	637.8	1.769	.98139	27.53988	1641.8	637.8	1.769	.98139	27.53988	1641.8
33	180	-0.800	-0.800	634.7	1.760	.97644	27.40371	1844.8	634.6	1.760	.97647	27.40183	1844.8	634.6	1.760	.97647	27.40183	1844.8
34	180	-0.825	-0.825	634.7	1.760	.97644	27.40371	1844.8	634.6	1.760	.97647	27.40183	1844.8	634.6	1.760	.97647	27.40183	1844.8
35	180	-0.850	-0.850	633.1	1.755	.97398	27.33468	1944.4	633.0	1.755	.97401	27.33278	1944.4	633.0	1.755	.97401	27.33278	1944.4
36	180	-0.875	-0.875	633.1	1.755	.97398	27.33468	1944.4	633.0	1.755	.97401	27.33278	1944.4	633.0	1.755	.97401	27.33278	1944.4
37	180	-0.900	-0.900	615.5	1.704	.96492	26.92052	2200.21	615.4	1.704	.96495	26.91864	2200.21	615.4	1.704	.96495	26.91864	2200.21
38	180	-0.925	-0.925	615.5	1.704	.96492	26.92052	2200.21	615.4	1.704	.96495	26.91864	2200.21	615.4	1.704	.96495	26.91864	2200.21
39	180	-0.950	-0.950	602.7	1.668	.95225	26.02317	2302.7	602.6	1.668	.95228	26.02129	2302.7	602.6	1.668	.95228	26.02129	2302.7
40	180	-0.975	-0.975	602.7	1.668	.95225	26.02317	2302.7	602.6	1.668	.95228	26.02129	2302.7	602.6	1.668	.95228	26.02129	2302.7
41	270	-0.900	-0.900	643.1	1.778	.98828	27.67868	1406.84	643.0	1.778	.98831	27.67680	1406.84	643.0	1.778	.98831	27.67680	1406.84
42	270	-0.925	-0.925	643.1	1.778	.98828	27.67868	1406.84	643.0	1.778	.98831	27.67680	1406.84	643.0	1.778	.98831	27.67680	1406.84
43	270	-0.950	-0.950	637.5	1.681	.94663	26.23025	2312.28	637.4	1.681	.94666	26.22837	2312.28	637.4	1.681	.94666	26.22837	2312.28
44	270	-0.975	-0.975	637.5	1.681	.94663	26.23025	2312.28	637.4	1.681	.94666	26.22837	2312.28	637.4	1.681	.94666	26.22837	2312.28
45	90	-0.900	-0.900	633.5	1.727	.95322	26.44509	3475.0	633.4	1.727	.95325	26.44321	3475.0	633.4	1.727	.95325	26.44321	3475.0
46	90	-0.925	-0.925	633.5	1.727	.95322	26.44509	3475.0	633.4	1.727	.95325	26.44321	3475.0	633.4	1.727	.95325	26.44321	3475.0
47	90	-0.950	-0.950	597.9	1.654	.91987	25.81609	3475.0	597.8	1.654	.91990	25.81421	3475.0	597.8	1.654	.91990	25.81421	3475.0
48	90	-0.975	-0.975	597.9	1.654	.91987	25.81609	3475.0	597.8	1.654	.91990	25.81421	3475.0	597.8	1.654	.91990	25.81421	3475.0

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XII.- DATA^a FOR 180° CONE; $M_{\infty} = 4.63$ - Continued

(b) $\alpha = 5^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\theta = 67.5^\circ, p_t = 7871.9 \text{ psf}$				$\theta = 90.0^\circ, p_t = 7871.9 \text{ psf}$			
				p_t , psf	C_p	$p_t/p_{t,2}$	M_t	p_t , psf	C_p	$p_t/p_{t,2}$	M_t
1	0	-0.200	-0.000	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
2	0	-0.250	-0.025	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
3	0	-0.300	-0.050	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
4	0	-0.350	-0.075	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
5	0	-0.400	-0.100	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
6	0	-0.450	-0.125	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
7	0	-0.500	-0.150	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
8	0	-0.550	-0.175	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
9	0	-0.600	-0.200	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
10	0	-0.650	-0.225	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
11	0	-0.700	-0.250	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
12	0	-0.750	-0.275	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
13	0	-0.800	-0.300	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
14	0	-0.850	-0.325	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
15	0	-0.900	-0.350	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
16	0	-0.950	-0.375	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
17	0	-1.000	-0.400	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
18	0	-1.050	-0.425	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
19	0	-1.100	-0.450	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
20	0	-1.150	-0.475	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
21	0	-1.200	-0.500	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
22	180	-0.200	-0.025	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
23	180	-0.250	-0.050	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
24	180	-0.300	-0.075	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
25	180	-0.350	-0.100	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
26	180	-0.400	-0.125	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
27	180	-0.450	-0.150	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
28	180	-0.500	-0.175	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
29	180	-0.550	-0.200	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
30	180	-0.600	-0.225	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
31	180	-0.650	-0.250	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
32	180	-0.700	-0.275	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
33	180	-0.750	-0.300	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
34	180	-0.800	-0.325	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
35	180	-0.850	-0.350	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
36	180	-0.900	-0.375	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
37	180	-0.950	-0.400	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
38	180	-1.000	-0.425	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
39	180	-1.050	-0.450	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
40	180	-1.100	-0.475	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
41	270	-0.200	-0.025	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
42	270	-0.250	-0.050	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
43	90	-0.200	-0.025	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
44	90	-0.250	-0.050	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539
45	90	-0.300	-0.075	636.2	1.764	.97876	.17539	636.2	1.764	.97876	.17539

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XII. - DATA^a FOR 180° CONE; $M_{\infty} = 4.63$ - Continued

(c) $\alpha = 10^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\phi = 0.0^\circ, p_t = 7871.9 \text{ psf}$					$\phi = 22.5^\circ, p_t = 7871.9 \text{ psf}$					$\phi = 45.0^\circ, p_t = 7871.9 \text{ psf}$				
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t
1	0	0.30	0.00	528.2	1.741	0.9653	27.12572	22105	628.2	1.741	0.9653	27.12572	22105	628.2	1.741	0.9653	27.12572	22105
2	0	0.20	0.00	625.6	1.736	0.96162	27.05669	22922	625.6	1.736	0.96162	27.05669	22922	625.6	1.736	0.96162	27.05669	22922
3	0	0.10	0.00	625.0	1.732	0.95916	26.91865	23713	625.0	1.732	0.95916	26.91865	23713	625.0	1.732	0.95916	26.91865	23713
4	0	0.00	0.05	623.4	1.727	0.95710	26.84963	24481	623.4	1.727	0.95710	26.84963	24481	623.4	1.727	0.95710	26.84963	24481
5	0	0.30	0.10	621.8	1.723	0.95510	26.78158	25228	621.8	1.723	0.95510	26.78158	25228	621.8	1.723	0.95510	26.78158	25228
6	0	0.20	0.10	620.0	1.718	0.95310	26.71354	25996	620.0	1.718	0.95310	26.71354	25996	620.0	1.718	0.95310	26.71354	25996
7	0	0.10	0.15	618.4	1.713	0.95110	26.64550	26764	618.4	1.713	0.95110	26.64550	26764	618.4	1.713	0.95110	26.64550	26764
8	0	0.00	0.20	616.8	1.708	0.94910	26.57746	27532	616.8	1.708	0.94910	26.57746	27532	616.8	1.708	0.94910	26.57746	27532
9	0	0.30	0.25	615.2	1.695	0.94710	26.50942	28300	615.2	1.695	0.94710	26.50942	28300	615.2	1.695	0.94710	26.50942	28300
10	0	0.20	0.25	613.6	1.686	0.94510	26.44138	29068	613.6	1.686	0.94510	26.44138	29068	613.6	1.686	0.94510	26.44138	29068
11	0	0.10	0.30	612.0	1.676	0.94310	26.37334	29836	612.0	1.676	0.94310	26.37334	29836	612.0	1.676	0.94310	26.37334	29836
12	0	0.00	0.35	610.4	1.666	0.94110	26.30530	30604	610.4	1.666	0.94110	26.30530	30604	610.4	1.666	0.94110	26.30530	30604
13	0	0.30	0.40	608.8	1.654	0.93910	26.23726	31372	608.8	1.654	0.93910	26.23726	31372	608.8	1.654	0.93910	26.23726	31372
14	0	0.20	0.45	607.2	1.644	0.93710	26.16922	32140	607.2	1.644	0.93710	26.16922	32140	607.2	1.644	0.93710	26.16922	32140
15	0	0.10	0.50	605.6	1.631	0.93510	26.10118	32908	605.6	1.631	0.93510	26.10118	32908	605.6	1.631	0.93510	26.10118	32908
16	0	0.00	0.55	604.0	1.618	0.93310	26.03314	33676	604.0	1.618	0.93310	26.03314	33676	604.0	1.618	0.93310	26.03314	33676
17	0	0.30	0.60	602.4	1.604	0.93110	25.96510	34444	602.4	1.604	0.93110	25.96510	34444	602.4	1.604	0.93110	25.96510	34444
18	0	0.20	0.65	600.8	1.589	0.92910	25.89706	35212	600.8	1.589	0.92910	25.89706	35212	600.8	1.589	0.92910	25.89706	35212
19	0	0.10	0.70	599.2	1.574	0.92710	25.82902	35980	599.2	1.574	0.92710	25.82902	35980	599.2	1.574	0.92710	25.82902	35980
20	0	0.00	0.75	597.6	1.559	0.92510	25.76098	36748	597.6	1.559	0.92510	25.76098	36748	597.6	1.559	0.92510	25.76098	36748
21	0	0.30	0.80	596.0	1.544	0.92310	25.69294	37516	596.0	1.544	0.92310	25.69294	37516	596.0	1.544	0.92310	25.69294	37516
22	0	0.20	0.85	594.4	1.529	0.92110	25.62490	38284	594.4	1.529	0.92110	25.62490	38284	594.4	1.529	0.92110	25.62490	38284
23	0	0.10	0.90	592.8	1.514	0.91910	25.55686	39052	592.8	1.514	0.91910	25.55686	39052	592.8	1.514	0.91910	25.55686	39052
24	0	0.00	0.95	591.2	1.499	0.91710	25.48882	39820	591.2	1.499	0.91710	25.48882	39820	591.2	1.499	0.91710	25.48882	39820
25	0	0.30	1.00	589.6	1.484	0.91510	25.42078	40588	589.6	1.484	0.91510	25.42078	40588	589.6	1.484	0.91510	25.42078	40588
26	0	0.20	1.05	588.0	1.469	0.91310	25.35274	41356	588.0	1.469	0.91310	25.35274	41356	588.0	1.469	0.91310	25.35274	41356
27	0	0.10	1.10	586.4	1.454	0.91110	25.28470	42124	586.4	1.454	0.91110	25.28470	42124	586.4	1.454	0.91110	25.28470	42124
28	0	0.00	1.15	584.8	1.439	0.90910	25.21666	42892	584.8	1.439	0.90910	25.21666	42892	584.8	1.439	0.90910	25.21666	42892
29	0	0.30	1.20	583.2	1.424	0.90710	25.14862	43660	583.2	1.424	0.90710	25.14862	43660	583.2	1.424	0.90710	25.14862	43660
30	0	0.20	1.25	581.6	1.409	0.90510	25.08058	44428	581.6	1.409	0.90510	25.08058	44428	581.6	1.409	0.90510	25.08058	44428
31	0	0.10	1.30	580.0	1.394	0.90310	25.01254	45196	580.0	1.394	0.90310	25.01254	45196	580.0	1.394	0.90310	25.01254	45196
32	0	0.00	1.35	578.4	1.379	0.90110	24.94450	45964	578.4	1.379	0.90110	24.94450	45964	578.4	1.379	0.90110	24.94450	45964
33	0	0.30	1.40	576.8	1.364	0.89910	24.87646	46732	576.8	1.364	0.89910	24.87646	46732	576.8	1.364	0.89910	24.87646	46732
34	0	0.20	1.45	575.2	1.349	0.89710	24.80842	47500	575.2	1.349	0.89710	24.80842	47500	575.2	1.349	0.89710	24.80842	47500
35	0	0.10	1.50	573.6	1.334	0.89510	24.74038	48268	573.6	1.334	0.89510	24.74038	48268	573.6	1.334	0.89510	24.74038	48268
36	0	0.00	1.55	572.0	1.319	0.89310	24.67234	49036	572.0	1.319	0.89310	24.67234	49036	572.0	1.319	0.89310	24.67234	49036
37	0	0.30	1.60	570.4	1.304	0.89110	24.60430	49804	570.4	1.304	0.89110	24.60430	49804	570.4	1.304	0.89110	24.60430	49804
38	0	0.20	1.65	568.8	1.289	0.88910	24.53626	50572	568.8	1.289	0.88910	24.53626	50572	568.8	1.289	0.88910	24.53626	50572
39	0	0.10	1.70	567.2	1.274	0.88710	24.46822	51340	567.2	1.274	0.88710	24.46822	51340	567.2	1.274	0.88710	24.46822	51340
40	0	0.00	1.75	565.6	1.259	0.88510	24.40018	52108	565.6	1.259	0.88510	24.40018	52108	565.6	1.259	0.88510	24.40018	52108
41	0	0.30	1.80	564.0	1.244	0.88310	24.33214	52876	564.0	1.244	0.88310	24.33214	52876	564.0	1.244	0.88310	24.33214	52876
42	0	0.20	1.85	562.4	1.229	0.88110	24.26410	53644	562.4	1.229	0.88110	24.26410	53644	562.4	1.229	0.88110	24.26410	53644
43	0	0.10	1.90	560.8	1.214	0.87910	24.19606	54412	560.8	1.214	0.87910	24.19606	54412	560.8	1.214	0.87910	24.19606	54412
44	0	0.00	1.95	559.2	1.199	0.87710	24.12802	55180	559.2	1.199	0.87710	24.12802	55180	559.2	1.199	0.87710	24.12802	55180
45	0	0.30	2.00	557.6	1.184	0.87510	24.06000	55948	557.6	1.184	0.87510	24.06000	55948	557.6	1.184	0.87510	24.06000	55948

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XII.- DATA^a FOR 180° CONE; $M_{\infty} = 4.63$ - Continued(c) $\alpha = 10^\circ$ - Concluded

Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 67.5^\circ, p_t = 7871.9 \text{ psf}$	$\Phi = 90.0^\circ, p_t = 7871.9 \text{ psf}$	M_t	$\Phi = 7871.9 \text{ psf}$	$p_t/p_{t,2}$	$p_t/p_{t,2}$	$p_t/p_{t,2}$	M_t
				p_t , psf	C_p	$p_t/p_{t,2}$	$p_t/p_{t,2}$	$p_t/p_{t,2}$	$p_t/p_{t,2}$	$p_t/p_{t,2}$	M_t
1	0	0	0.000	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
2	0	0.220	0.025	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
3	0	0.430	0.050	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
4	0	0.640	0.075	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
5	0	0.850	0.100	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
6	0	1.060	0.125	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
7	0	1.270	0.150	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
8	0	1.480	0.175	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
9	0	1.690	0.200	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
10	0	1.900	0.225	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
11	0	2.110	0.250	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
12	0	2.320	0.275	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
13	0	2.530	0.300	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
14	0	2.740	0.325	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
15	0	2.950	0.350	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
16	0	3.160	0.375	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
17	0	3.370	0.400	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
18	0	3.580	0.425	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
19	0	3.790	0.450	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
20	0	4.000	0.475	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
21	180	2.00	0.025	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
22	180	2.210	0.050	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
23	180	2.420	0.075	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
24	180	2.630	0.100	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
25	180	2.840	0.125	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
26	180	3.050	0.150	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
27	180	3.260	0.175	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
28	180	3.470	0.200	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
29	180	3.680	0.225	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
30	180	3.890	0.250	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
31	180	4.100	0.275	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
32	180	4.310	0.300	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
33	180	4.520	0.325	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
34	180	4.730	0.350	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
35	180	4.940	0.375	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
36	180	5.150	0.400	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
37	180	5.360	0.425	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
38	180	5.570	0.450	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
39	180	5.780	0.475	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
40	180	5.990	0.500	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
41	270	2.000	0.250	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
42	270	2.210	0.275	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
43	270	2.420	0.300	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
44	270	2.630	0.325	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128
45	270	2.840	0.350	628.2	1.741	0.9647	0.9647	0.9647	0.9647	0.9647	22128

^aConversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XII.- DATA^a FOR 180° CONE; $M_{\infty} = 4.63$ - Continued

(d) $\alpha = 15^\circ$

Orifice θ , deg	s , in.	s/b	s/s^*	$\Phi = 0.0^\circ, p_t = 7871.9 \text{ psf}$			
				p_t , psf	C_p	$p_t/p_{t,2}$	p_t/p_{∞}
1	0	.000	.0000	615.4	1.704	.94686	26.57354
2	0	.025	.0000	612.2	1.695	.94194	26.43550
3	0	.050	.0000	609.0	1.686	.93702	26.29745
4	0	.075	.0000	605.8	1.677	.93210	26.15940
5	0	.100	.0000	602.5	1.668	.92718	26.02135
6	0	.125	.0000	600.1	1.663	.92472	25.95234
7	0	.150	.0000	597.9	1.654	.91981	25.81430
8	0	.175	.0000	593.1	1.640	.91243	25.60723
9	0	.200	.0000	588.1	1.626	.90505	25.40016
10	0	.225	.0000	584.3	1.617	.90013	25.26212
11	0	.250	.0000	578.7	1.598	.89029	24.98603
12	0	.275	.0000	573.9	1.585	.88292	24.77896
13	0	.300	.0000	565.9	1.562	.87062	24.43385
14	0	.325	.0000	558.1	1.541	.85831	24.08874
15	0	.350	.0000	549.9	1.516	.84602	23.74363
16	0	.375	.0000	540.3	1.488	.83127	23.32950
17	0	.400	.0000	529.1	1.456	.81405	22.84634
18	0	.425	.0000	513.1	1.410	.78946	22.15612
19	0	.450	.0000	495.8	1.353	.75584	21.20581
20	0	.475	.0000	476.8	1.283	.70584	19.80937
21	180	.025	.0000	625.9	1.734	.96300	27.02667
22	180	.050	.0000	627.5	1.739	.96546	27.09561
23	180	.075	.0000	629.1	1.744	.96792	27.16456
24	180	.100	.0000	630.7	1.748	.97037	27.23350
25	180	.125	.0000	632.3	1.753	.97283	27.30245
26	180	.150	.0000	633.9	1.757	.97529	27.37139
27	180	.175	.0000	635.5	1.762	.97774	27.44034
28	180	.200	.0000	637.1	1.767	.98019	27.50928
29	180	.225	.0000	638.7	1.771	.98264	27.57823
30	180	.250	.0000	640.3	1.776	.98511	27.64718
31	180	.275	.0000	640.3	1.776	.98511	27.64718
32	180	.300	.0000	641.9	1.780	.98757	27.71612
33	180	.325	.0000	643.5	1.785	.98999	27.78507
34	180	.350	.0000	645.1	1.778	.98511	27.64718
35	180	.375	.0000	638.7	1.771	.98264	27.57823
36	180	.400	.0000	637.1	1.767	.98019	27.50928
37	180	.425	.0000	629.1	1.744	.97283	27.30245
38	180	.450	.0000	625.9	1.734	.96300	27.02667
39	180	.475	.0000	590.8	1.633	.90896	25.50086
40	270	.100	.0000	619.6	1.716	.95318	26.75088
41	270	.200	.0000	613.2	1.698	.94335	26.47510
42	270	.300	.0000	594.2	1.700	.96649	27.04599
43	270	.400	.0000	568.1	1.677	.93210	26.15940
44	90	.250	.0000	605.9	1.677	.93210	26.15940
45	90	.375	.0000	581.9	1.608	.89521	25.12407

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XII.- DATA^a FOR 180° CONE; $M_{\infty} = 4.63$ - Continued(e) $\alpha = 20^\circ$

Orifice θ , deg	s, in.	s/D	s/s*	$\theta = 0.0^\circ, P_t = 7871.9 \text{ psf}$					$\theta = 22.5^\circ, P_t = 7871.9 \text{ psf}$					$\theta = 45.0^\circ, P_t = 7871.9 \text{ psf}$				
				P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t	P_t , psf	C_p	$P_t/P_{t,2}$	$P_t/P_{t,\infty}$	M_t
1	0	.230	.000	596.3	1.649	.91735	25.74527	.3523	596.3	1.649	.91735	25.74527	.3523	596.3	1.649	.91735	25.74527	.3523
2	0	.230	.025	591.5	1.635	.90505	25.40016	.3661	591.5	1.635	.90505	25.40016	.3661	591.5	1.635	.90505	25.40016	.3661
3	0	.430	.050	588.3	1.626	.90259	25.33114	.3802	588.3	1.626	.90259	25.33114	.3802	588.3	1.626	.90259	25.33114	.3802
4	0	.530	.100	586.7	1.621	.89767	25.19310	.3854	586.7	1.621	.89767	25.19310	.3854	586.7	1.621	.89767	25.19310	.3854
5	0	.630	.150	583.5	1.612	.89059	24.98603	.3958	583.5	1.612	.89059	24.98603	.3958	583.5	1.612	.89059	24.98603	.3958
6	0	1.230	.250	578.7	1.598	.88537	24.64788	.4206	578.7	1.598	.88537	24.64788	.4206	578.7	1.598	.88537	24.64788	.4206
7	0	1.230	.300	575.5	1.583	.87800	24.43365	.4351	575.5	1.583	.87800	24.43365	.4351	575.5	1.583	.87800	24.43365	.4351
8	0	1.430	.350	570.7	1.575	.87062	24.22679	.4493	570.7	1.575	.87062	24.22679	.4493	570.7	1.575	.87062	24.22679	.4493
9	0	1.630	.400	565.9	1.562	.86324	24.03932	.4632	565.9	1.562	.86324	24.03932	.4632	565.9	1.562	.86324	24.03932	.4632
10	0	1.830	.450	561.1	1.548	.85586	23.86634	.4768	561.1	1.548	.85586	23.86634	.4768	561.1	1.548	.85586	23.86634	.4768
11	0	2.030	.500	556.5	1.534	.84839	23.70352	.4902	556.5	1.534	.84839	23.70352	.4902	556.5	1.534	.84839	23.70352	.4902
12	0	2.230	.550	551.9	1.521	.84100	23.54674	.5033	551.9	1.521	.84100	23.54674	.5033	551.9	1.521	.84100	23.54674	.5033
13	0	2.430	.600	547.3	1.508	.83367	23.39145	.5163	547.3	1.508	.83367	23.39145	.5163	547.3	1.508	.83367	23.39145	.5163
14	0	2.630	.650	542.7	1.497	.82635	23.23634	.5292	542.7	1.497	.82635	23.23634	.5292	542.7	1.497	.82635	23.23634	.5292
15	0	2.830	.700	538.1	1.487	.81905	23.08134	.5419	538.1	1.487	.81905	23.08134	.5419	538.1	1.487	.81905	23.08134	.5419
16	0	3.030	.750	533.5	1.479	.81179	22.92634	.5547	533.5	1.479	.81179	22.92634	.5547	533.5	1.479	.81179	22.92634	.5547
17	0	3.230	.800	529.1	1.472	.80450	22.77134	.5673	529.1	1.472	.80450	22.77134	.5673	529.1	1.472	.80450	22.77134	.5673
18	0	3.430	.850	524.7	1.466	.79719	22.61634	.5798	524.7	1.466	.79719	22.61634	.5798	524.7	1.466	.79719	22.61634	.5798
19	0	3.630	.900	520.3	1.461	.78986	22.46134	.5922	520.3	1.461	.78986	22.46134	.5922	520.3	1.461	.78986	22.46134	.5922
20	0	3.830	.950	516.0	1.457	.78250	22.30634	.6046	516.0	1.457	.78250	22.30634	.6046	516.0	1.457	.78250	22.30634	.6046
21	0	4.030	.1000	511.6	1.454	.77512	22.15134	.6169	511.6	1.454	.77512	22.15134	.6169	511.6	1.454	.77512	22.15134	.6169
22	0	4.230	.1050	507.3	1.452	.76772	22.00000	.6291	507.3	1.452	.76772	22.00000	.6291	507.3	1.452	.76772	22.00000	.6291
23	0	4.430	.1100	503.0	1.451	.76029	21.84866	.6413	503.0	1.451	.76029	21.84866	.6413	503.0	1.451	.76029	21.84866	.6413
24	0	4.630	.1150	498.7	1.451	.75282	21.69722	.6534	498.7	1.451	.75282	21.69722	.6534	498.7	1.451	.75282	21.69722	.6534
25	0	4.830	.1200	494.4	1.452	.74532	21.54572	.6655	494.4	1.452	.74532	21.54572	.6655	494.4	1.452	.74532	21.54572	.6655
26	0	5.030	.1250	490.1	1.454	.73778	21.39416	.6774	490.1	1.454	.73778	21.39416	.6774	490.1	1.454	.73778	21.39416	.6774
27	0	5.230	.1300	485.8	1.457	.73020	21.24254	.6894	485.8	1.457	.73020	21.24254	.6894	485.8	1.457	.73020	21.24254	.6894
28	0	5.430	.1350	481.5	1.461	.72258	21.09086	.7013	481.5	1.461	.72258	21.09086	.7013	481.5	1.461	.72258	21.09086	.7013
29	0	5.630	.1400	477.2	1.466	.71492	20.93916	.7132	477.2	1.466	.71492	20.93916	.7132	477.2	1.466	.71492	20.93916	.7132
30	0	5.830	.1450	472.9	1.472	.70720	20.78740	.7250	472.9	1.472	.70720	20.78740	.7250	472.9	1.472	.70720	20.78740	.7250
31	0	6.030	.1500	468.6	1.479	.69944	20.63558	.7368	468.6	1.479	.69944	20.63558	.7368	468.6	1.479	.69944	20.63558	.7368
32	0	6.230	.1550	464.3	1.487	.69163	20.48370	.7486	464.3	1.487	.69163	20.48370	.7486	464.3	1.487	.69163	20.48370	.7486
33	0	6.430	.1600	460.0	1.496	.68377	20.33176	.7603	460.0	1.496	.68377	20.33176	.7603	460.0	1.496	.68377	20.33176	.7603
34	0	6.630	.1650	455.7	1.506	.67586	20.17976	.7720	455.7	1.506	.67586	20.17976	.7720	455.7	1.506	.67586	20.17976	.7720
35	0	6.830	.1700	451.4	1.517	.66790	20.02770	.7837	451.4	1.517	.66790	20.02770	.7837	451.4	1.517	.66790	20.02770	.7837
36	0	7.030	.1750	447.1	1.529	.65989	19.87558	.7953	447.1	1.529	.65989	19.87558	.7953	447.1	1.529	.65989	19.87558	.7953
37	0	7.230	.1800	442.8	1.542	.65183	19.72350	.8068	442.8	1.542	.65183	19.72350	.8068	442.8	1.542	.65183	19.72350	.8068
38	0	7.430	.1850	438.5	1.556	.64372	19.57146	.8183	438.5	1.556	.64372	19.57146	.8183	438.5	1.556	.64372	19.57146	.8183
39	0	7.630	.1900	434.2	1.571	.63556	19.41946	.8297	434.2	1.571	.63556	19.41946	.8297	434.2	1.571	.63556	19.41946	.8297
40	0	7.830	.1950	429.9	1.587	.62735	19.26750	.8411	429.9	1.587	.62735	19.26750	.8411	429.9	1.587	.62735	19.26750	.8411
41	0	8.030	.2000	425.6	1.604	.61909	19.11558	.8524	425.6	1.604	.61909	19.11558	.8524	425.6	1.604	.61909	19.11558	.8524
42	0	8.230	.2050	421.3	1.622	.61078	18.96370	.8637	421.3	1.622	.61078	18.96370	.8637	421.3	1.622	.61078	18.96370	.8637
43	0	8.430	.2100	417.0	1.641	.60242	18.81186	.8749	417.0	1.641	.60242	18.81186	.8749	417.0	1.641	.60242	18.81186	.8749
44	0	8.630	.2150	412.7	1.661	.59401	18.66006	.8861	412.7	1.661	.59401	18.66006	.8861	412.7	1.661	.59401	18.66006	.8861
45	0	8.830	.2200	408.4	1.682	.58556	18.50834	.8972	408.4	1.682	.58556	18.50834	.8972	408.4	1.682	.58556	18.50834	.8972
46	0	9.030	.2250	404.1	1.704	.57707	18.35660	.9083	404.1	1.704	.57707	18.35660	.9083	404.1	1.704	.57707	18.35660	.9083
47	0	9.230	.2300	400.0	1.727	.56856	18.20486	.9194	400.0	1.727	.56856	18.20486	.9194	400.0	1.727	.56856	18.20486	.9194
48	0	9.430	.2350	395.7	1.750	.56006	18.05312	.9304	395.7	1.750	.56006	18.05312	.9304	395.7	1.750	.56006	18.05312	.9304
49	0	9.630	.2400	391.4	1.773	.55156	17.90138	.9414	391.4	1.773	.55156	17.90138	.9414	391.4	1.773	.55156	17.90138	.9414
50	0	9.830	.2450	387.1	1.797	.54306	17.74964	.9524	387.1	1.797	.54306	17.74964	.9524	387.1	1.797	.54306	17.74964	.9524
51	0	10.030	.2500	382.8	1.821	.53456	17.59790	.9634	382.8	1.821	.53456	17.59790	.9634	382.8	1.821	.53456	17.59790	.9634
52	0	10.230	.2550	378.5	1.845	.52606	17.44616	.9744	378.5	1.845	.52606	17.44616	.9744	378.5	1.845	.52606	17.44616	.9744
53	0	10.430	.2600	374.2	1.869	.51756	17.29442	.9854	374.2	1.869	.51756	17.29442	.9854	374.2	1.869	.51756	17.29442	.9854
54	0	10.630	.2650	369.9	1.893	.50906	17.14268	.9964	369.9	1.893	.50906	17.14268	.9964	369.9	1.893	.50906	17.14268	.9964
55	0	10.830	.2700	365.6	1.917	.50056	16.99094	1.0074	365.6	1.917	.50056	16.99094	1.0074	365.6	1.917	.50056	16.99094	1.0074
56	0	11.030	.2750	361.3	1.941	.49206	16.83920	1.0184	361.3	1.941	.49206	16.83920	1.0184	361.3	1.941	.49206	16.83920	1.0184
57	0	11.230	.2800	357.0	1.965	.48356	16.68746	1.0294	357.0	1.965	.48356	16.68746	1.0294	357.0	1.965	.48356	16.68746	1.0294
58	0	11.430	.2850	352.7	1.989	.47506	16.53572	1.0404	352.7	1.989	.47506	16.53572	1.0404	352.7	1.989	.47506	16.53572	1.0404
59	0	11.630	.2900	348.4	2.013	.46656	16.38398	1.0514	348.4	2.013	.46656	16.38398	1.0514	348.4	2.013	.46656	16.38398	1.0514
60	0	11.830	.2950	344.1	2.037	.45806	16.23224	1.0624	344.1	2.037	.45806	16.23224	1.0624	344.1	2.037	.45806	16.23224	1.0624
61	0	12.030	.3000	339.8	2.061	.44956	16.08050	1.0734	339.8	2.061	.44956	16.08050	1.0734	339.8	2.061	.44956	16.08050	1.0734
62	0	12.230	.3050	335.5	2.085	.44106	15.92876	1.0844	335.5	2.085	.44106	15.92876	1.0844	335.5	2.085	.44106	15.92876	1.0844
63	0	12.430	.3100	331.2	2.109	.43256	15.77702	1.0954	331.2</									

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

TABLE XII.- DATA^a FOR 180° CONE; $M_{\infty} = 4.63$ - Concluded

(e) $\alpha = 20^\circ$ - Concluded

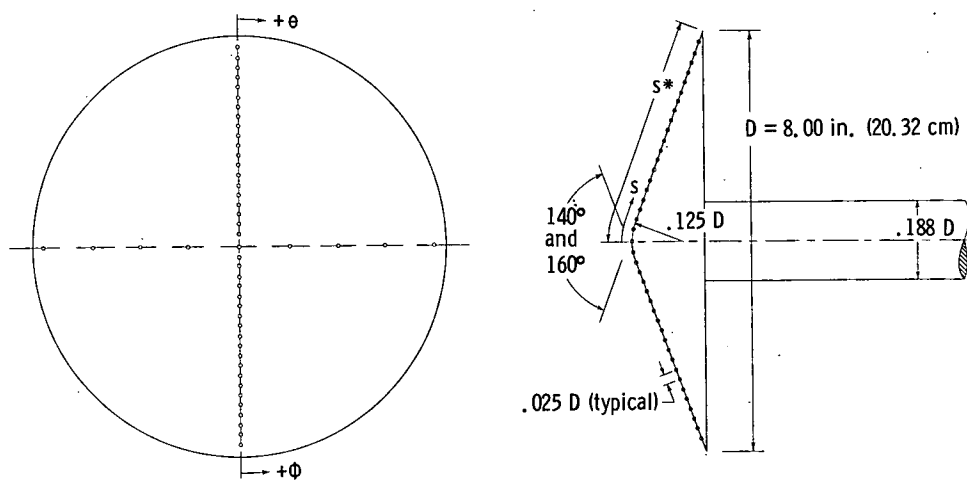
Orifice θ , deg	s , in.	s/D	s/s^*	$\Phi = 67.5^\circ, p_t = 7871.9 \text{ psf}$				$\Phi = 90.0^\circ, p_t = 7871.9 \text{ psf}$				
				$p_{t,1}$ psf	C_p	$p_{t,1}/p_{t,2}$	$p_{t,1}/p_{t,0}$	$M_{t,1}$	$p_{t,1}$ psf	C_p	$p_{t,1}/p_{t,2}$	$p_{t,1}/p_{t,0}$
1	0	.000	.0000	596.2	1.649	.91728	25.74348	.35338	596.2	1.649	.91728	25.74348
2	0	.000	.0000	596.2	1.644	.91728	25.74348	.35338	596.2	1.644	.91728	25.74348
3	0	.000	.0000	596.2	1.639	.91728	25.74348	.35338	596.2	1.639	.91728	25.74348
4	0	.000	.0000	596.2	1.634	.91728	25.74348	.35338	596.2	1.634	.91728	25.74348
5	0	.000	.0000	596.2	1.629	.91728	25.74348	.35338	596.2	1.629	.91728	25.74348
6	0	.000	.0000	596.2	1.624	.91728	25.74348	.35338	596.2	1.624	.91728	25.74348
7	0	.000	.0000	596.2	1.619	.91728	25.74348	.35338	596.2	1.619	.91728	25.74348
8	0	.000	.0000	596.2	1.614	.91728	25.74348	.35338	596.2	1.614	.91728	25.74348
9	0	.000	.0000	596.2	1.609	.91728	25.74348	.35338	596.2	1.609	.91728	25.74348
10	0	.000	.0000	596.2	1.604	.91728	25.74348	.35338	596.2	1.604	.91728	25.74348
11	0	.000	.0000	596.2	1.599	.91728	25.74348	.35338	596.2	1.599	.91728	25.74348
12	0	.000	.0000	596.2	1.594	.91728	25.74348	.35338	596.2	1.594	.91728	25.74348
13	0	.000	.0000	596.2	1.589	.91728	25.74348	.35338	596.2	1.589	.91728	25.74348
14	0	.000	.0000	596.2	1.584	.91728	25.74348	.35338	596.2	1.584	.91728	25.74348
15	0	.000	.0000	596.2	1.579	.91728	25.74348	.35338	596.2	1.579	.91728	25.74348
16	0	.000	.0000	596.2	1.574	.91728	25.74348	.35338	596.2	1.574	.91728	25.74348
17	0	.000	.0000	596.2	1.569	.91728	25.74348	.35338	596.2	1.569	.91728	25.74348
18	0	.000	.0000	596.2	1.564	.91728	25.74348	.35338	596.2	1.564	.91728	25.74348
19	0	.000	.0000	596.2	1.559	.91728	25.74348	.35338	596.2	1.559	.91728	25.74348
20	0	.000	.0000	596.2	1.554	.91728	25.74348	.35338	596.2	1.554	.91728	25.74348
21	0	.000	.0000	596.2	1.549	.91728	25.74348	.35338	596.2	1.549	.91728	25.74348
22	0	.000	.0000	596.2	1.544	.91728	25.74348	.35338	596.2	1.544	.91728	25.74348
23	0	.000	.0000	596.2	1.539	.91728	25.74348	.35338	596.2	1.539	.91728	25.74348
24	0	.000	.0000	596.2	1.534	.91728	25.74348	.35338	596.2	1.534	.91728	25.74348
25	0	.000	.0000	596.2	1.529	.91728	25.74348	.35338	596.2	1.529	.91728	25.74348
26	0	.000	.0000	596.2	1.524	.91728	25.74348	.35338	596.2	1.524	.91728	25.74348
27	0	.000	.0000	596.2	1.519	.91728	25.74348	.35338	596.2	1.519	.91728	25.74348
28	0	.000	.0000	596.2	1.514	.91728	25.74348	.35338	596.2	1.514	.91728	25.74348
29	0	.000	.0000	596.2	1.509	.91728	25.74348	.35338	596.2	1.509	.91728	25.74348
30	0	.000	.0000	596.2	1.504	.91728	25.74348	.35338	596.2	1.504	.91728	25.74348
31	0	.000	.0000	596.2	1.499	.91728	25.74348	.35338	596.2	1.499	.91728	25.74348
32	0	.000	.0000	596.2	1.494	.91728	25.74348	.35338	596.2	1.494	.91728	25.74348
33	0	.000	.0000	596.2	1.489	.91728	25.74348	.35338	596.2	1.489	.91728	25.74348
34	0	.000	.0000	596.2	1.484	.91728	25.74348	.35338	596.2	1.484	.91728	25.74348
35	0	.000	.0000	596.2	1.479	.91728	25.74348	.35338	596.2	1.479	.91728	25.74348
36	0	.000	.0000	596.2	1.474	.91728	25.74348	.35338	596.2	1.474	.91728	25.74348
37	0	.000	.0000	596.2	1.469	.91728	25.74348	.35338	596.2	1.469	.91728	25.74348
38	0	.000	.0000	596.2	1.464	.91728	25.74348	.35338	596.2	1.464	.91728	25.74348
39	0	.000	.0000	596.2	1.459	.91728	25.74348	.35338	596.2	1.459	.91728	25.74348
40	0	.000	.0000	596.2	1.454	.91728	25.74348	.35338	596.2	1.454	.91728	25.74348
41	0	.000	.0000	596.2	1.449	.91728	25.74348	.35338	596.2	1.449	.91728	25.74348
42	0	.000	.0000	596.2	1.444	.91728	25.74348	.35338	596.2	1.444	.91728	25.74348
43	0	.000	.0000	596.2	1.439	.91728	25.74348	.35338	596.2	1.439	.91728	25.74348
44	0	.000	.0000	596.2	1.434	.91728	25.74348	.35338	596.2	1.434	.91728	25.74348
45	0	.000	.0000	596.2	1.429	.91728	25.74348	.35338	596.2	1.429	.91728	25.74348

^a Conversion factors: 1 inch = 2.54 cm; 1 psf = 47.88 N/m².

Orifice number	θ , deg	s/D	s/s*	
			140° cone	160° cone
1	0	0.000	0.0000	.0000
2		.025	.0471	.0493
3		.050	.0943	.0985
4		.075	.1414	.1478
5		.100	.1886	.1971
6		.125	.2357	.2463
7		.150	.2829	.2956
8		.175	.3300	.3448
9		.200	.3772	.3941
10		.225	.4243	.4434
11		.250	.4715	.4926
12		.275	.5186	.5419
13		.300	.5658	.5912
14		.325	.6129	.6404
15		.350	.6601	.6897
16		.375	.7072	.7389
17		.400	.7544	.7882
18		.425	.8015	.8375
19		.450	.8487	.8867
20		.475	.8958	.9360
21		.500	.9430	.9852
22	180	.025	.0471	.0493
23		.050	.0943	.0985
24		.075	.1414	.1478
25		.100	.1886	.1971

Orifice number	θ , deg	s/D	s/s*	
			140° cone	160° cone
26	180	0.125	0.2357	0.2463
27		.150	.2829	.2956
28		.175	.3300	.3448
29		.200	^a .3772	.3941
30		.225	.4243	.4434
31		.250	.4715	.4926
32		.275	.5186	.5419
33		.300	.5658	.5912
34		.325	.6129	.6404
35		.350	.6601	.6897
36		.375	.7072	.7389
37		.400	.7544	.7882
38		.425	.8015	.8375
39		.450	.8487	.8867
40		.475	.8958	.9360
41		.500	.9430	.9852
42	270	.125	.2357	.2463
43		.250	.4715	.4926
44		.375	.7072	.7389
45		.500	.9430	.9852
46	90	.125	.2357	.2463
47		.250	.4715	.4926
48		.375	.7072	.7389
49		.500	.9430	.9852

^aData for orifice 29 on the 140° cone were inaccurate due to leakage.

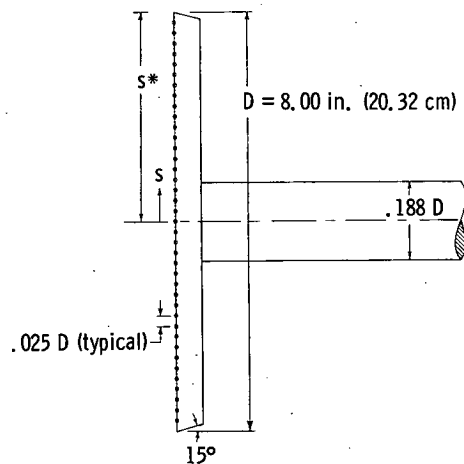
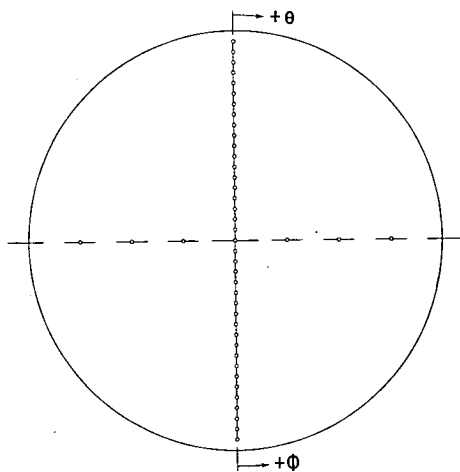


(a) 140° and 160° cones.

Figure 1.- Model details and pressure-orifice locations. (Dimensions are presented as fractions of base diameter D and total surface length s^* .)

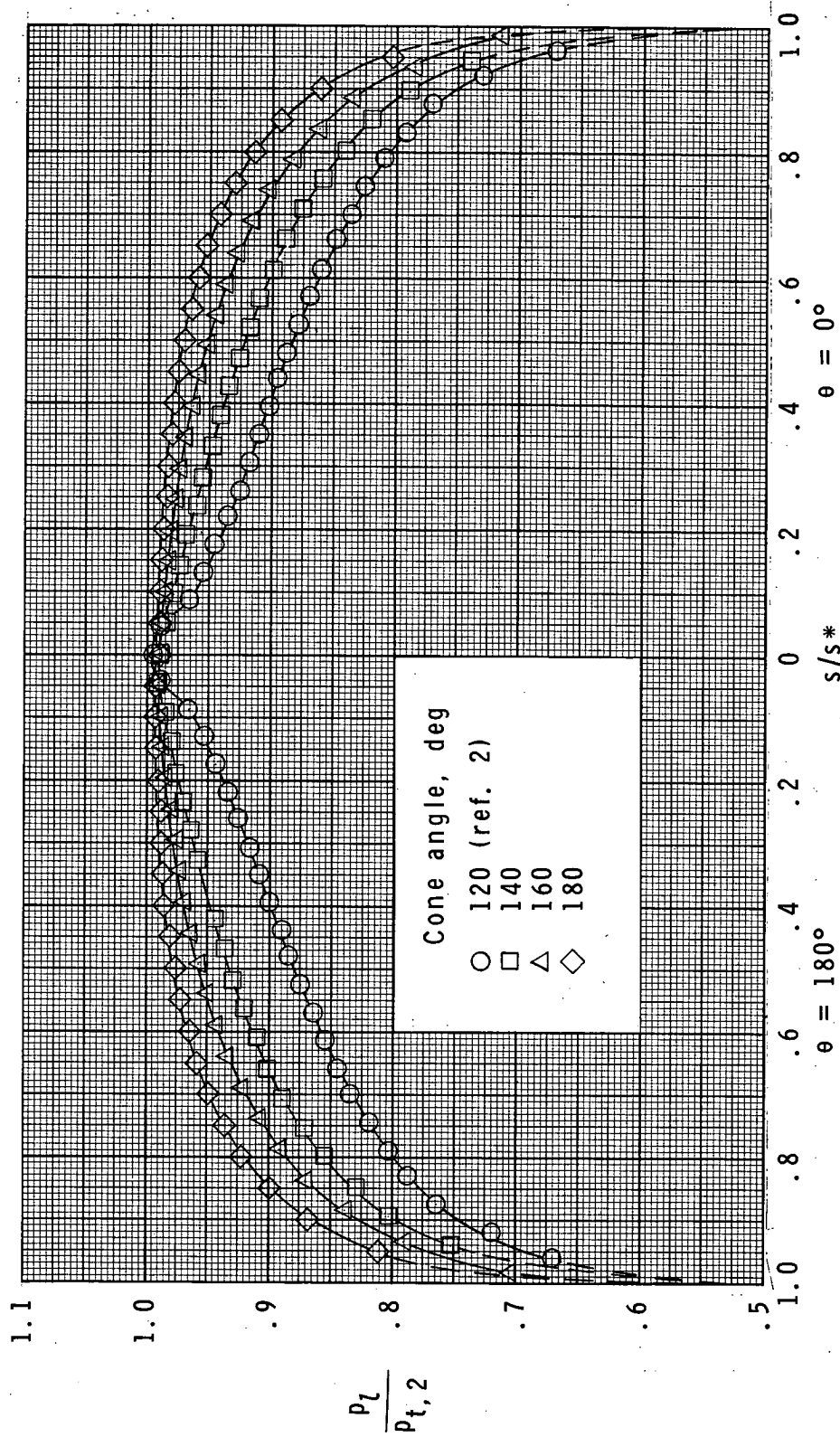
Orifice number	θ , deg	s/D	s/s^*
1	0 ↓ 180 ↓	.000	0.0000
2		.025	.0500
3		.050	.1000
4		.075	.1500
5		.100	.2000
6		.125	.2500
7		.150	.3000
8		.175	.3500
9		.200	.4000
10		.225	.4500
11		.250	.5000
12		.275	.5500
13		.300	.6000
14		.325	.6500
15		.350	.7000
16		.375	.7500
17		.400	.8000
18		.425	.8500
19		.450	.9000
20		.475	.9500
21	180 ↓	.025	.0500
22		.050	.1000
23		.075	.1500

Orifice number	θ , deg	s/D	s/s^*
24	180 ↓ 270 ↓ 90 ↓	0.100	0.2000
25		.125	.2500
26		.150	.3000
27		.175	.3500
28		.200	.4000
29		.225	.4500
30		.250	.5000
31		.275	.5500
32		.300	.6000
33		.325	.6500
34		.350	.7000
35		.375	.7500
36		.400	.8000
37		.425	.8500
38		.450	.9000
39		.475	.9500
40		.125	.2500
41		.250	.5000
42		.375	.7500
43		.125	.2500
44		.250	.5000
45		.375	.7500



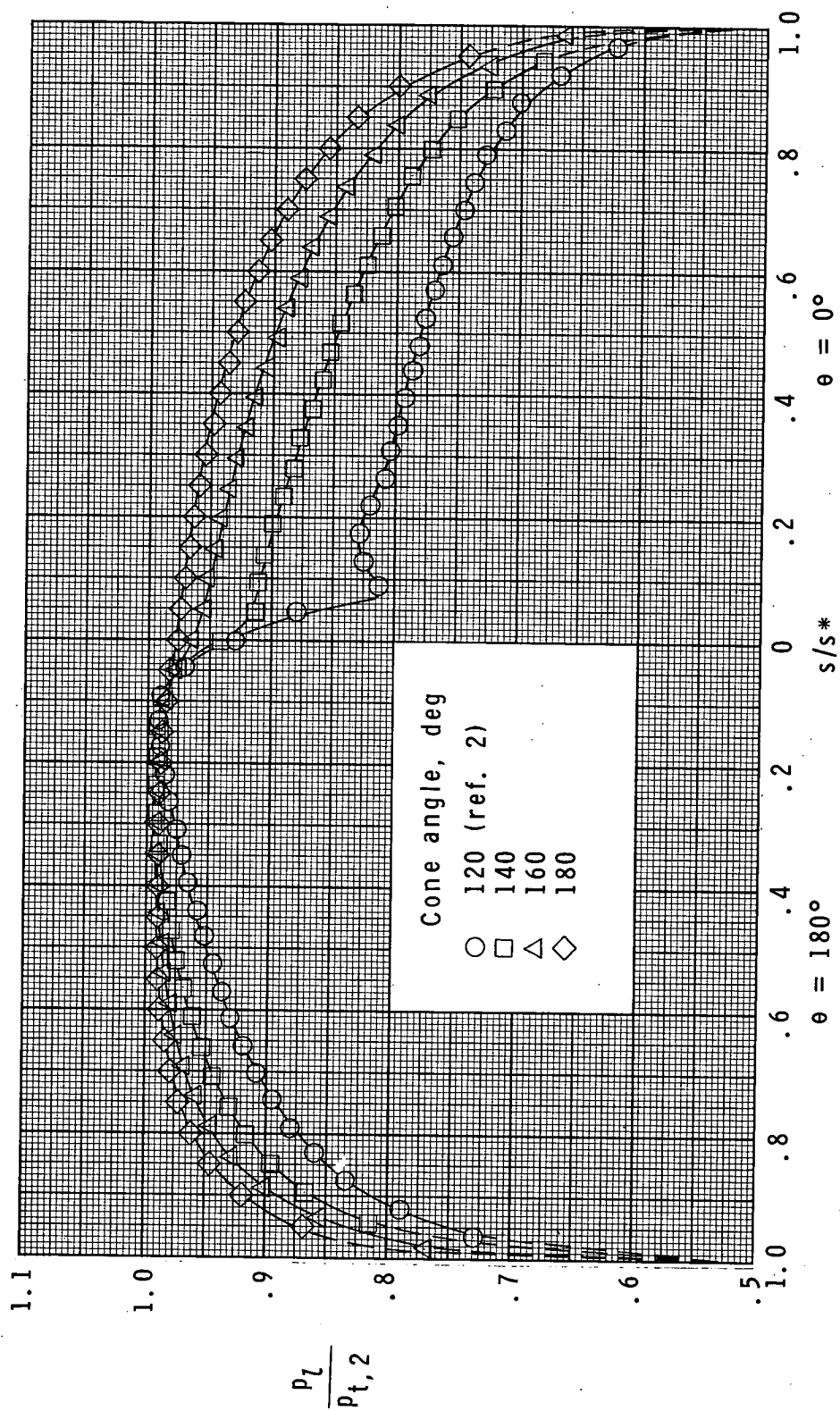
(b) 180° cone (flat disk).

Figure 1.- Concluded.



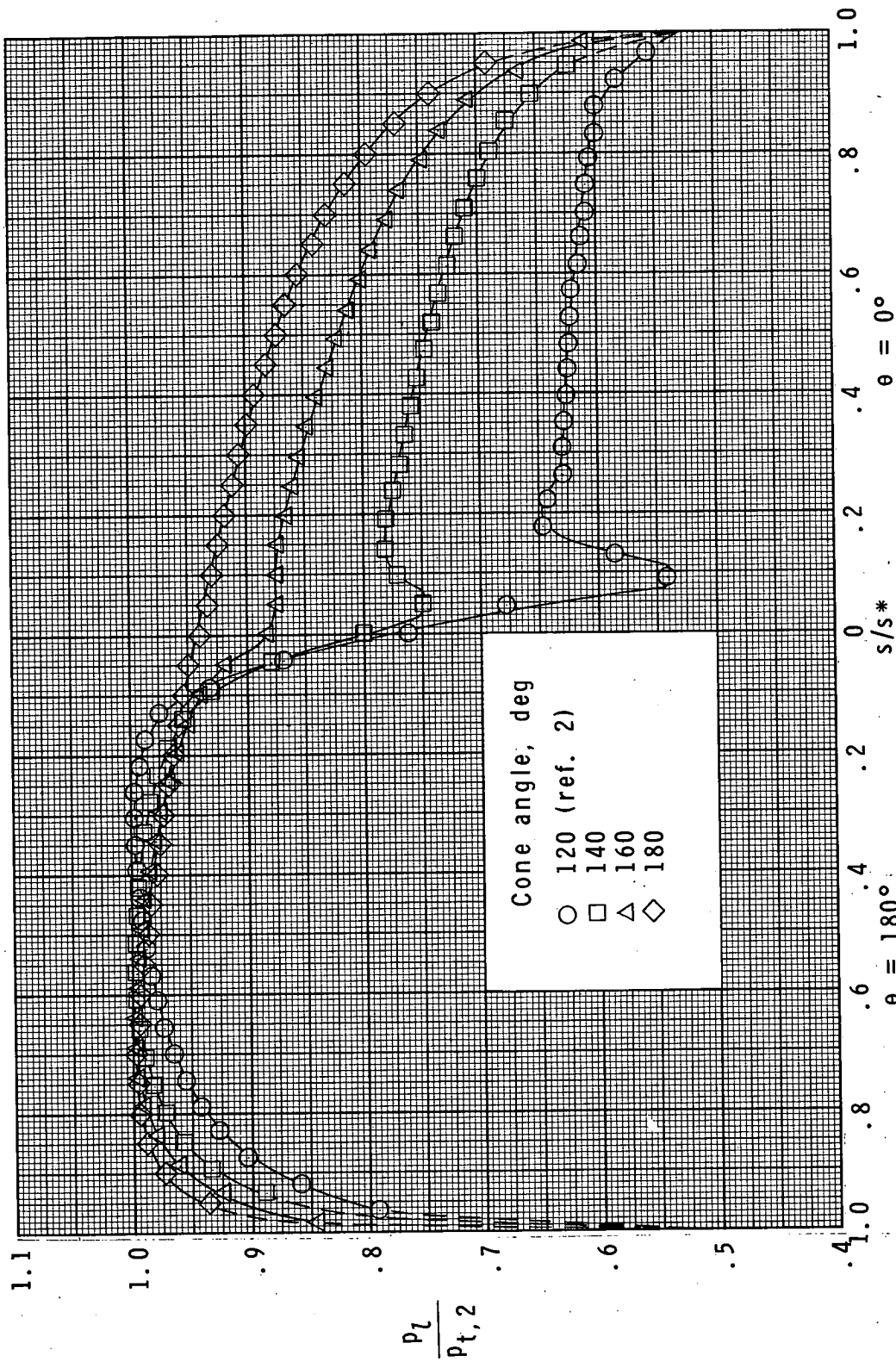
(a) $\alpha = 0^\circ$.

Figure 2.- Effect of cone angle on pressure distributions for $M_\infty = 2.96$, $\phi = 0.0^\circ$.



(b) $\alpha = 10^\circ$

Figure 2.- Continued.



(c) $\alpha = 20^\circ$.

Figure 2.- Concluded.

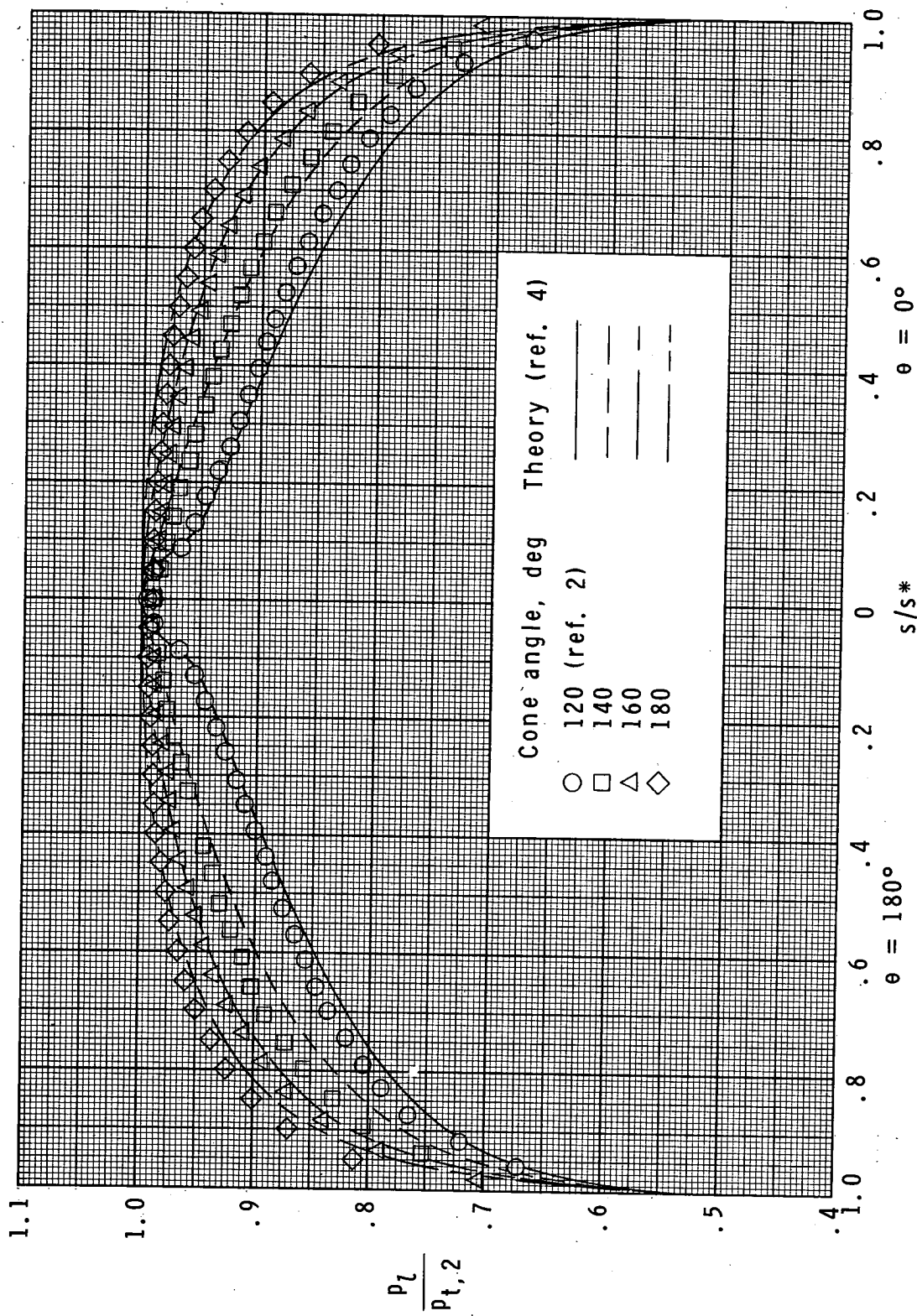
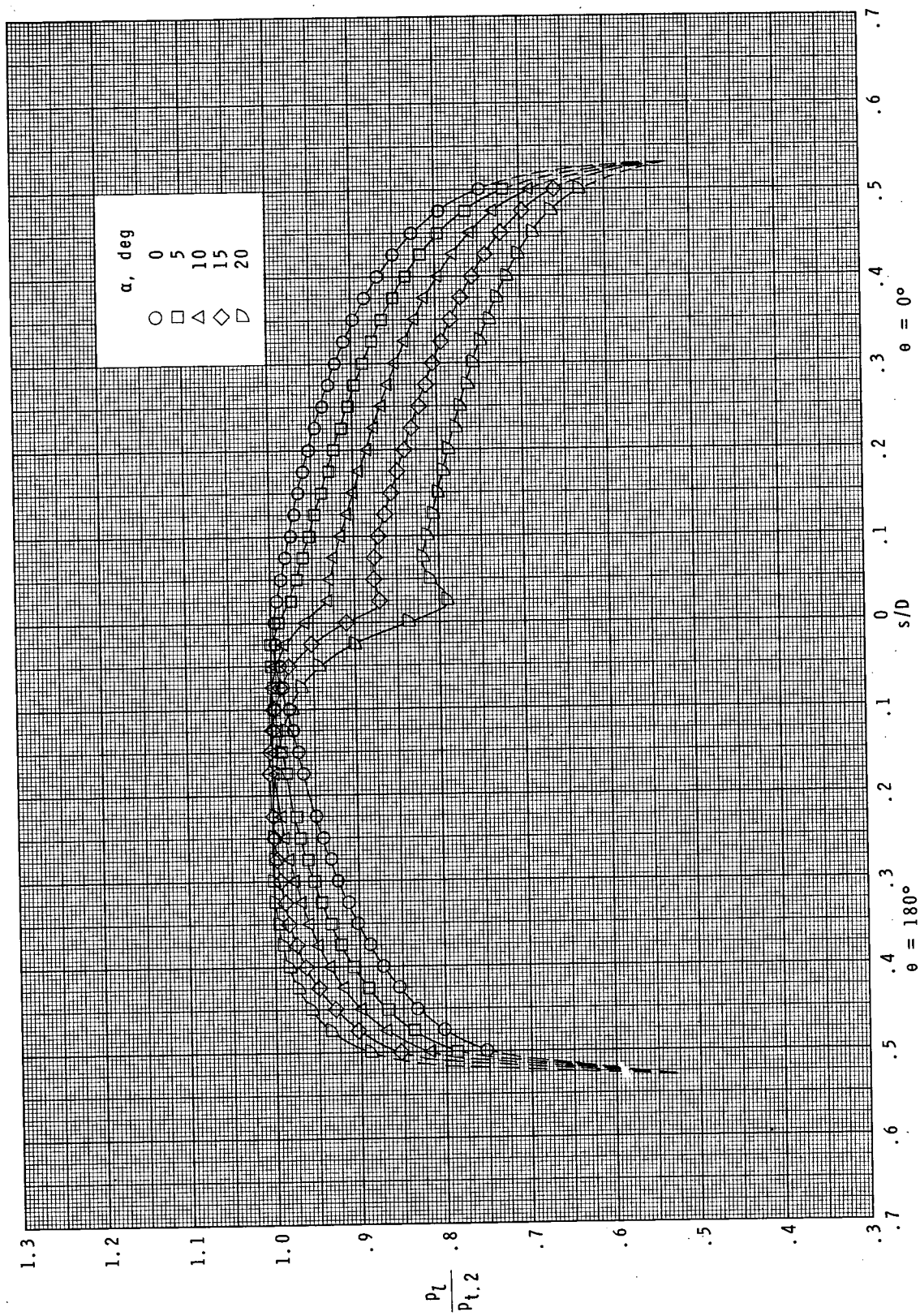
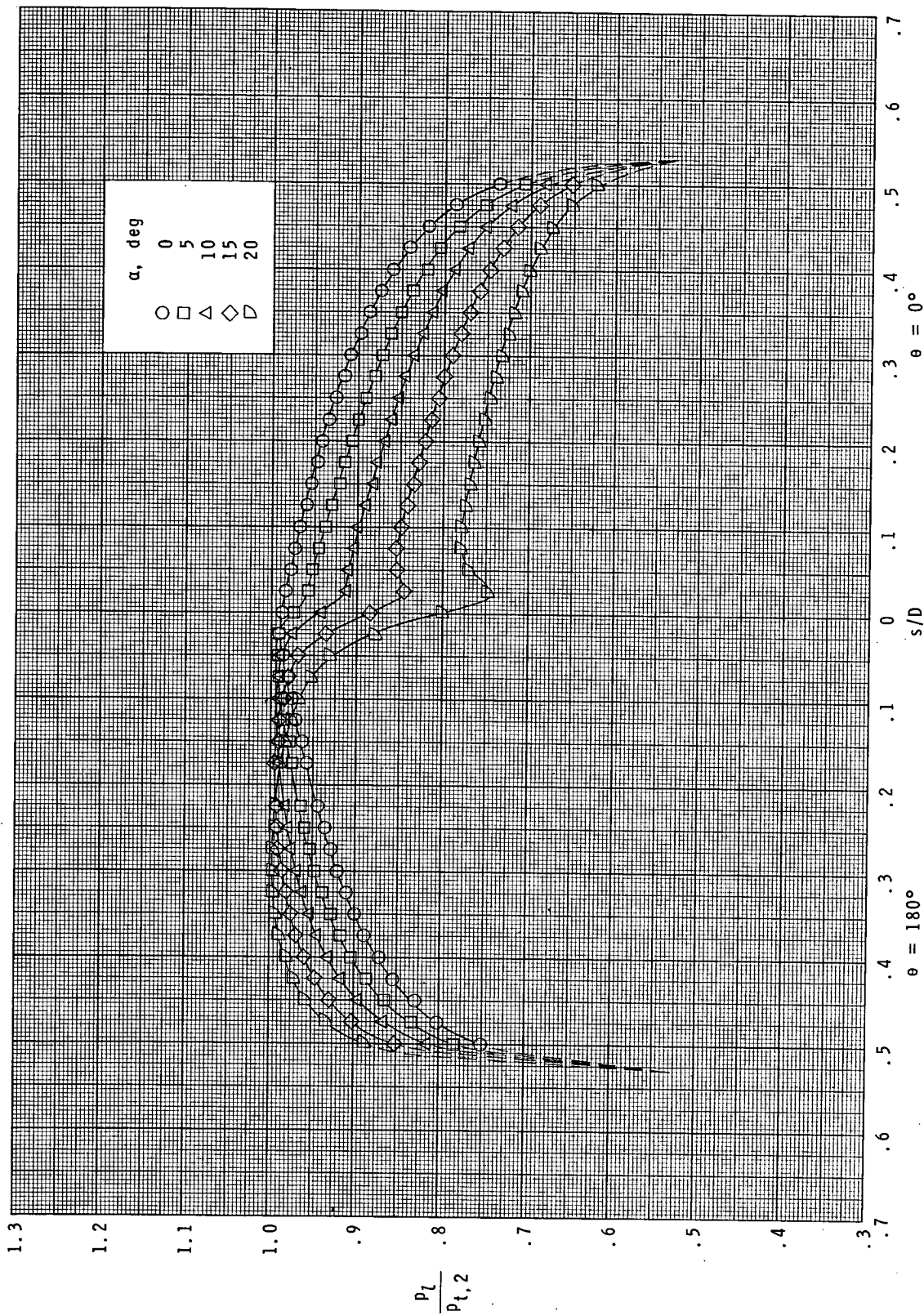


Figure 3.- Comparison of experimental and theoretical pressure distributions for cone models at $\alpha = 0^\circ$ and $M_\infty = 2.96$. $\phi = 0.0^\circ$.



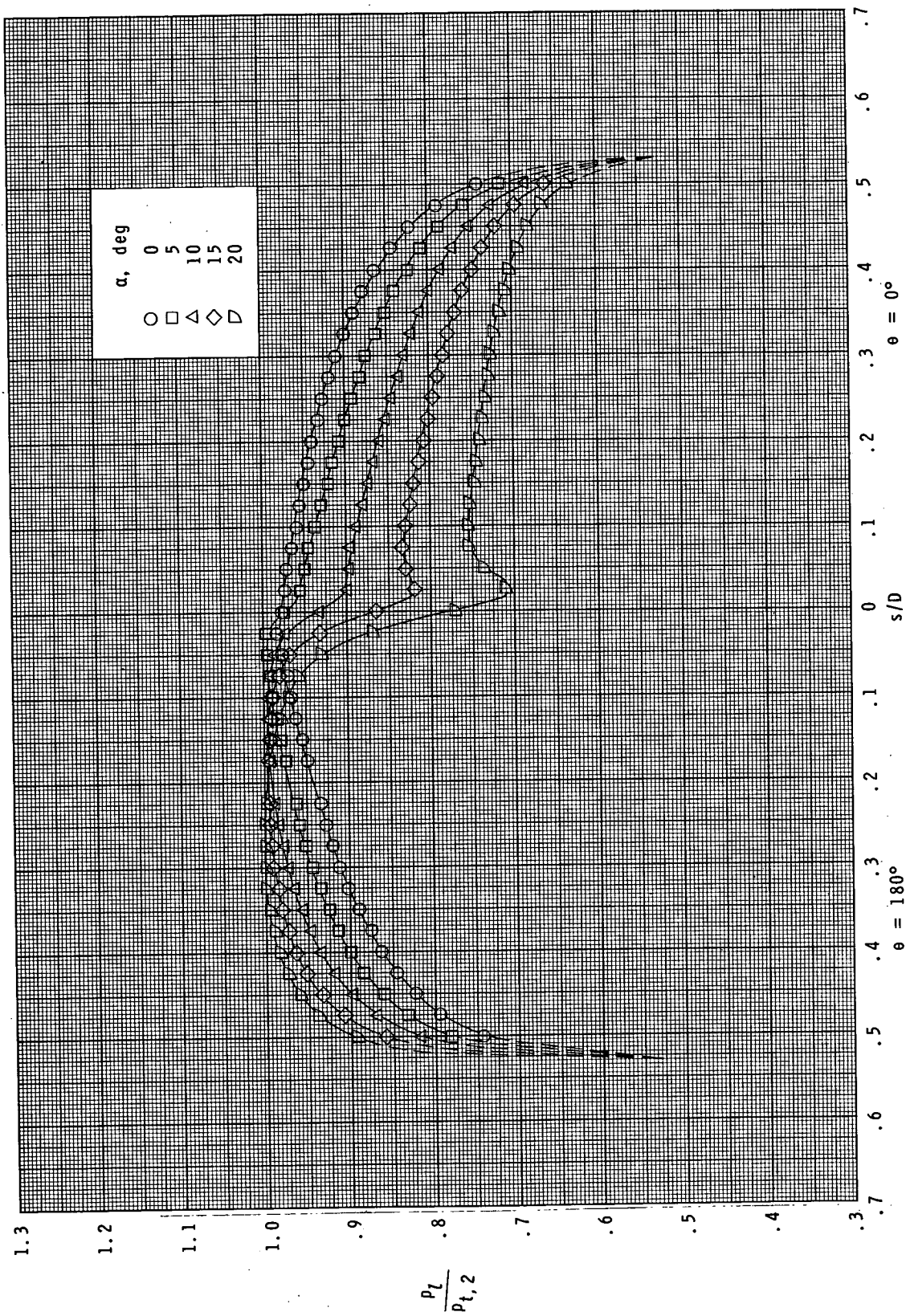
(a) $M_\infty = 2.30$.

Figure 4.- Effect of angle of attack on the pressure distributions of the 140° cone. $\phi = 0.0^\circ$.



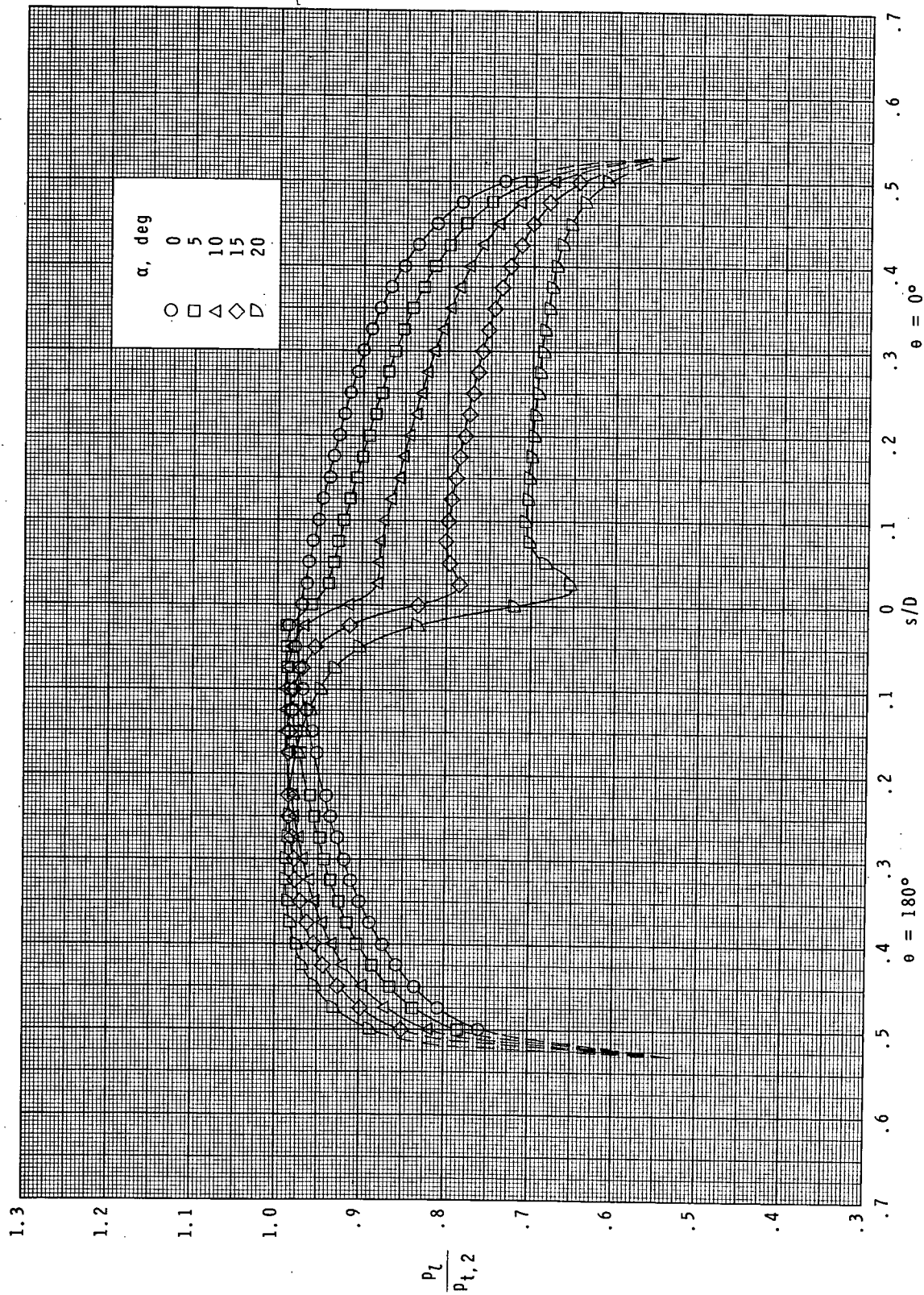
(b) $M_\infty = 2.96$.

Figure 4.- Continued.



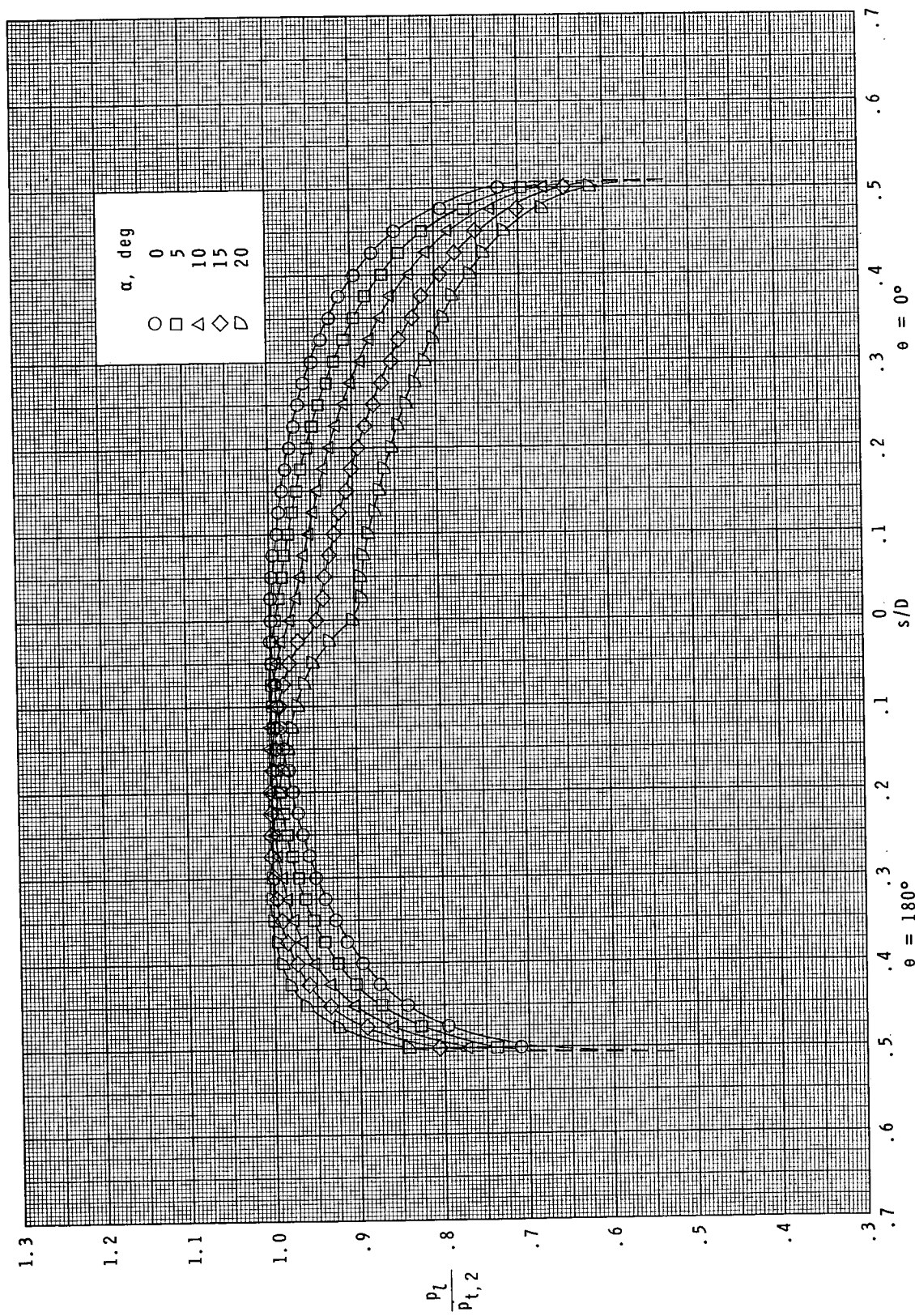
(c) $M_\infty = 3.95$.

Figure 4.- Continued.



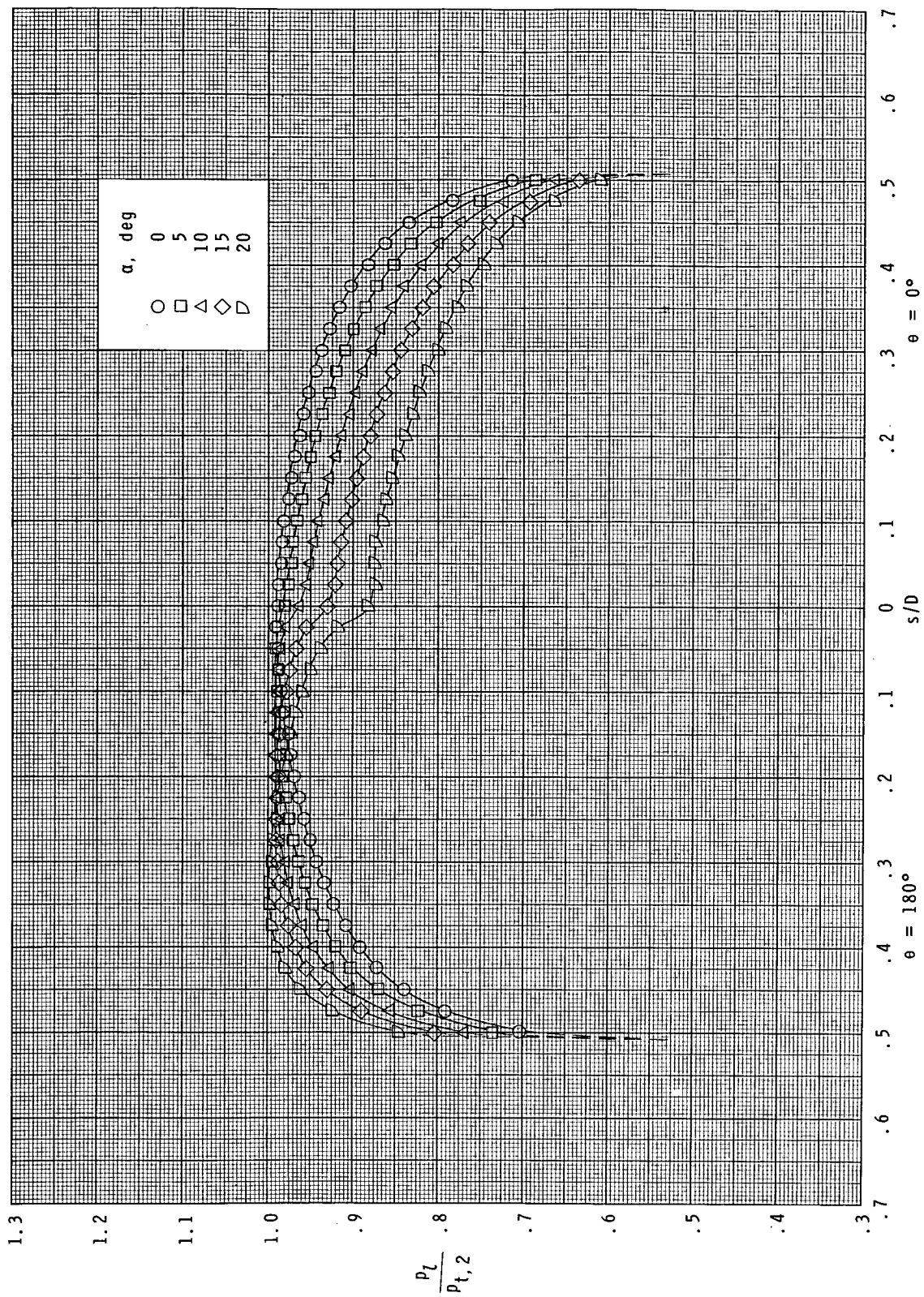
(d) $M_\infty = 4.63$;

Figure 4.- Concluded.



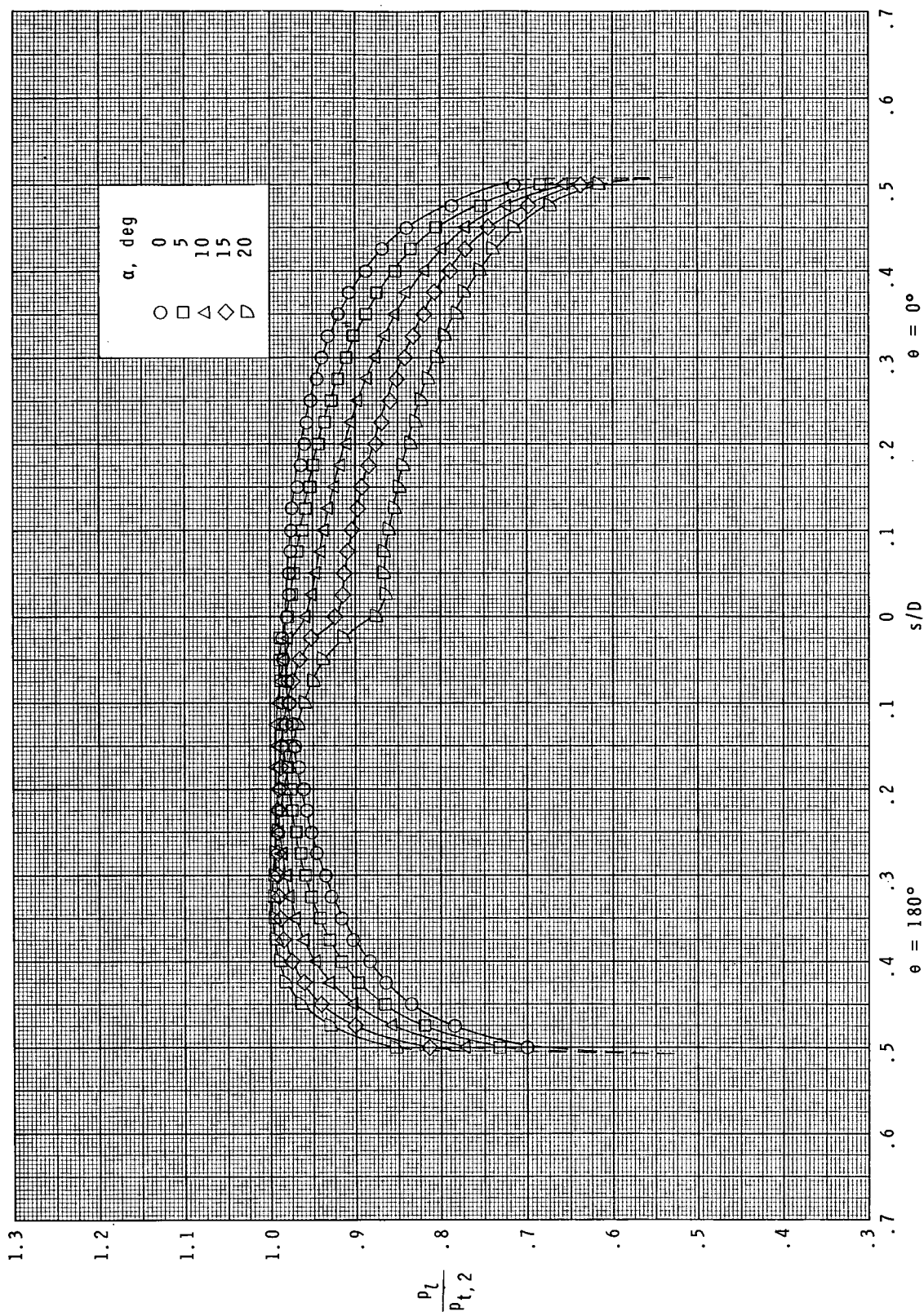
(a) $M_\infty = 2.30$.

Figure 5.- Effect of angle of attack on the pressure distributions of the 160° cone, $\phi = 0.0^\circ$.



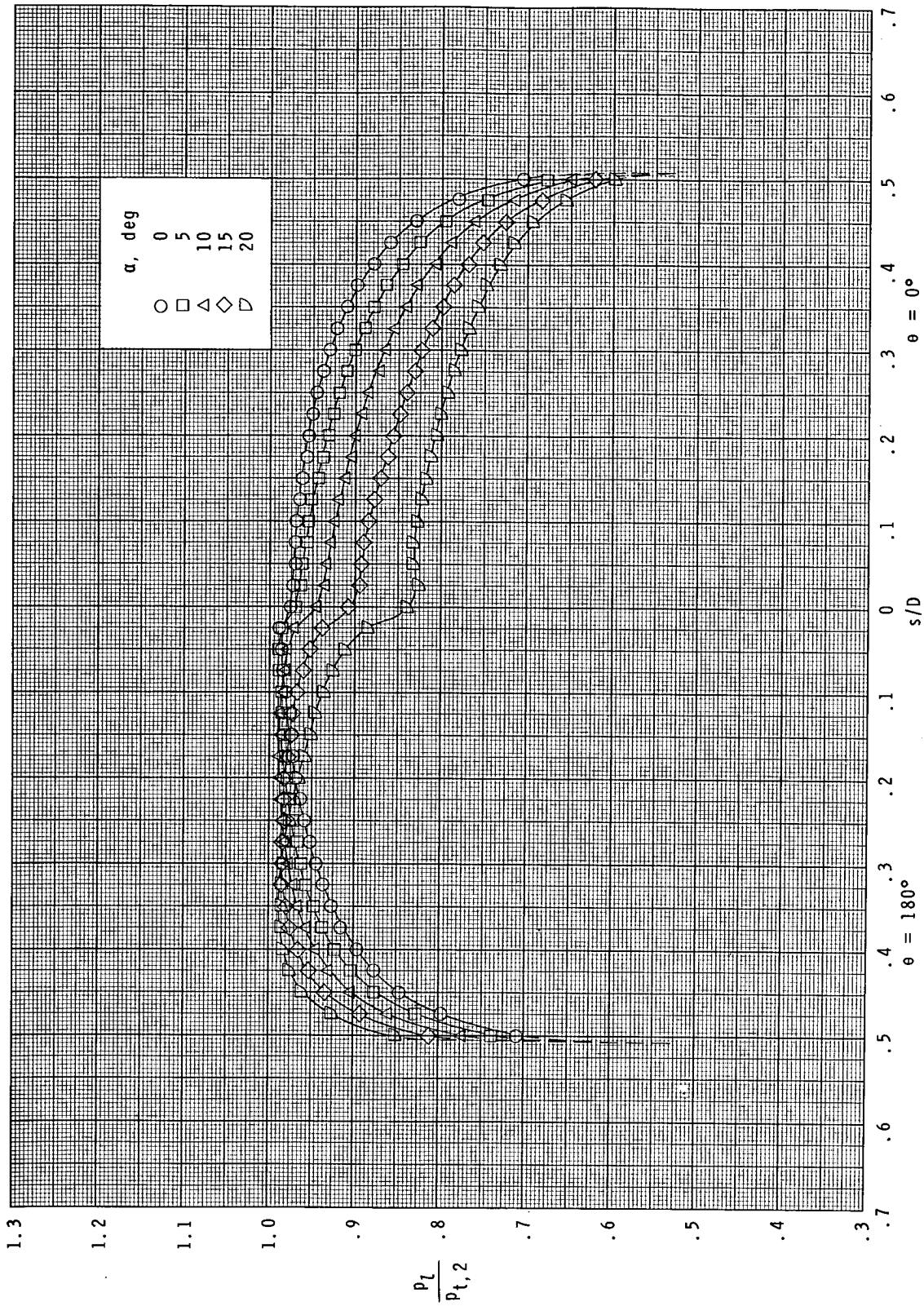
(b) $M_\infty = 2.96$.

Figure 5.- Continued.



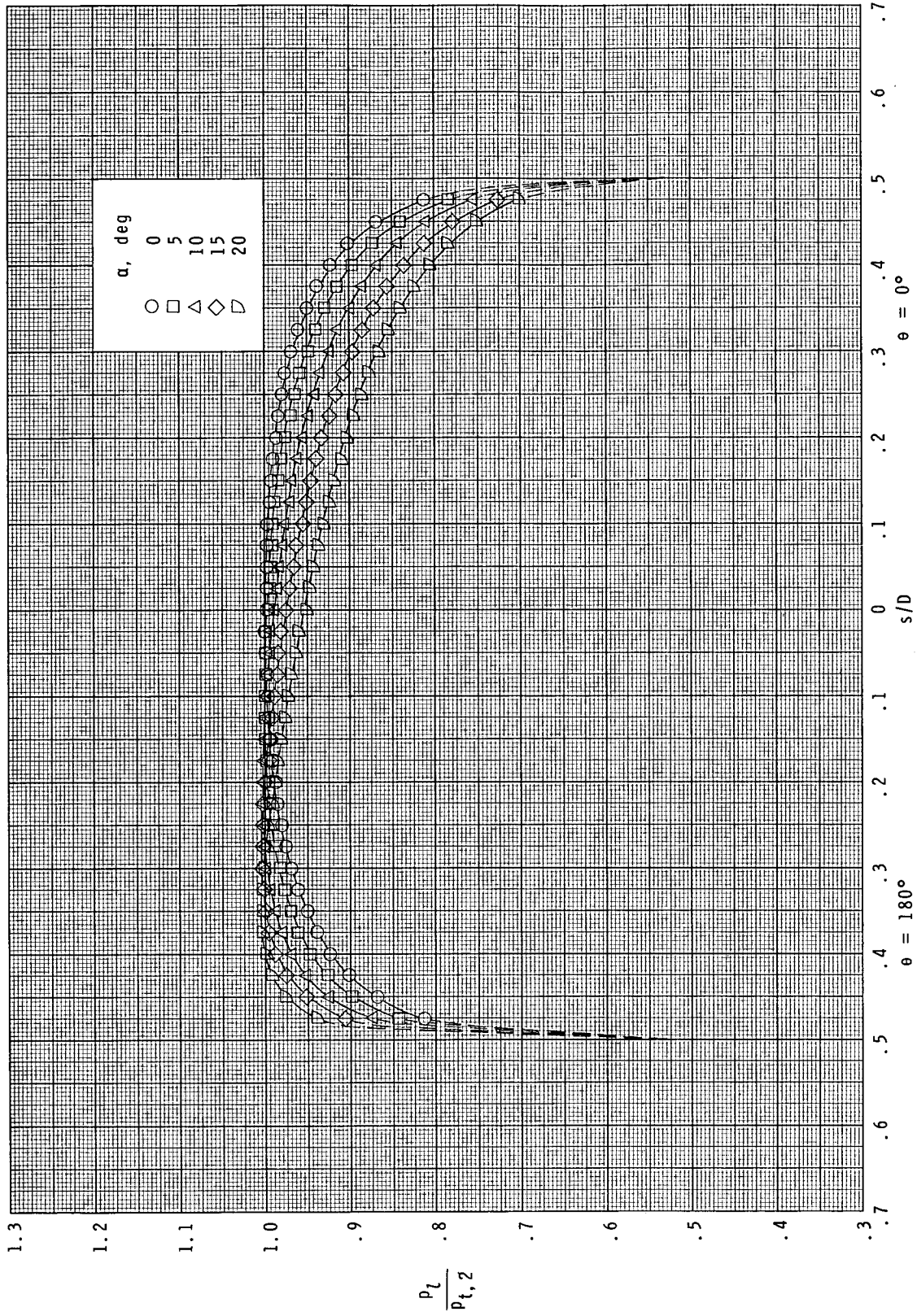
(c) $M_\infty = 3.95$.

Figure 5.- Continued.



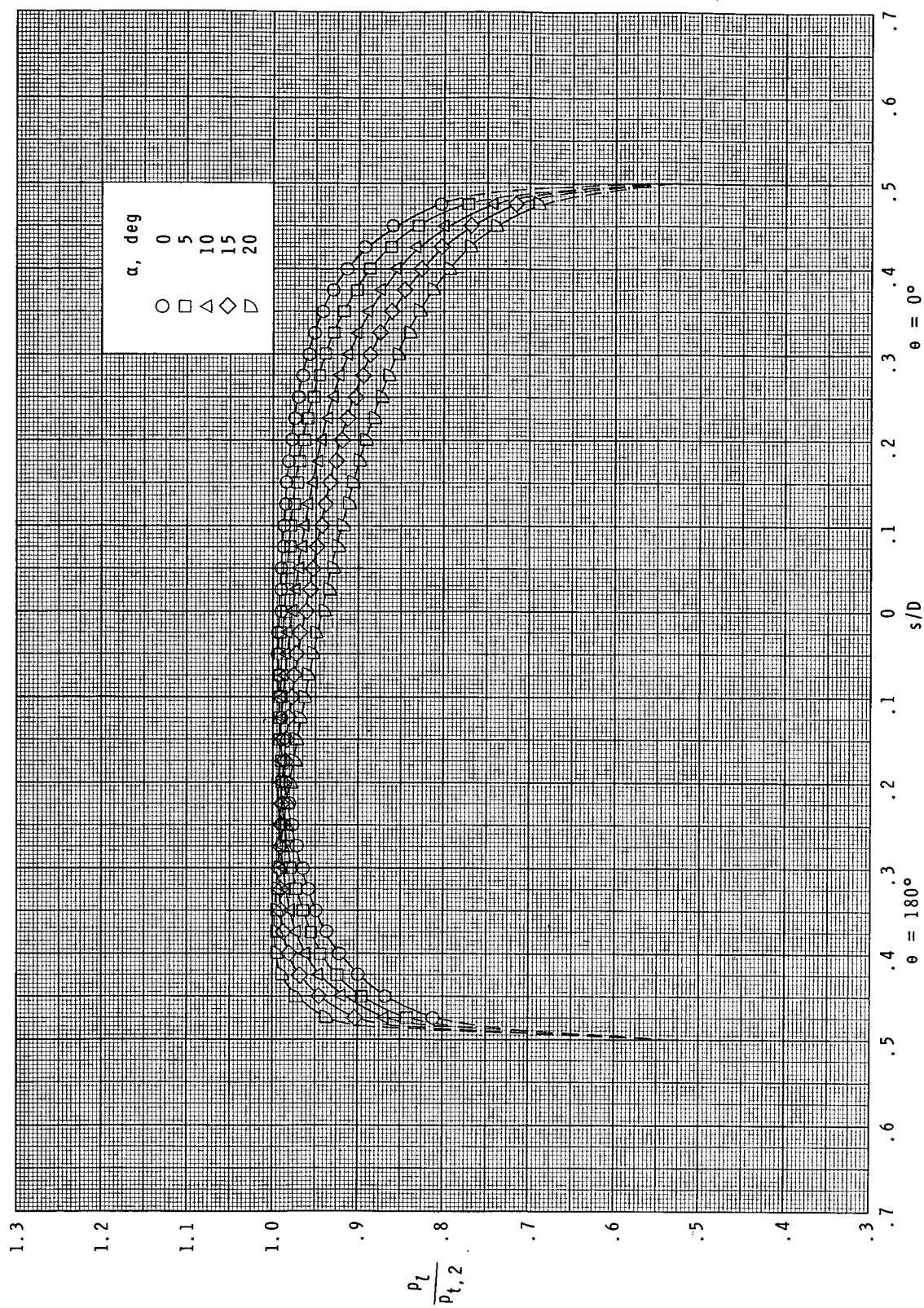
(d) $M_\infty = 4.63$.

Figure 5.- Concluded.



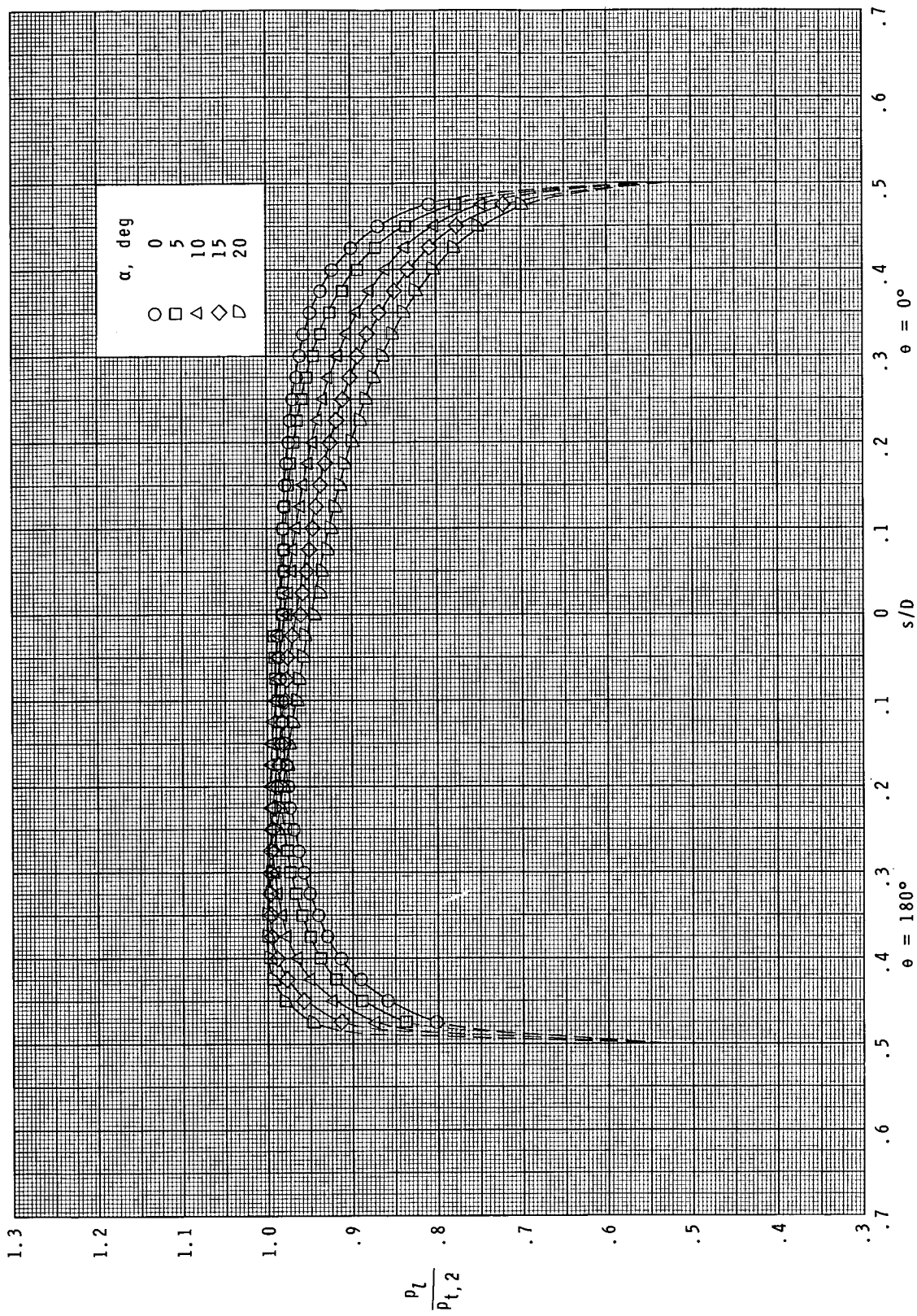
(a) $M_\infty = 2.30$.

Figure 6.- Effect of angle of attack on the pressure distributions of the 180° cone (flat disk). $\phi = 0.0^\circ$.



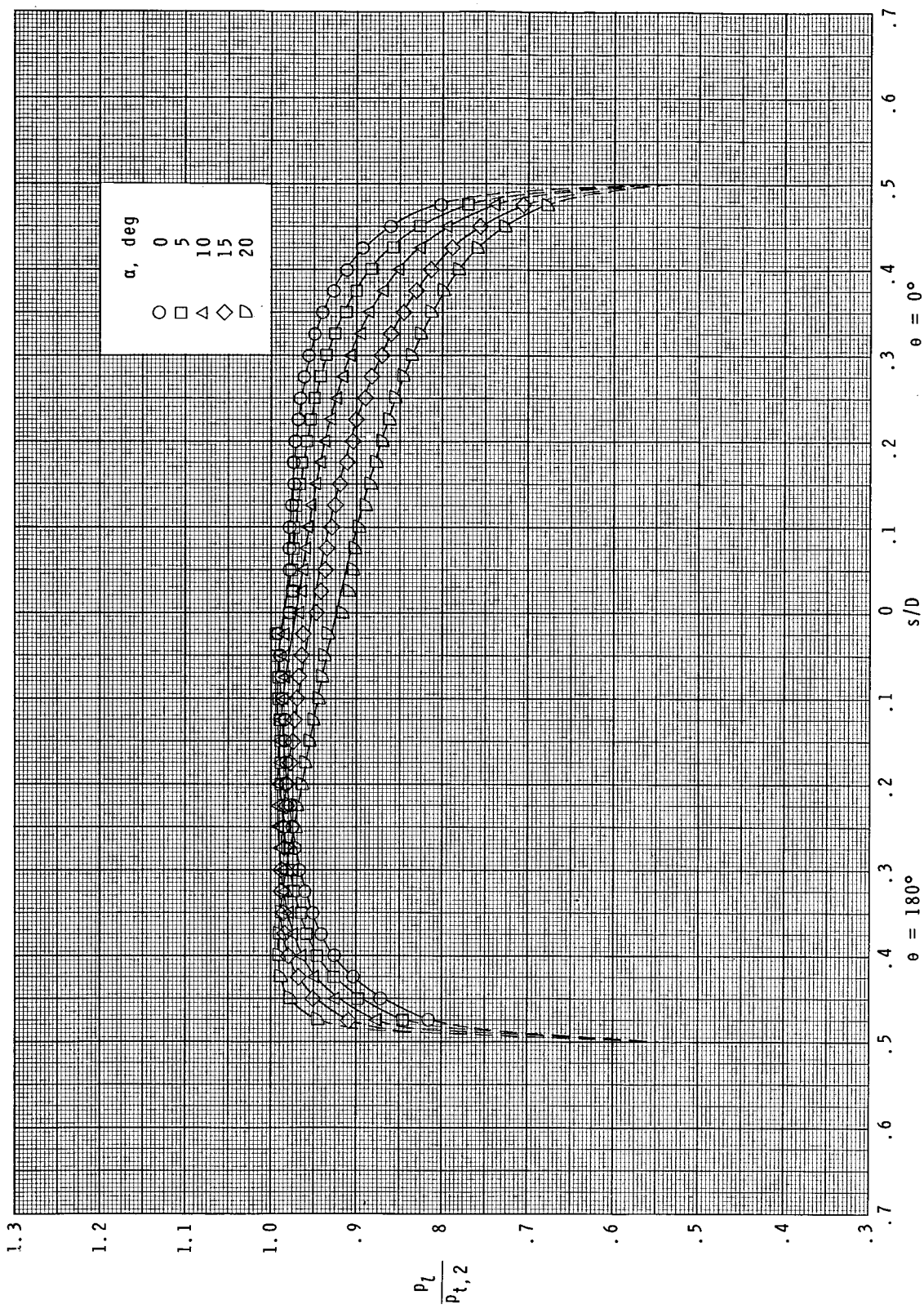
(b) $M_\infty = 2.96$.

Figure 6.- Continued.



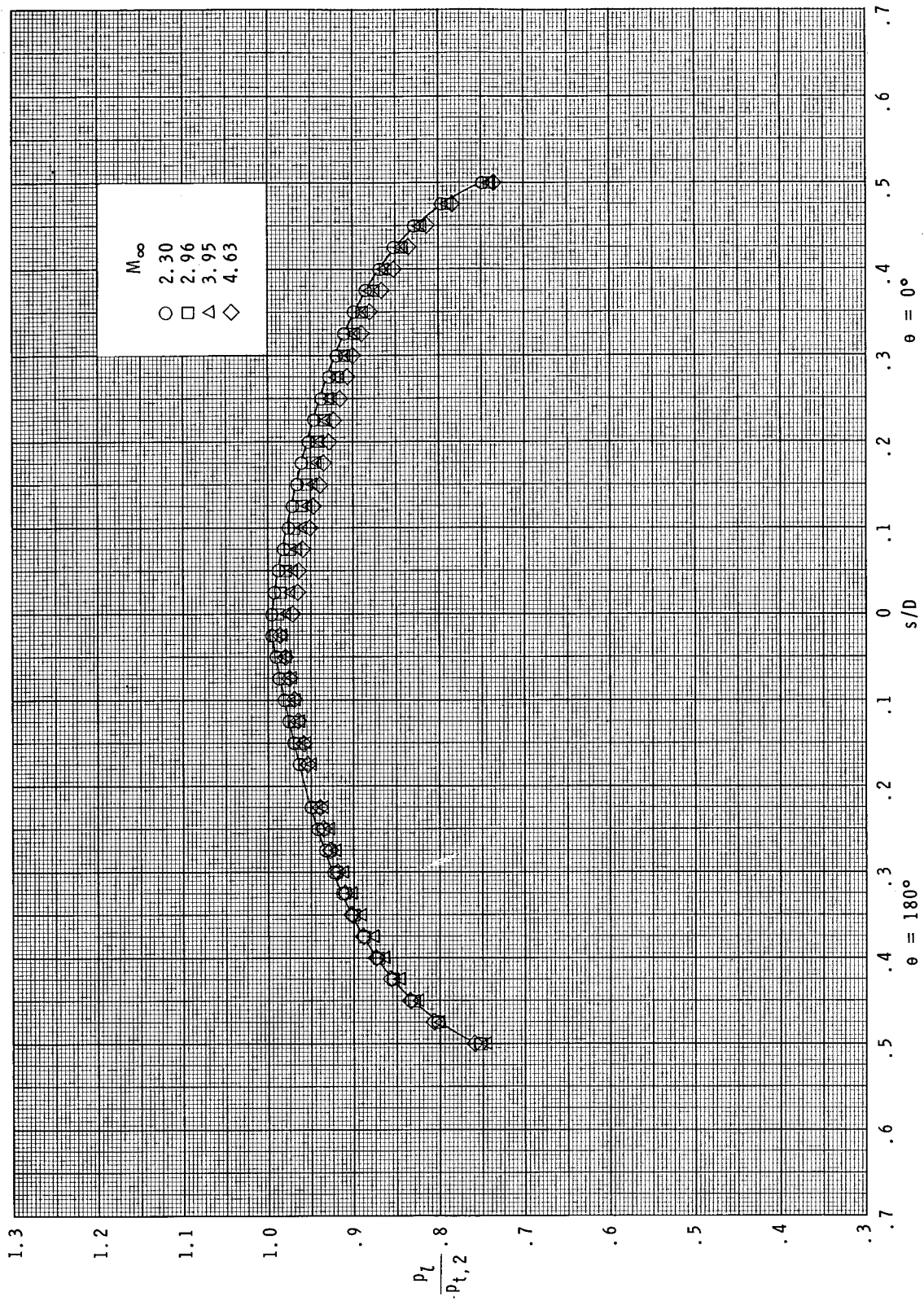
(c) $M_\infty = 3.95$.

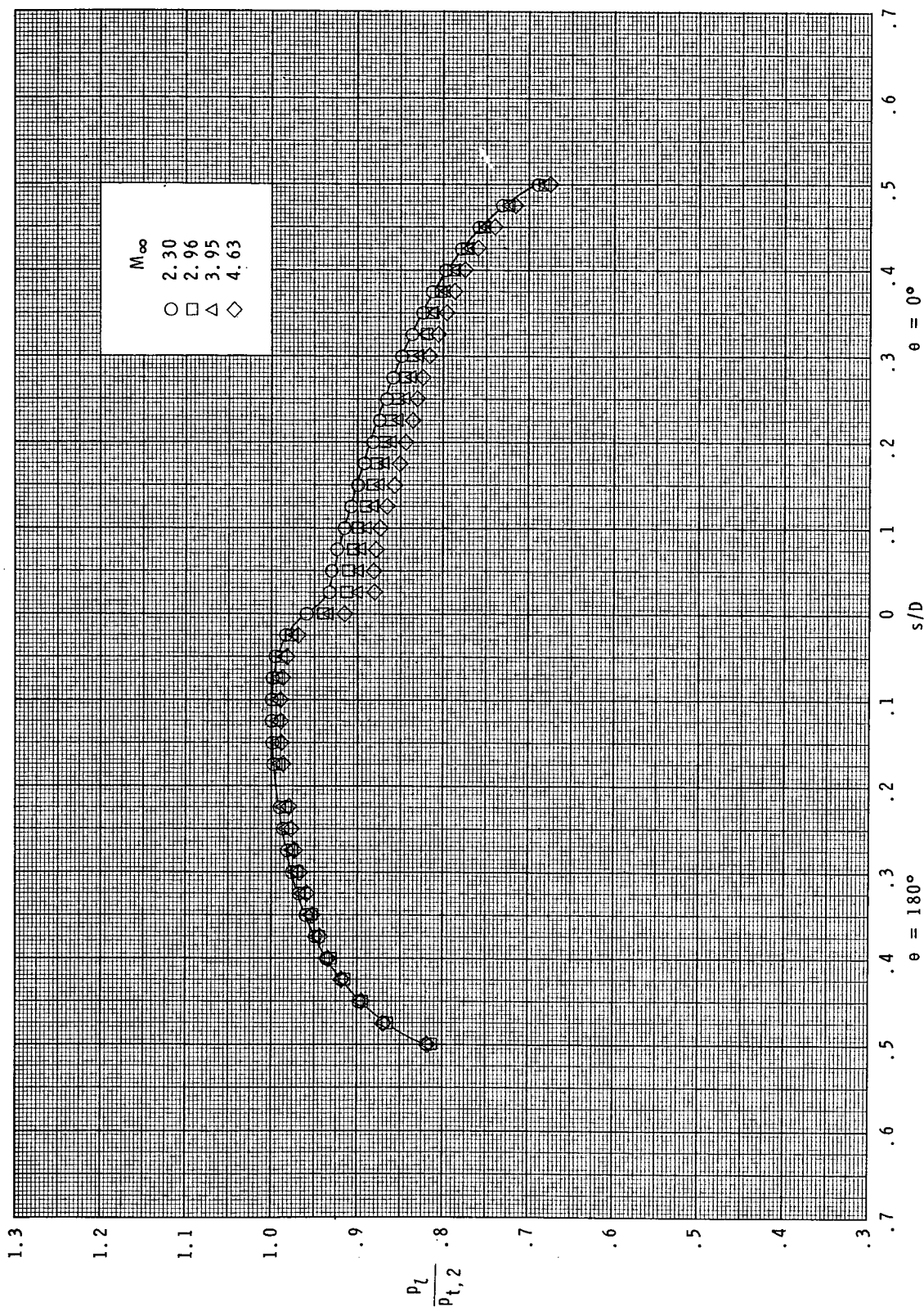
Figure 6.- Continued.



(d) $M_\infty = 4.63$.

Figure 6.- Concluded.

(a) $\alpha = 0^\circ$.Figure 7.- Effect of Mach number on the pressure distributions of the 140° cone. $\phi = 0.0^\circ$.



(b) $\alpha = 10^\circ$.

Figure 7.- Continued.

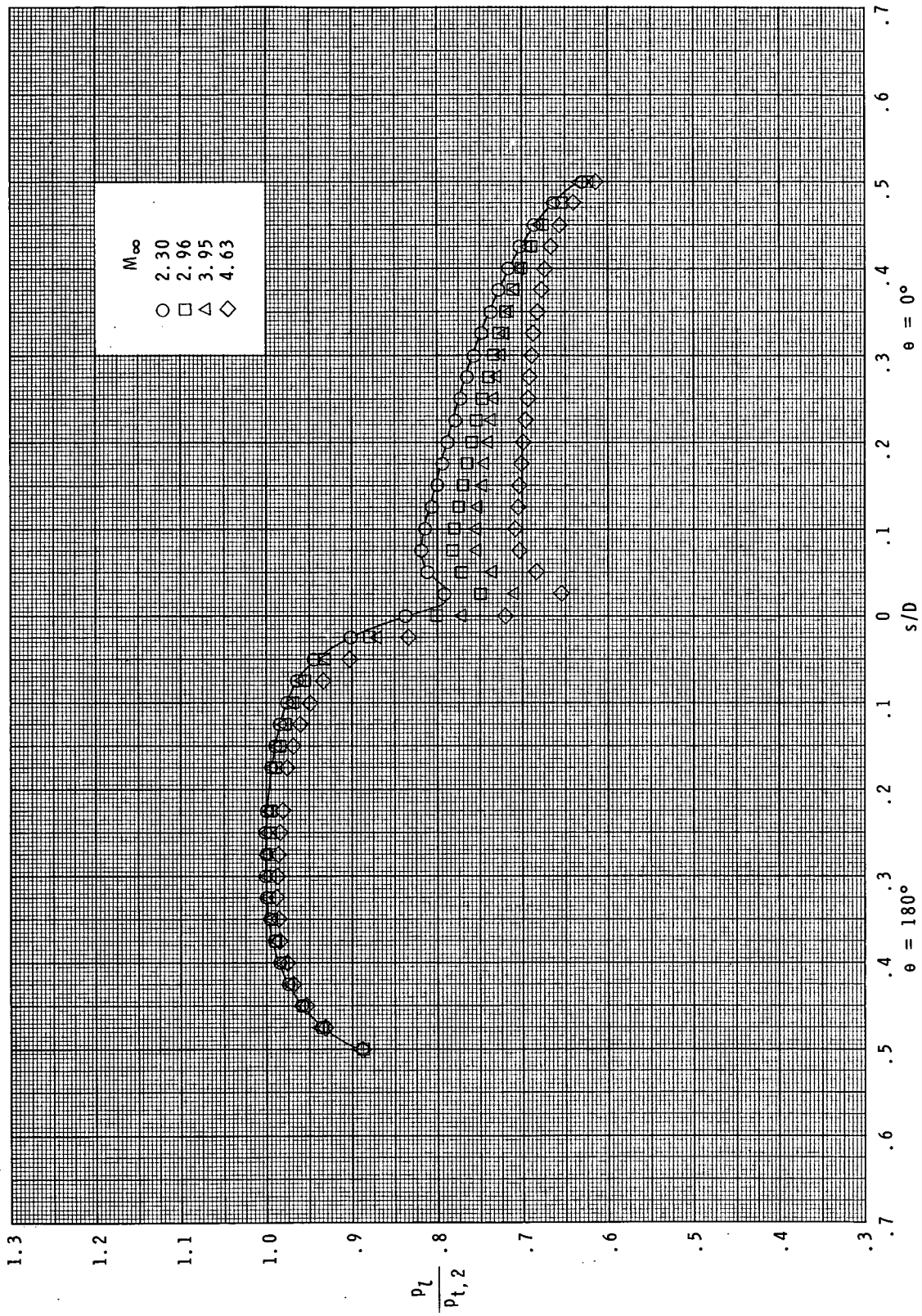
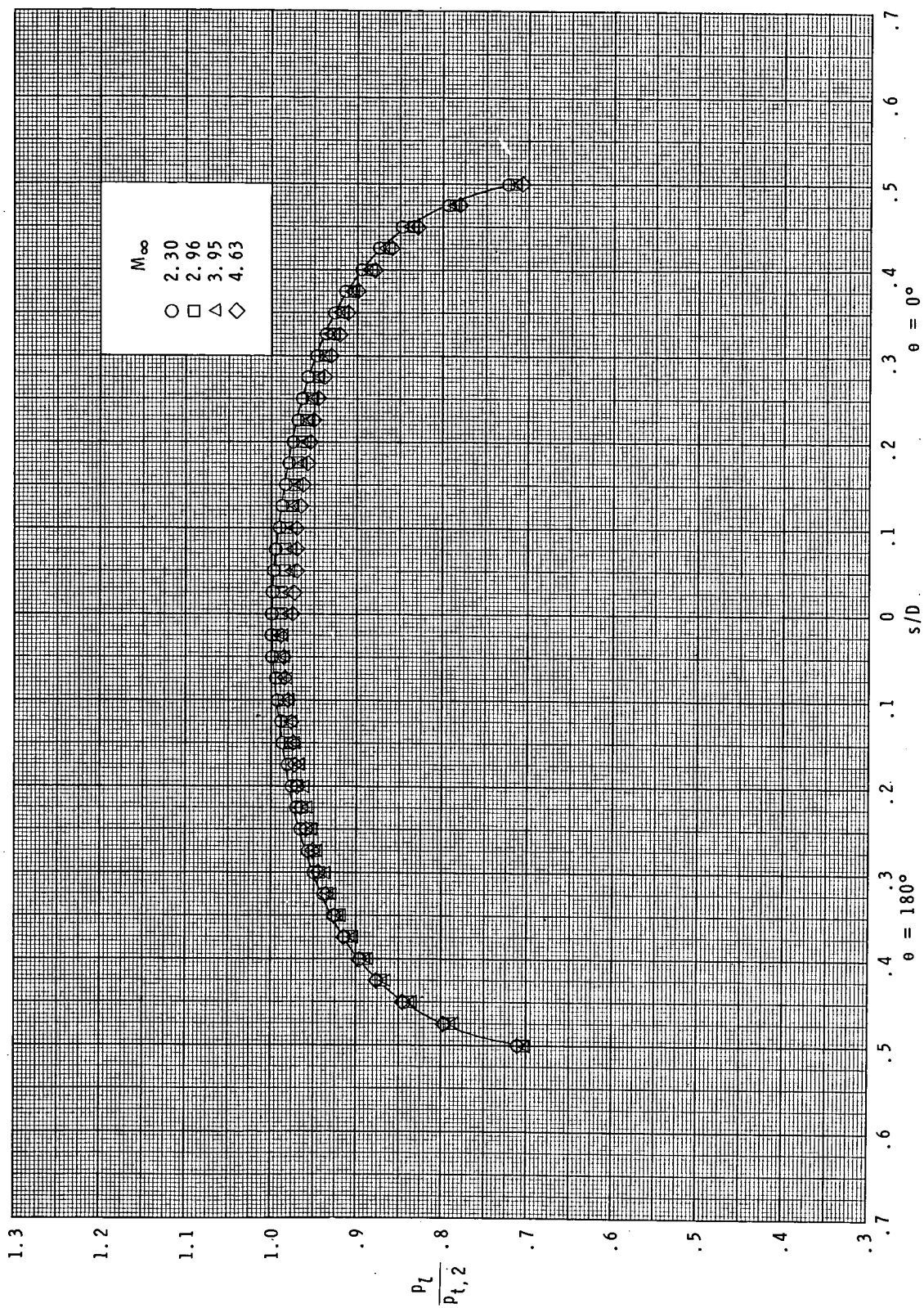
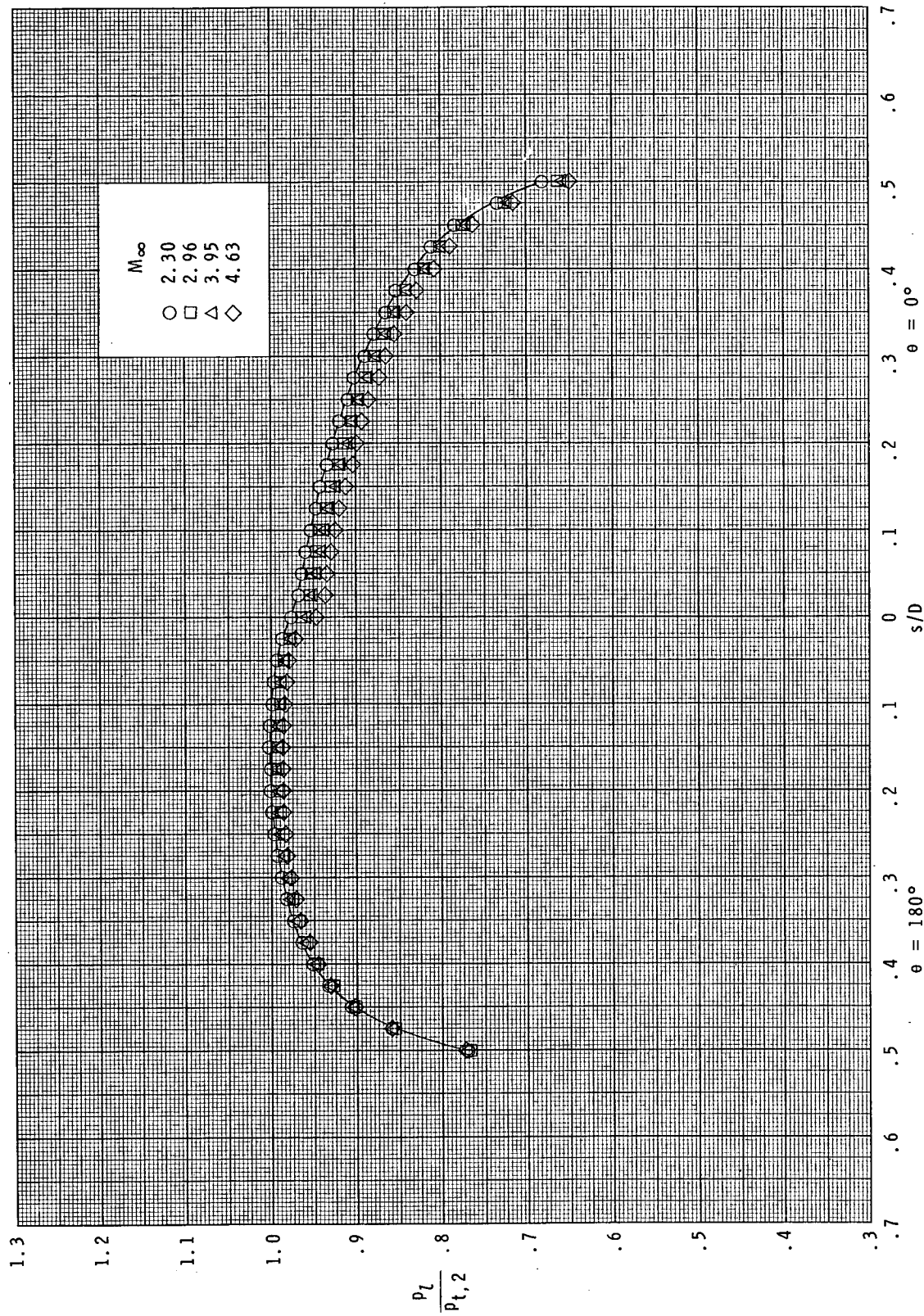
(c) $\alpha = 20^\circ$.

Figure 7.- Concluded.



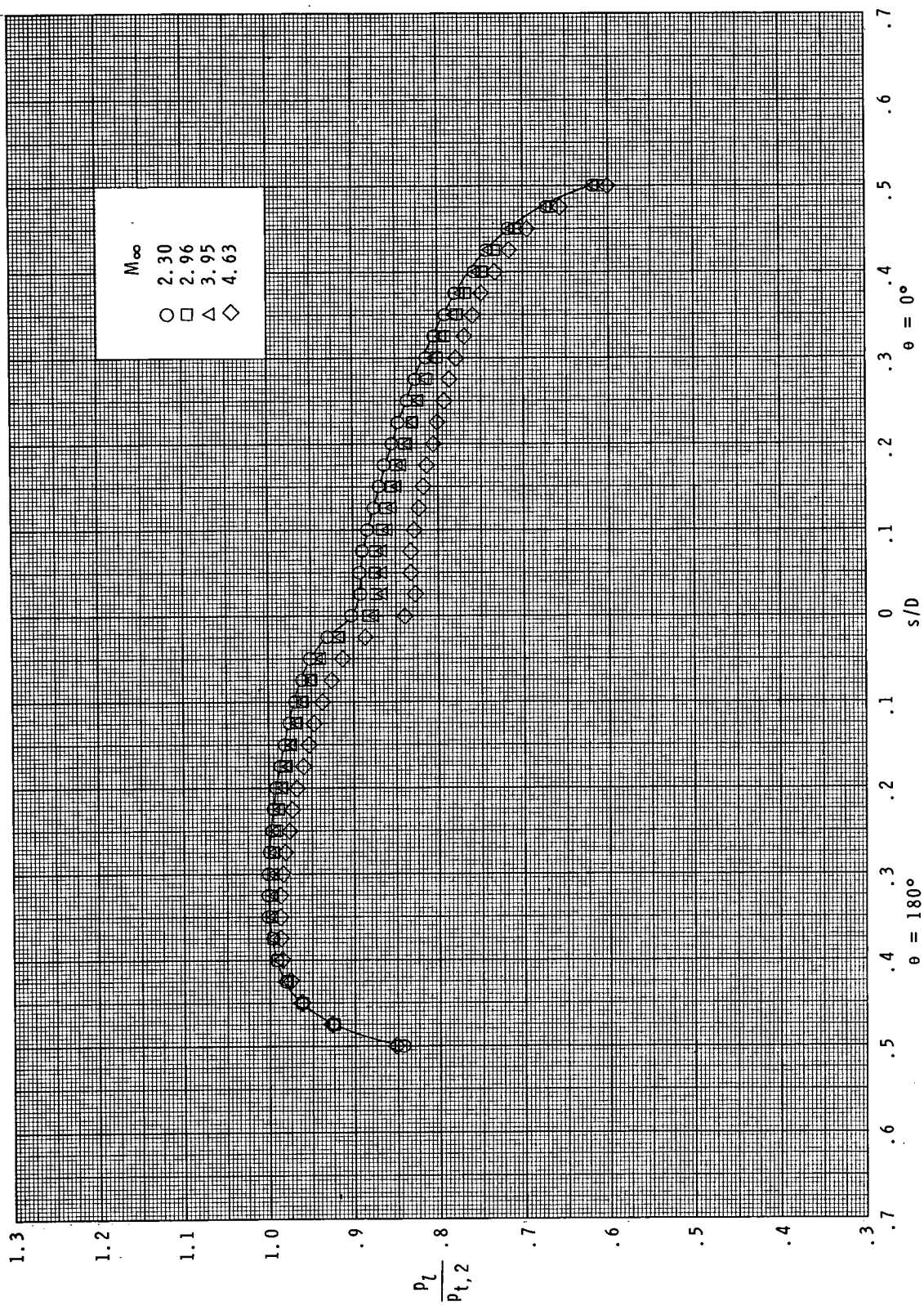
(a) $\alpha = 0^\circ$.

Figure 8.- Effect of Mach number on the pressure distributions of the 160° cone. $\phi = 0.0^\circ$.



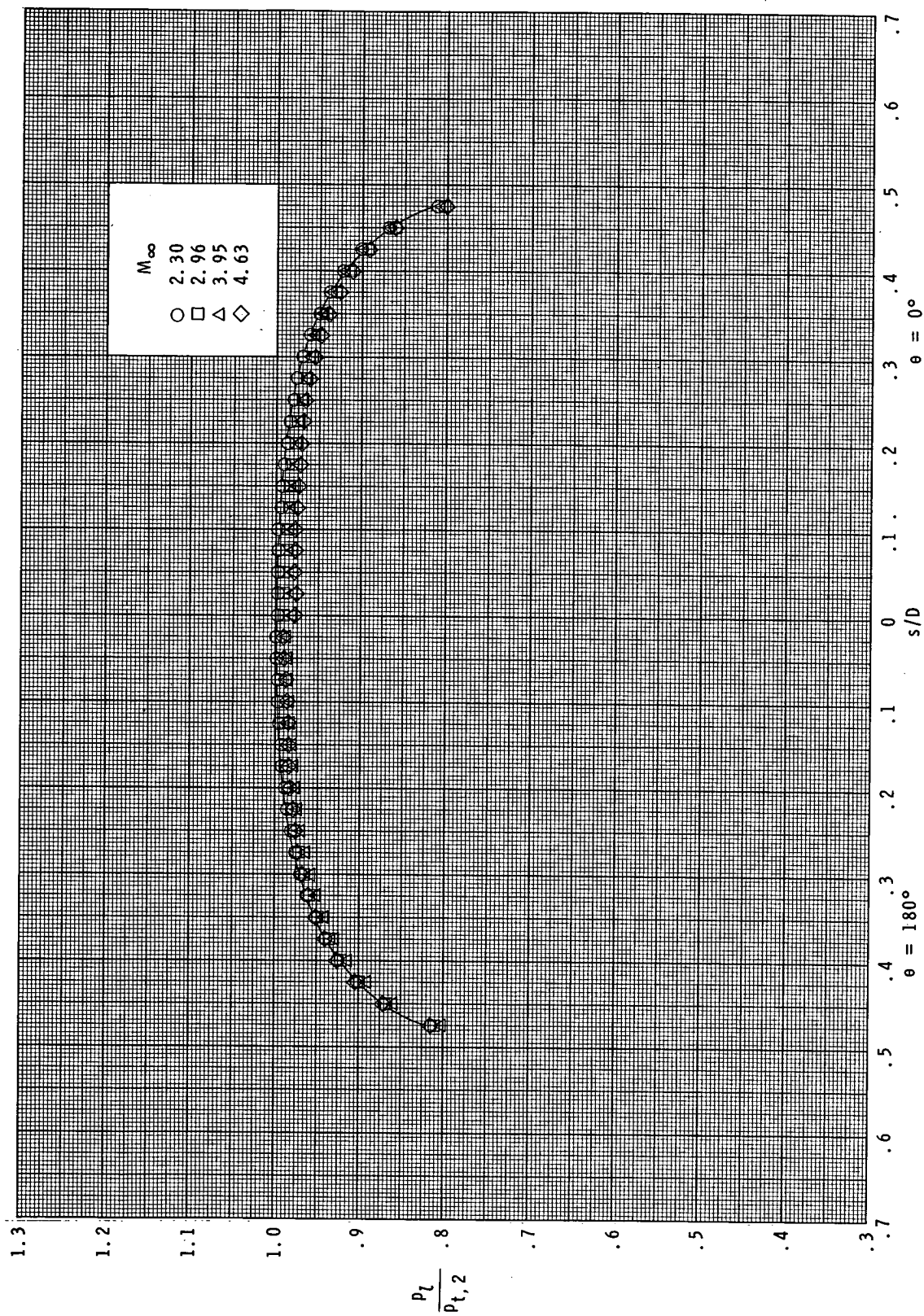
(b) $\alpha = 10^\circ$.

Figure 8.- Continued.



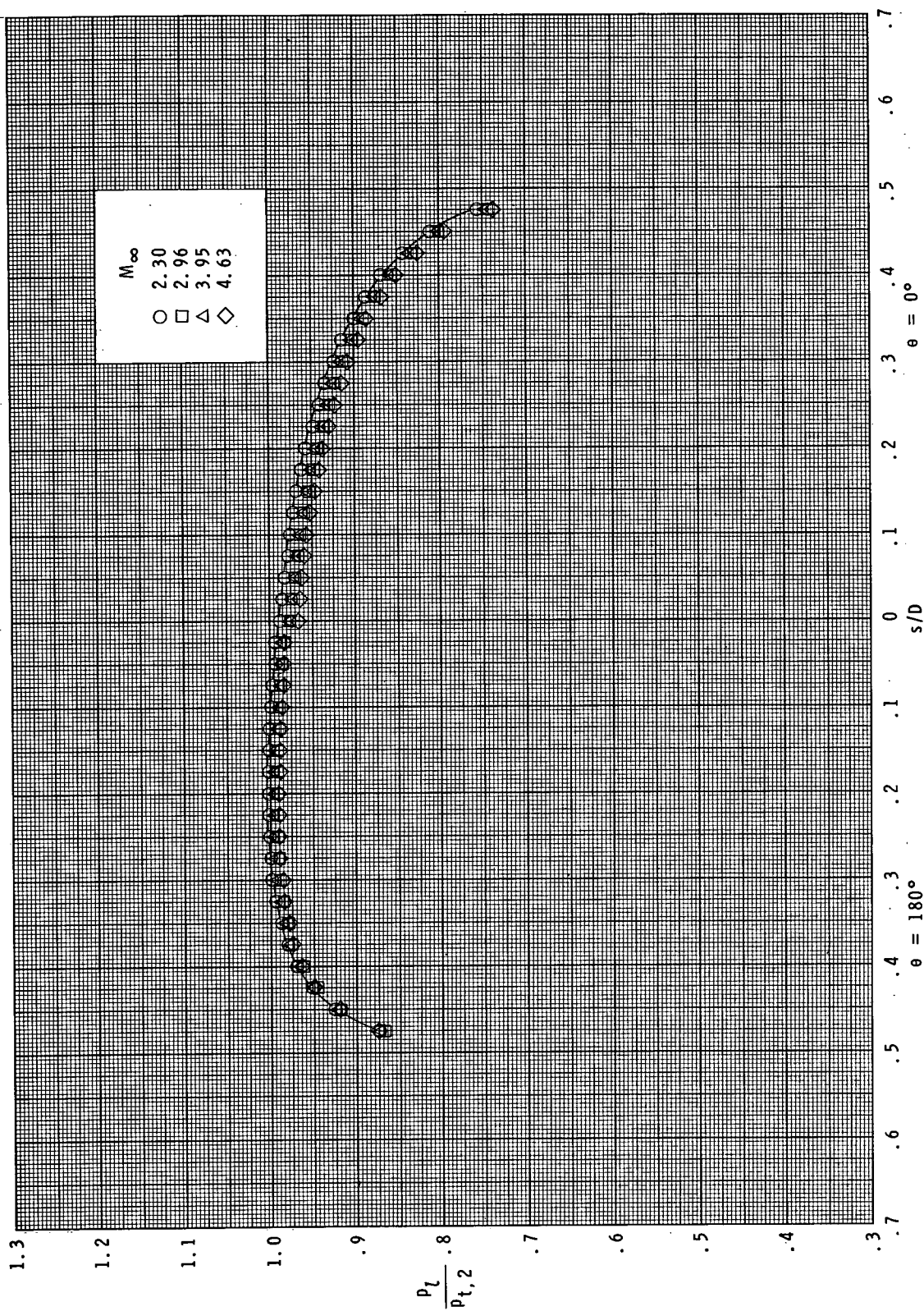
(c) $\alpha = 20^\circ$.

Figure 8.- Concluded.



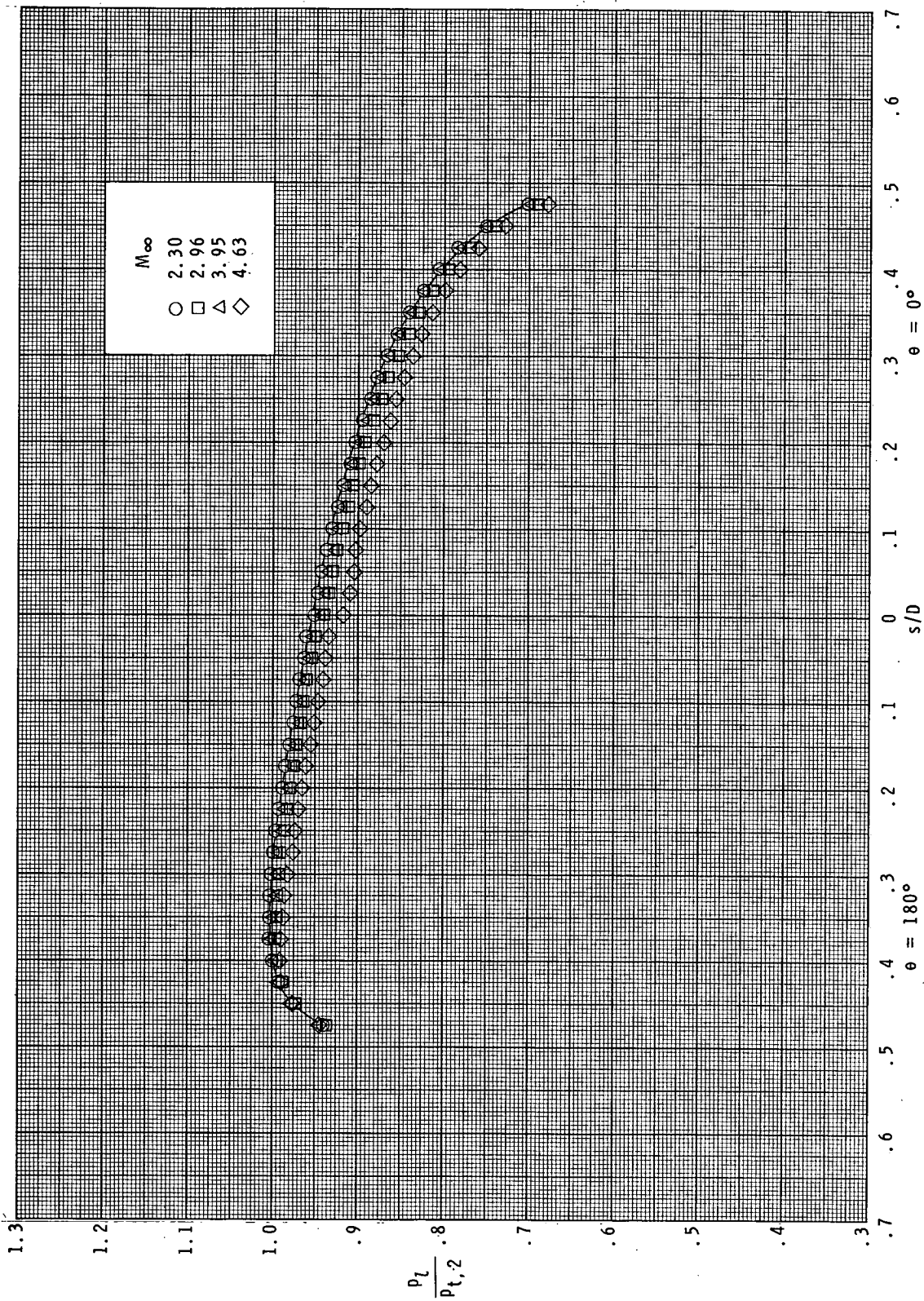
(a) $\alpha = 0^\circ$.

Figure 9.7 Effect of Mach number on the pressure distributions of the 180° cone (flat disk). $\phi = 0.0^\circ$.



(b) $\alpha = 10^\circ$.

Figure 9.- Continued.



(c) $\alpha = 20^\circ$.

Figure 9. - Concluded.

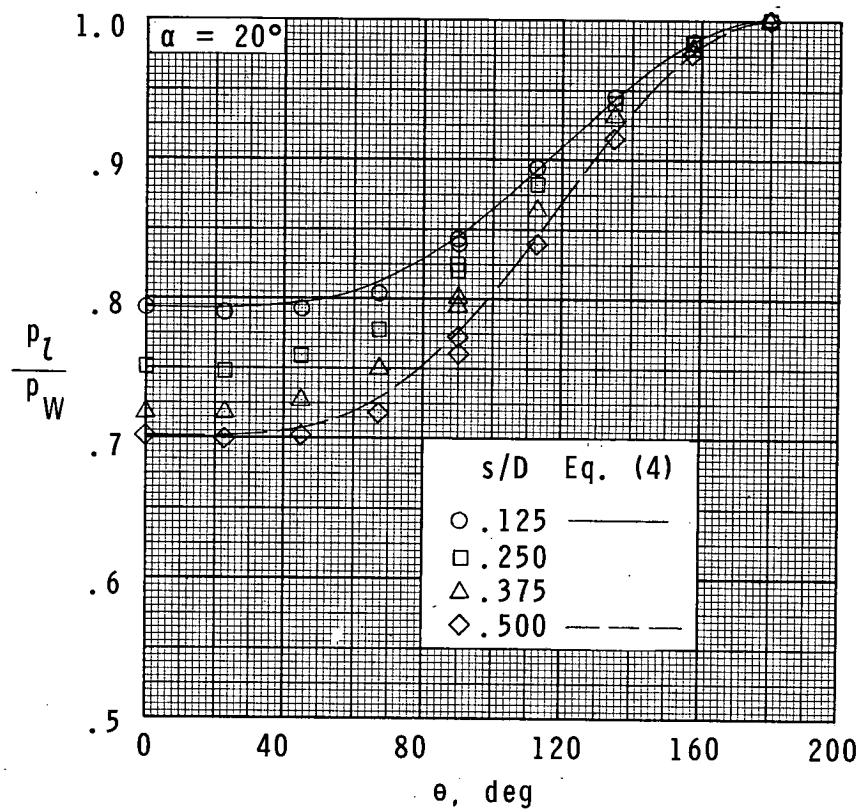
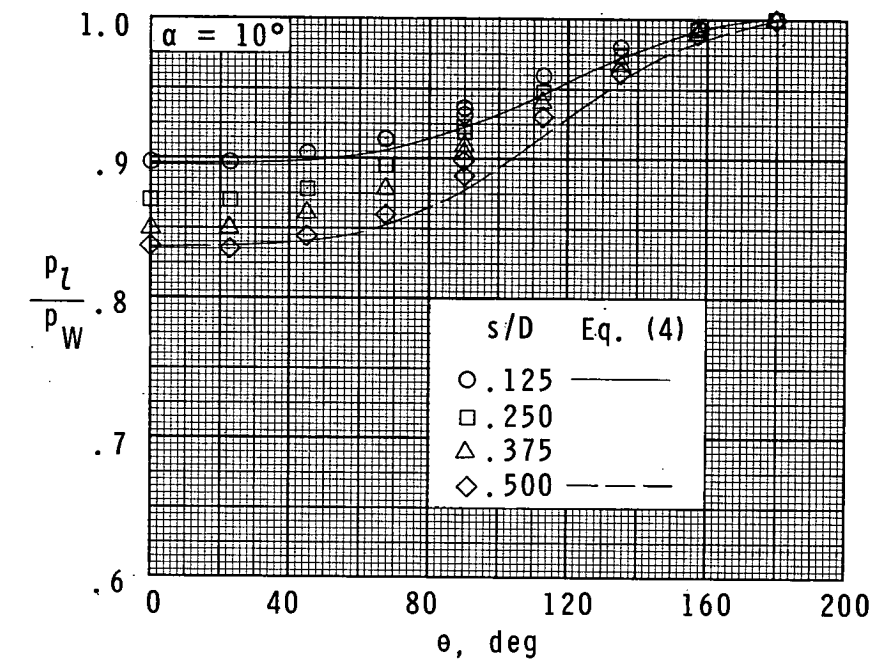


Figure 10.- Circumferential pressure distributions for the 140° cone at two angles of attack and $M_\infty = 2.96$.

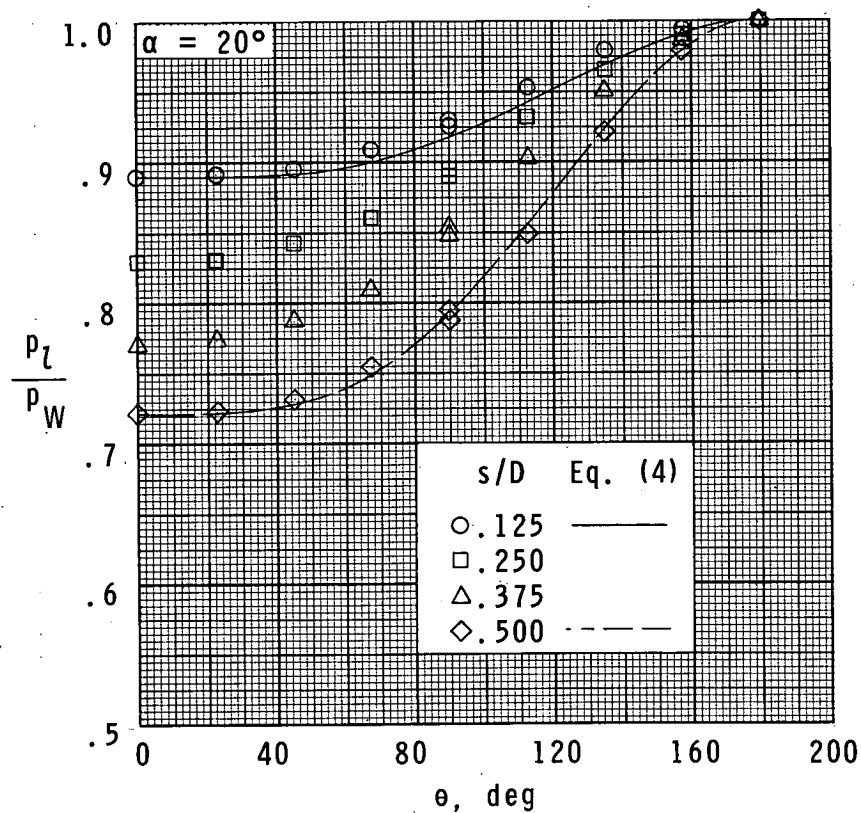
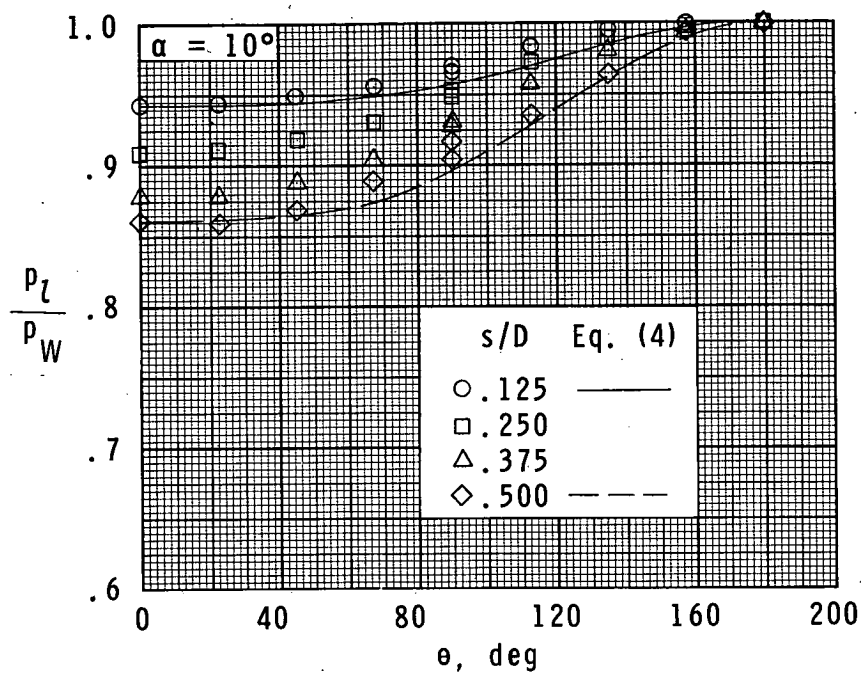


Figure 11.- Circumferential pressure distributions for the 160° cone at two angles of attack and $M_\infty = 2.96$.

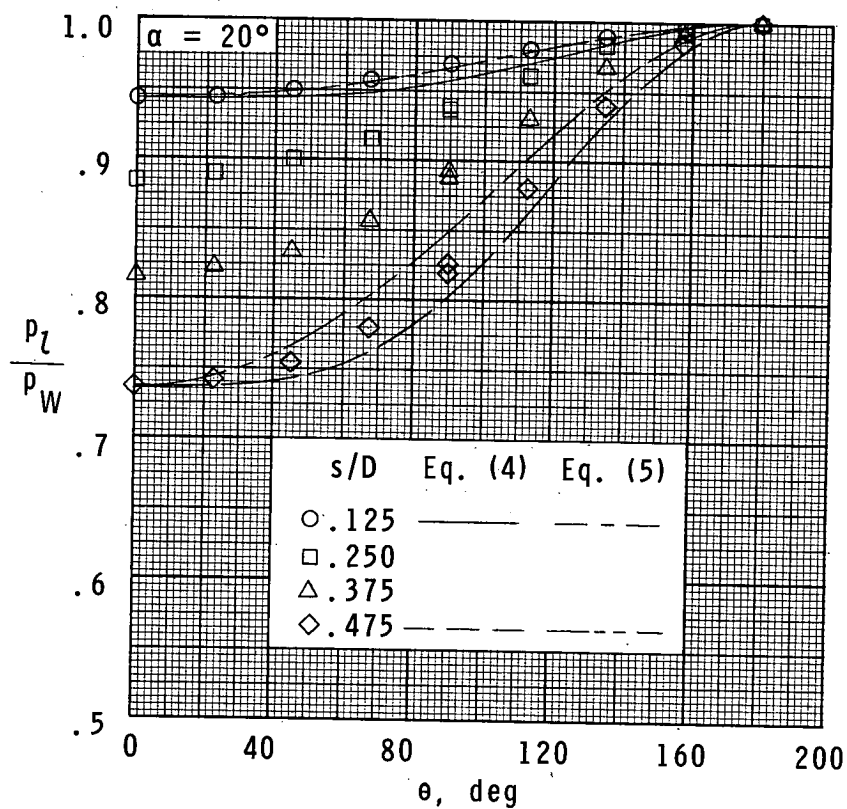
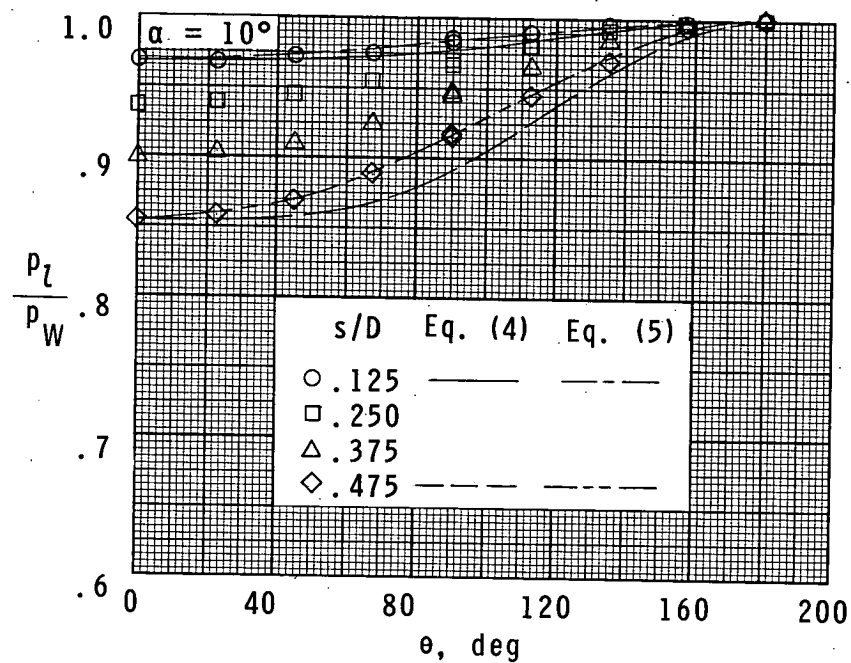


Figure 12.- Circumferential pressure distributions for the 180° cone (flat disk) at two angles of attack and $M_\infty = 2.96$.

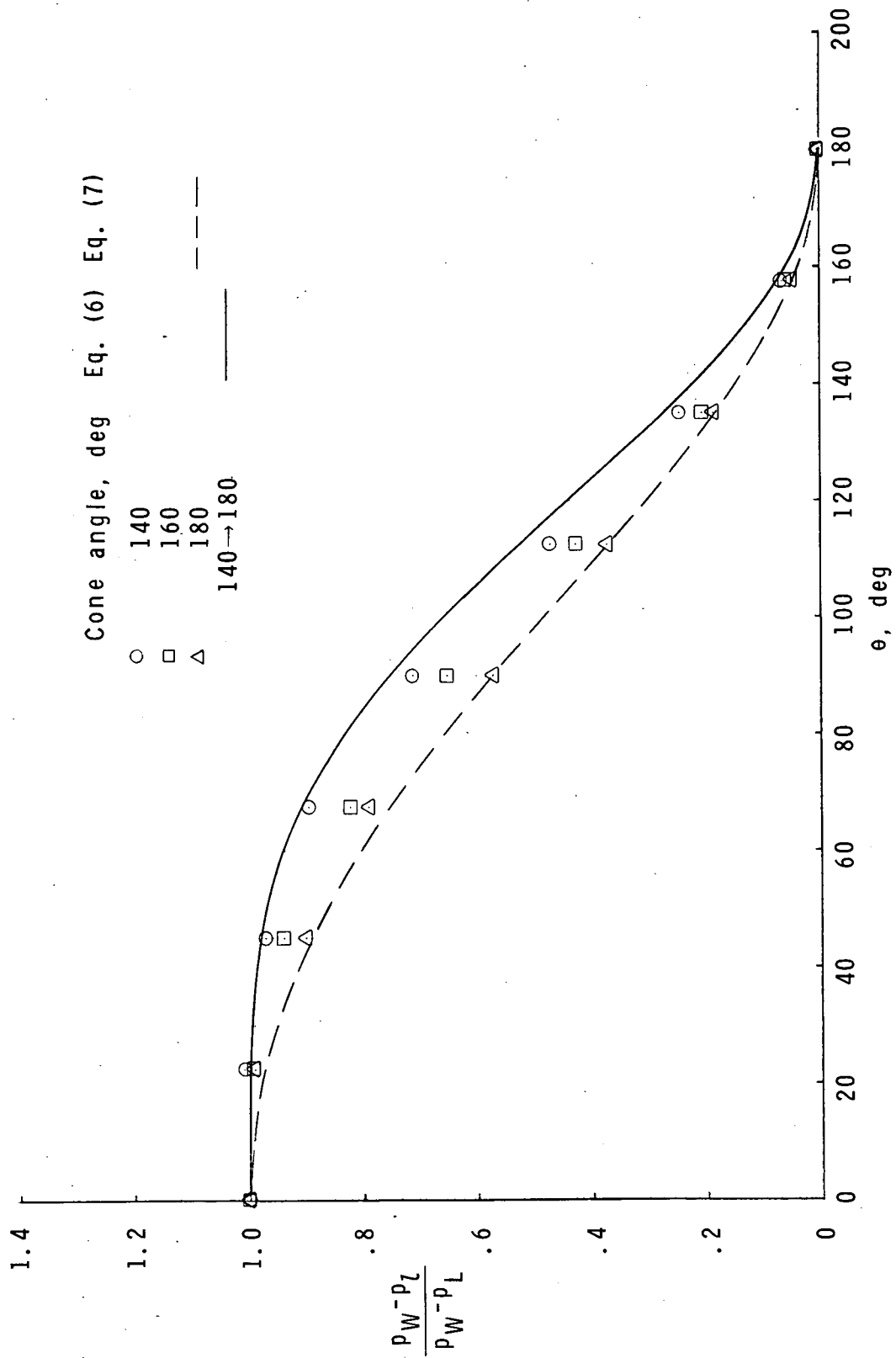


Figure 13.- Comparison of experimental and empirical circumferential pressure distributions for the 140°, 160°, and 180° cones at $M_{\infty} = 2.96$.

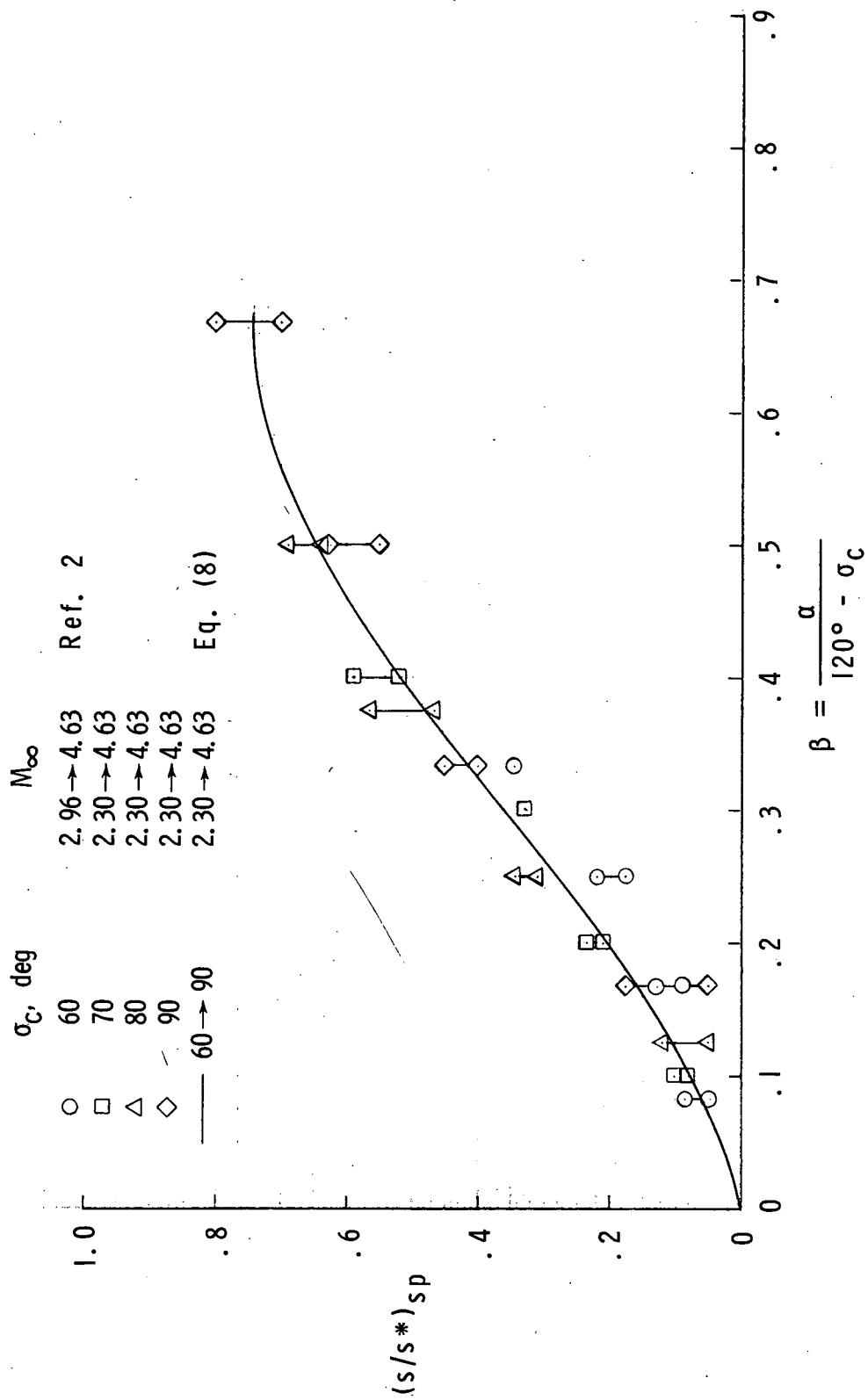


Figure 14.- Correlation of stagnation-point location for the cones at various angles of attack. (Connected symbols indicate maximum deviation within Mach number range.)

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